

# **Navigation Problems for U.S. Coast Guard Exams**

How to Solve Every Problem Type on Exams from 200 to Unlimited Tonnage  
Near Coastal and Oceans

**Christopher D. Nolan**  
Practical Navigator Training  
[www.practicalnavigator.org](http://www.practicalnavigator.org)



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## **How to Use This Textbook**

This series of guides assumes that readers want to either refresh or master certain navigation techniques in order to pass an exam or meet other qualification requirements and is therefore written in a “no-nonsense” fashion.

Standard texts such as Bowditch and Dutton’s do an excellent job of discussing navigation theory. What they lack are clear instructions on navigation problem solving to the level required for exams or problem solving. This guide attempts to furnish concrete example problems to help mariners master the techniques.

Each problem type features a brief introduction followed by a handful of cultivated example problems with detailed solutions, including snapshots from required publications or ephemerides. Most problems are taken directly from the US Coast Guard test database and therefore represent the types of problems expected on the Navigation Problems license exams. After the demonstration section are extra practice problems and answers that you can solve on your own.

When ephemeris data are required, all figures are taken from the 1981 Training Nautical Almanac, Sight Reduction Tables for Marine Navigation (Pub HO 229), or the 1983 Tide and Tidal Current Tables. All publications are available on the web or via the companion online course, available at <https://practical-navigator-training.teachable.com/p/navigation-problems-for-uscg-exams>.

## **Study Strategy for Your Exam**

The main types of examinations are near coastal or oceans. On oceans exams, you may see traditional “near coastal” topics, so it pays to be proficient in all categories. It is recommended to start with near coastal problems and master those before moving on to oceans problems. Additionally, exam problems are often synthesized from several different skills. For example, chronometer problems are included in almost all oceans navigation problems involving celestial bodies.

Aside from the near coastal and oceans distinction, license levels each have their own knowledge requirements. For example, 200-ton ocean candidates are not required to be proficient in Gnomonic chart navigation, while 500-ton ocean masters are. Although required knowledge is found in 46 CFR 11.910, they are synthesized, re-ordered, and sometimes re-named for convenience in this text. However, the original CFR is also included below.

The best strategy for your exam is to master individual topics before moving on to new topics. You should be able to restate any required formulae, know the variety of problem types you may encounter, and routinely solve problems at a success rate over 95% before moving on. From there, it is simply a matter of repetition.

## Study Strategy for Your Exam (Required Knowledge)

Source: 46 CFR 11.910

- 1 = Unlimited Master & Mate
- 2 = 500/1600 Ton Master
- 3 = Unlimited 2<sup>nd</sup>/3<sup>rd</sup> Mate and 500/1600 Ton Mate
- 4 = 200 Ton Master

| Examination topics                      | 1 | 2 | 3 | 4 |
|-----------------------------------------|---|---|---|---|
| Navigation and position determination:  |   |   |   |   |
| Ocean Track Plotting:                   |   |   |   |   |
| Middle Latitude Sailing                 | 1 | 1 | 1 |   |
| Mercator Sailing                        | X | X | X | 7 |
| Great Circle Sailing                    | 1 | 1 | 1 | 7 |
| Parallel Sailing                        | 1 | 1 | 1 |   |
| Estimated Time of Arrival               | X | X | X |   |
| Piloting:                               |   |   |   |   |
| Distance Off                            | X | X | X | X |
| Bearing Problems                        | X | X | X | X |
| Fix or Running Fix                      | X | X | X | X |
| Chart Navigation                        | X | X | X | X |
| Dead Reckoning                          | X | X | X | X |
| Celestial Observations:                 |   |   |   |   |
| Latitude by Polaris                     | 1 | 1 | 1 | 1 |
| Latitude by Meridian Transit (Any Body) | 1 | 1 |   |   |
| Latitude by Meridian Transit (Sun Only) |   |   | 1 | 1 |
| Fix or Running Fix (Any Body)           | 1 | 1 | 1 |   |
| Fix or Running Fix (Sun Only)           |   |   |   | 1 |
| Star Identification                     | 1 | 1 | 1 |   |
| Star Selection                          | 1 | 1 | 1 |   |
| Times of Celestial Phenomena:           |   |   |   |   |
| Time of Meridian Transit (Any Body)     | 1 | 1 |   |   |
| Time of Meridian Transit (Sun Only)     |   |   | 1 | 1 |
| Zone Time of Sun Rise/Set/Twilight      | 1 | 1 | 1 | 1 |
| Speed by RPM                            | X | X | X |   |
| Fuel Conservation                       | X | X |   | 1 |

| Examination topics                                     | 1 | 2 | 3 | 4 |
|--------------------------------------------------------|---|---|---|---|
| Electronic Navigation                                  | X | X | X | X |
| Instruments & Accessories                              | X | X | X | X |
| Aids to Navigation                                     | X | X | X | X |
| Charts, Navigation Publication, & Notices to Mariners  | X | X | X | X |
| Nautical Astronomy & Navigation Definitions            | 1 | 1 | 1 | 1 |
| Chart Sketch                                           |   |   |   |   |
| Seamanship:                                            |   |   |   |   |
| Marlinspike Seamanship                                 |   |   | X | X |
| Purchases, Blocks, & Tackle                            |   |   | X | X |
| Watchkeeping:                                          |   |   |   |   |
| COLREGS                                                | X | X | X | X |
| Inland Navigational Rules                              | X | X | X | X |
| Basic Principles, Watchkeeping                         | X | X | X | X |
| Navigation Safety Regulations (33 CFR 164)             | X |   | X |   |
| Compass - Magnetic & Gyro:                             |   |   |   |   |
| Principles, Operation, and Maintenance of Gyro Compass | X | X | X | 7 |
| Principles of Magnetic Compass                         | X | X | X | X |
| Gyro Compass Error/Correction                          | X | X | X | 7 |
| Magnetic Compass Error/Correction                      | X | X | X | X |
| Determination of Compass Error:                        |   |   |   |   |
| Azimuth (Any Body)                                     | X | X | X | 7 |
| Azimuth (Sun Only)                                     |   |   |   |   |
| Amplitude (Any Body)                                   | X | X | X | 7 |
| Amplitude (Sun Only)                                   |   |   |   |   |
| Terrestrial Observation                                | X | X | X | X |

## **Study Strategy for Your Exam (Simplified Requirements with Module)**

|                                           | Q108             | Q116              | Q126            | Q141          | Not Applicable  |
|-------------------------------------------|------------------|-------------------|-----------------|---------------|-----------------|
| <b>Navigation Problems: Near Coastal</b>  | Unlimited Master | 2nd/3rd Unlimited | 500/1600 Master | 500/1600 Mate | 200 Master/Mate |
| Mercator Sailing                          | x                | x                 | x               | x             |                 |
| ETA                                       | x                | x                 | x               | x             |                 |
| Speed by RPM                              | x                | x                 | x               | x             |                 |
| Fuel Conservation                         | x                |                   | x               |               |                 |
| Electronic Navigation (Chronometer)       | x                | x                 | x               | x             |                 |
| Distance Off, Bearing, Dead Reckoning     | x                | x                 | x               | x             |                 |
| Gyro Error                                | x                | x                 | x               | x             |                 |
| Magnetic Compass Error                    | x                | x                 | x               | x             |                 |
| Azimuth                                   | x                | x                 | x               | x             |                 |
| Amplitude                                 | x                | x                 | x               | x             |                 |
| Tides and Currents                        | x                | x                 | x               | x             |                 |
|                                           | Q109             | Q117              | Q127            | Q142          | Q154            |
| <b>Navigation Problems: Oceans</b>        | Unlimited Master | 2nd/3rd Unlimited | 500/1600 Master | 500/1600 Mate | 200 Master/Mate |
| Middle Latitude Sailing                   | x                | x                 | x               | x             |                 |
| Mercator Sailing                          | x                | x                 | x               | x             | x               |
| Great Circle Sailing                      | x                | x                 | x               | x             | x               |
| Parallel Sailing                          | x                | x                 | x               | x             |                 |
| ETA                                       | x                | x                 | x               | x             |                 |
| Distance Off, Bearing, and Dead Reckoning | x                | x                 | x               | x             | x               |
| Chart Navigation (Gnomonic)               | x                |                   | x               |               |                 |
| Latitude by Polaris                       | x                | x                 | x               | x             | x               |
| Latitude by Meridian Transit              | x                | x                 | x               | x             | x               |
| Sight Reduction                           | x                | x                 | x               | x             | x               |
| Sight Reduction (Fix or Running Fix)      | x                | x                 | x               | x             | x               |
| Star Identification                       | x                | x                 | x               | x             |                 |
| Star Selection                            | x                | x                 | x               | x             |                 |
| Zone Time of Rise/Set/Twilight/Transit    | x                | x                 | x               | x             | x               |
| Azimuth                                   | x                | x                 | x               | x             |                 |
| Amplitude                                 | x                | x                 | x               | x             |                 |
| Tides and Currents                        | x                | x                 | x               | x             |                 |

## **About the Author**

Christopher D. Nolan graduated with honors from the U.S. Coast Guard Academy in 2002 with a bachelor's degree in Marine and Environmental Science. He also graduated from Oregon State University in 2016 with a master's degree in Fisheries and Wildlife Administration.

In the Coast Guard, he served aboard the following cutters:

ALEX HALEY (WMEC-39) – Kodiak, AK. First Lieutenant (3rd Mate)  
DORADO (WPB-87306) – Crescent City, CA. Commanding Officer (Master)  
EAGLE (WIX-327) – New London, CT. Navigator/Operations Officer (2nd Mate)  
JEFFERSON ISLAND (WPB-1340) – Portland, ME. Commanding Officer (Master)

After completing service in the USCG, he sailed as a master of the sailing school vessels CORWITH CRAMER and ROBERT C. SEAMANS and taught as an assistant professor of Nautical Science with Sea Education Association in Woods Hole, MA. He also served as the master of the START OF INDIA, an engineless square rigger associated with the San Diego Maritime Museum.

After obtaining his original mariner's license in 2006, he now holds an STCW license as Master, less than 3000 GT and a domestic license as Master up to 1600 GRT upon oceans.

He is the co-author of *Eagle Seamanship – A Manual for Square Rigger Sailing* and the author of *The Cutterman's Guide to Passing the Rules of the Road Exam*, and *The Cutterman's Guide to Maneuvering Boards*, as well as *The Cutterman's Guide to Basic Celestial Navigation*.

Additionally, he teaches online and in-person professional maritime licensing courses as part of Practical Navigator Training [www.practicalnavigator.org](http://www.practicalnavigator.org).

## **Basic Navigational Math Review**

Certain basic calculations are necessary for successfully solving later, more advanced problems. This preface serves as a refresher for basic navigational calculations.

### **Converting Positions to and from Decimal Notation**

Given a standard position in latitude and longitude, converting to decimal notation is completed by dividing the minutes of position by 60.

**Problem P-1.** Convert  $24^{\circ} 15.7'$  N into decimal notation.

Step 1: Break the initial position into degrees and minutes of position.  
 $24^{\circ} 15.7' = 24^{\circ} + 15.7'$

Step 2: Divide the minutes of position by 60.  
 $\frac{15.7'}{60} = 0.262^{\circ}$

Step 3: Combine the degrees and decimals of position into a final answer.  
 $24^{\circ} + 0.262^{\circ} = \mathbf{24.262^{\circ} N}$

Given a decimal position in latitude and longitude, converting to standard notation is completed by multiplying the decimal portion of the position by 60.

**Problem P-2.** Convert  $133.673^{\circ}$  W into standard notation.

Step 1: Break the initial position into degrees and decimals of position.  
 $133.673^{\circ} = 133^{\circ} + 0.673^{\circ}$

Step 2: Multiply the decimal of position by 60.  
 $0.673^{\circ} \times 60 = 40.38'$

Step 3: Combine the degrees and minutes of position into a final answer.  
 $133^{\circ} + 40.38' = \mathbf{133^{\circ} 40.38' W}$

### Converting Time into Decimal Notation

Given a standard time, converting to decimal notation is completed by dividing the minutes by 60.

**Problem P-3.** Convert 3 hours and 16 minutes into decimal notation.

- Step 1: Break the initial position into degrees and minutes of position.  
3 hours, 16 minutes = 3 hours + 16 minutes.
- Step 2: Divide the minutes of position by 60.  
 $\frac{16}{60} = 0.266$  hours.
- Step 3: Combine the degrees and decimals of position into a final answer.  
3 hours + 0.266 hours = **3.266 hours**

Given a decimal time, converting to standard notation is completed by multiplying the decimal portion by 60.

**Problem P-4.** Convert 4.277 hours into standard notation of hours and minutes, and then again into hours, minutes, and seconds.

- Step 1: Break the initial position into degrees and decimals of position.  
4.277 hours = 4 hours + 0.277 hours.
- Step 2: Multiply the decimal portion by 60.  
 $0.277 \times 60 = 16.62$  minutes.
- Step 3: Combine the degrees and minutes of position into a final answer.  
4 hours + 16.62 minutes = **4 hours, 16.62 minutes.**
- Step 4: If necessary, converting decimal minutes to seconds is accomplished the same way.  
 $16.62$  minutes = 16 minutes + 0.62 minutes.  
 $0.62 \times 60 = 37.2$  seconds.  
16.62 minutes = 16 minutes, 37.2 seconds.  
Thus, the total answer would be **4 hours, 16 minutes, 37.2 seconds.**

### Converting Time Between Zone Time and GMT

Depending on the problem, it is sometimes convenient to work exclusively in Zone Time or GMT. So if a problem describes times in multiple formats, it is necessary to convert to or from GMT.

**Problem P-5.** If the current ship time is 0834 and the ship is observing ZD (+4), what is the time in GMT?

Step 1: To correct zone time to GMT in the western hemisphere, add the zone descriptor to the ship time.

$$0834 + 0400 = \mathbf{1234}.$$

**Problem P-6.** If the current ship time is 0834, and the ship is observing ZD (-4), what is the time in GMT?

Step 1: To correct zone time to GMT in the eastern hemisphere, subtract the zone descriptor from the ship time.

$$0834 - 0400 = \mathbf{0434}.$$

### Adding Degrees and Minutes

Adding degrees and minutes causes the most arithmetic errors when solving navigation problems, because the degree system is based on 60, not 100. It is usually best to complete the math in two steps:

**Problem P-7.** Add the following two latitudes.  $23^{\circ} 47.3' \text{ N}$  and  $11^{\circ} 33.9' \text{ N}$ .

Step 1: Add the whole degrees first and then the minutes.

$$23^{\circ} 47.3' + 11^{\circ} 33.9' = (23^{\circ} + 11^{\circ}) + (47.3' + 33.9') = 34^{\circ} + 81.2'$$

Step 2: Convert the minutes into degrees and minutes.

$$81.2' = 1^{\circ} + 21.2'$$

Step 3: Sum the parts.

$$34^{\circ} + 1^{\circ} + 21.2' = \mathbf{35^{\circ} 21.2' \text{ N}}$$



**Problem P-8.** Sum the following two latitudes.  $23^{\circ} 17.3' \text{ N}$  and  $11^{\circ} 33.9' \text{ S}$ . Sometimes when subtracting minutes, it is helpful convert  $1^{\circ}$  to minutes (e.g. subtract  $1^{\circ}$  but add  $60'$  to the minutes value).

Step 1: Subtract  $1^{\circ}$  and then add  $60'$  to the first value to make the math easy.

$$\underline{23^{\circ} 17.3'} + (-11^{\circ} 33.9') = \underline{22^{\circ} 77.3'} + (-11.33.9')$$

Step 2: Add the whole degrees first and then the minutes.

$$(22^{\circ} + (-11^{\circ})) + (77.3' + (-33.9')) = 11^{\circ} + 43.4'$$

Step 3: Sum the parts.

$$11^{\circ} + 43.4' = \mathbf{11^{\circ} 43.4' \text{ N}}$$

## Interpolating for Values of Greenwich Hour Angle

In order to save space in the almanac, values of Greenwich Hour Angle in the Nautical Almanac are given only for whole hours. Unless observations are made on the hour, interpolation is necessary. This principle applies for all celestial bodies, and the correction is always added.

**Problem P-9.** It is 22 February and you make an observation of the sun at 15:48:13 UTC. The tabular value of GHA of the sun for 1500 UTC is  $41^{\circ} 37.3'$ . What is the calculated GHA of the sun for the time of observation?

Step 1: Note the tabular value of GHA for the next lower whole hour (1500 UTC in this case).  
1500 UTC =  $41^{\circ} 37.3'$ .

Step 2: Determine the difference in time between the time of observation and the next lower whole hour (1500 UTC in this case).  
Observation – 15:48:13  
Whole Hours – 15:00:00  
Difference = 15:48:13 – 15:00:00 = 00:48:13

Step 3: Enter the Increments and Corrections pages in the Nautical Almanac and find the value for 48 minutes and 13 seconds in the “Sun/Planets” column.  
48 minutes 13 seconds:  $12^{\circ} 03.3'$  correction

|       |          |          |
|-------|----------|----------|
| 22 00 | 176 36.1 | S10 18.2 |
| 01    | 191 36.2 | 17.3     |
| 02    | 206 36.2 | 16.4     |
| 03    | 221 36.3 | .. 15.5  |
| 04    | 236 36.4 | 14.6     |
| 05    | 251 36.5 | 13.6     |
| 06    | 266 36.6 | S10 12.7 |
| 07    | 281 36.6 | 11.8     |
| 08    | 296 36.7 | 10.9     |
| S 09  | 311 36.8 | .. 10.0  |
| U 10  | 326 36.9 | 09.1     |
| N 11  | 341 37.0 | 08.2     |
| D 12  | 356 37.1 | S10 07.3 |
| A 13  | 11 37.1  | 06.4     |
| Y 14  | 26 37.2  | 05.4     |
| 15    | 41 37.3  | .. 04.5  |
| 16    | 56 37.4  | 03.6     |
| 17    | 71 37.5  | 02.7     |
| 18    | 86 37.6  | S10 01.8 |
| 19    | 101 37.6 | 00.9     |
| 20    | 116 37.7 | 10 00.0  |
| 21    | 131 37.8 | 9 59.0   |
| 22    | 146 37.9 | 58.1     |
| 23    | 161 38.0 | 57.2     |

48<sup>m</sup>

INCREMENTS AND CORRECTIONS

49<sup>m</sup>

| 48 | SUN<br>PLANETS | ARIES   | MOON    | v<br>or<br>d | Corr <sup>n</sup> | v<br>or<br>d | Corr <sup>n</sup> | v<br>or<br>d | Corr <sup>n</sup> | 49 | SUN<br>PLANETS | ARIES   | MOON    | v<br>or<br>d | Corr <sup>n</sup> | v<br>or<br>d | Corr <sup>n</sup> | v<br>or<br>d | Corr <sup>n</sup> |
|----|----------------|---------|---------|--------------|-------------------|--------------|-------------------|--------------|-------------------|----|----------------|---------|---------|--------------|-------------------|--------------|-------------------|--------------|-------------------|
| s  | °              | °       | °       | °            | °                 | °            | °                 | °            | °                 | s  | °              | °       | °       | °            | °                 | °            | °                 | °            | °                 |
| 00 | 12 00.0        | 12 02.0 | 11 27.2 | 0.0          | 0.0               | 6.0          | 4.9               | 12.0         | 9.7               | 00 | 12 15.0        | 12 17.0 | 11 41.5 | 0.0          | 0.0               | 6.0          | 5.0               | 12.0         | 9.9               |
| 01 | 12 00.3        | 12 02.2 | 11 27.4 | 0.1          | 0.1               | 6.1          | 4.9               | 12.1         | 9.8               | 01 | 12 15.3        | 12 17.3 | 11 41.8 | 0.1          | 0.1               | 6.1          | 5.0               | 12.1         | 10.0              |
| 02 | 12 00.5        | 12 02.5 | 11 27.7 | 0.2          | 0.2               | 6.2          | 5.0               | 12.2         | 9.9               | 02 | 12 15.5        | 12 17.5 | 11 42.0 | 0.2          | 0.2               | 6.2          | 5.1               | 12.2         | 10.1              |
| 03 | 12 00.8        | 12 02.7 | 11 27.9 | 0.3          | 0.2               | 6.3          | 5.1               | 12.3         | 9.9               | 03 | 12 15.8        | 12 17.8 | 11 42.2 | 0.3          | 0.2               | 6.3          | 5.2               | 12.3         | 10.1              |
| 04 | 12 01.0        | 12 03.0 | 11 28.2 | 0.4          | 0.3               | 6.4          | 5.2               | 12.4         | 10.0              | 04 | 12 16.0        | 12 18.0 | 11 42.5 | 0.4          | 0.3               | 6.4          | 5.3               | 12.4         | 10.2              |
| 05 | 12 01.3        | 12 03.2 | 11 28.4 | 0.5          | 0.4               | 6.5          | 5.3               | 12.5         | 10.1              | 05 | 12 16.3        | 12 18.3 | 11 42.7 | 0.5          | 0.4               | 6.5          | 5.4               | 12.5         | 10.3              |
| 06 | 12 01.5        | 12 03.5 | 11 28.6 | 0.6          | 0.5               | 6.6          | 5.3               | 12.6         | 10.2              | 06 | 12 16.5        | 12 18.5 | 11 42.9 | 0.6          | 0.5               | 6.6          | 5.4               | 12.6         | 10.4              |
| 07 | 12 01.8        | 12 03.7 | 11 28.9 | 0.7          | 0.6               | 6.7          | 5.4               | 12.7         | 10.3              | 07 | 12 16.8        | 12 18.8 | 11 43.2 | 0.7          | 0.6               | 6.7          | 5.5               | 12.7         | 10.5              |
| 08 | 12 02.0        | 12 04.0 | 11 29.1 | 0.8          | 0.6               | 6.8          | 5.5               | 12.8         | 10.3              | 08 | 12 17.0        | 12 19.0 | 11 43.4 | 0.8          | 0.7               | 6.8          | 5.6               | 12.8         | 10.6              |
| 09 | 12 02.3        | 12 04.2 | 11 29.3 | 0.9          | 0.7               | 6.9          | 5.6               | 12.9         | 10.4              | 09 | 12 17.3        | 12 19.3 | 11 43.7 | 0.9          | 0.7               | 6.9          | 5.7               | 12.9         | 10.6              |
| 10 | 12 02.5        | 12 04.5 | 11 29.6 | 1.0          | 0.8               | 7.0          | 5.7               | 13.0         | 10.5              | 10 | 12 17.5        | 12 19.5 | 11 43.9 | 1.0          | 0.8               | 7.0          | 5.8               | 13.0         | 10.7              |
| 11 | 12 02.8        | 12 04.7 | 11 29.8 | 1.1          | 0.9               | 7.1          | 5.7               | 13.1         | 10.6              | 11 | 12 17.8        | 12 19.8 | 11 44.1 | 1.1          | 0.9               | 7.1          | 5.9               | 13.1         | 10.8              |
| 12 | 12 03.0        | 12 05.0 | 11 30.1 | 1.2          | 1.0               | 7.2          | 5.8               | 13.2         | 10.7              | 12 | 12 18.0        | 12 20.0 | 11 44.4 | 1.2          | 1.0               | 7.2          | 5.9               | 13.2         | 10.9              |
| 13 | 12 03.3        | 12 05.2 | 11 30.3 | 1.3          | 1.1               | 7.3          | 5.9               | 13.3         | 10.8              | 13 | 12 18.3        | 12 20.3 | 11 44.6 | 1.3          | 1.1               | 7.3          | 6.0               | 13.3         | 11.0              |
| 14 | 12 03.5        | 12 05.5 | 11 30.5 | 1.4          | 1.1               | 7.4          | 6.0               | 13.4         | 10.8              | 14 | 12 18.5        | 12 20.5 | 11 44.9 | 1.4          | 1.2               | 7.4          | 6.1               | 13.4         | 11.1              |

Step 4: Apply the correction to the tabular GHA for whole hours. The correction is always added.  
GHA for 1500 UTC =  $41^{\circ} 37.3'$   
Correction =  $12^{\circ} 03.3'$   
Total GHA =  $41^{\circ} 37.3' + 12^{\circ} 03.3' = 53^{\circ} 40.6'$

## Interpolating for Values of Declination

In order to save space in the almanac, values of declination in the Nautical Almanac are given only for whole hours. Unless observations are made on the hour, interpolation is necessary. This principle applies for all celestial bodies. The correction is either added or subtracted, depending on the trend of hourly declination.

Typically, mental interpolation is sufficient, however, the concept of  $d$  correction ensures accuracy. The abbreviated process is to note the daily  $d$  value at the bottom of each daily page. Then, enter the Increments and Corrections pages for the minutes necessary, finding the appropriate  $d$  value on that page and noting the correction.

**Problem P-10.** It is 22 February and you make an observation of the sun at 15:48:13 UTC. The tabular value of declination of the sun at 1500 UTC is S  $10^{\circ} 04.5'$ . What is the calculated declination of the sun for the time of observation?

Step 1: Note the tabular value of declination for the next lower whole hour (1500 UTC in this case).  
1500 UTC = S  $10^{\circ} 04.5'$ .

Step 2: Determine the difference in time between the time of observation and the next lower whole hour (1500 UTC in this case). Rounding to the nearest minute is sufficient.

Observation – 15:48:13

Whole Hours – 15:00:00

Difference = 15:48:13 –

15:00:00 = 48 min.

Step 3: Note the  $d$  value at the bottom of the daily page.  
 $d = 0.9$

Step 4: Enter the Increments and Corrections pages in the Nautical Almanac and find the page for 48 minutes. On that page, find the “ $v$  or  $d$  Corr” column, and locate the heading for a  $d$  value of 0.9. Note the correction  
 $d$  value – 0.9.  
Correction = 0.7'

|                   |          |          |
|-------------------|----------|----------|
| 22 00             | 176 36.1 | S10 18.2 |
| 01                | 191 36.2 | 17.3     |
| 02                | 206 36.2 | 16.4     |
| 03                | 221 36.3 | 15.5     |
| 04                | 236 36.4 | 14.6     |
| 05                | 251 36.5 | 13.6     |
| 06                | 266 36.6 | S10 12.7 |
| 07                | 281 36.6 | 11.8     |
| 08                | 296 36.7 | 10.9     |
| S 09              | 311 36.8 | 10.0     |
| U 10              | 326 36.9 | 09.1     |
| N 11              | 341 37.0 | 08.2     |
| D 12              | 356 37.1 | S10 07.3 |
| A 13              | 11 37.1  | 06.4     |
| Y 14              | 26 37.2  | 05.4     |
| 15                | 41 37.3  | 04.5     |
| 16                | 56 37.4  | 03.6     |
| 17                | 71 37.5  | 02.7     |
| 18                | 86 37.6  | S10 01.8 |
| 19                | 101 37.6 | 00.9     |
| 20                | 116 37.7 | 10 00.0  |
| 21                | 131 37.8 | 9 59.0   |
| 22                | 146 37.9 | 58.1     |
| 23                | 161 38.0 | 57.2     |
| S.D. 16.2 $d$ 0.9 |          |          |

| 48 <sup>m</sup> INCREMENTS AND CORRECTIONS 49 <sup>m</sup> |         |         |         |                          |                          |                          |    |         |         |         |                          |
|------------------------------------------------------------|---------|---------|---------|--------------------------|--------------------------|--------------------------|----|---------|---------|---------|--------------------------|
| 48                                                         | SUN     | ARIES   | MOON    | $v$ or Corr <sup>n</sup> | $v$ or Corr <sup>n</sup> | $v$ or Corr <sup>n</sup> | 49 | SUN     | ARIES   | MOON    | $v$ or Corr <sup>n</sup> |
| 00                                                         | 12 00.0 | 12 02.0 | 11 27.2 | 0.0 0.0                  | 0.0 4.9                  | 12.0 9.7                 | 00 | 12 15.0 | 12 17.0 | 11 41.5 | 0.0 0.0                  |
| 01                                                         | 12 00.3 | 12 02.2 | 11 27.4 | 0.1 0.1                  | 0.1 4.9                  | 12.1 9.8                 | 01 | 12 15.3 | 12 17.3 | 11 41.8 | 0.1 0.1                  |
| 02                                                         | 12 00.5 | 12 02.5 | 11 27.7 | 0.2 0.2                  | 0.2 5.0                  | 12.2 9.9                 | 02 | 12 15.5 | 12 17.5 | 11 42.0 | 0.2 0.2                  |
| 03                                                         | 12 00.8 | 12 02.7 | 11 27.9 | 0.3 0.3                  | 0.3 5.1                  | 12.3 9.9                 | 03 | 12 15.8 | 12 17.8 | 11 42.2 | 0.3 0.3                  |
| 04                                                         | 12 01.0 | 12 03.0 | 11 28.2 | 0.4 0.4                  | 0.4 5.2                  | 12.4 10.0                | 04 | 12 16.0 | 12 18.0 | 11 42.5 | 0.4 0.4                  |
| 05                                                         | 12 01.3 | 12 03.2 | 11 28.4 | 0.5 0.5                  | 0.5 5.3                  | 12.5 10.1                | 05 | 12 16.3 | 12 18.3 | 11 42.7 | 0.5 0.5                  |
| 06                                                         | 12 01.5 | 12 03.5 | 11 28.6 | 0.6 0.6                  | 0.6 5.4                  | 12.6 10.2                | 06 | 12 16.5 | 12 18.5 | 11 42.9 | 0.6 0.6                  |
| 07                                                         | 12 01.8 | 12 03.7 | 11 28.9 | 0.7 0.7                  | 0.7 5.4                  | 12.7 10.3                | 07 | 12 16.8 | 12 18.8 | 11 43.2 | 0.7 0.7                  |
| 08                                                         | 12 02.0 | 12 04.0 | 11 29.1 | 0.8 0.8                  | 0.8 5.5                  | 12.8 10.3                | 08 | 12 17.0 | 12 19.0 | 11 43.4 | 0.8 0.8                  |
| 09                                                         | 12 02.3 | 12 04.2 | 11 29.3 | 0.9 0.9                  | 0.9 5.6                  | 12.9 10.4                | 09 | 12 17.3 | 12 19.3 | 11 43.7 | 0.9 0.9                  |
| 10                                                         | 12 02.5 | 12 04.5 | 11 29.6 | 1.0 0.8                  | 1.0 5.7                  | 13.0 10.5                | 10 | 12 17.5 | 12 19.5 | 11 43.9 | 1.0 0.8                  |
| 11                                                         | 12 02.8 | 12 04.7 | 11 29.8 | 1.1 0.9                  | 1.1 5.7                  | 13.1 10.6                | 11 | 12 17.8 | 12 19.8 | 11 44.1 | 1.1 0.9                  |
| 12                                                         | 12 03.0 | 12 05.0 | 11 30.1 | 1.2 1.0                  | 1.2 5.8                  | 13.2 10.7                | 12 | 12 18.0 | 12 20.0 | 11 44.4 | 1.2 1.0                  |
| 13                                                         | 12 03.3 | 12 05.2 | 11 30.3 | 1.3 1.1                  | 1.3 5.9                  | 13.3 10.8                | 13 | 12 18.3 | 12 20.3 | 11 44.6 | 1.3 1.1                  |
| 14                                                         | 12 03.5 | 12 05.5 | 11 30.5 | 1.4 1.1                  | 1.4 6.0                  | 13.4 10.8                | 14 | 12 18.5 | 12 20.5 | 11 44.9 | 1.4 1.2                  |

Step 5: Apply the correction to the tabular declination for whole hours. In this case the correction is subtracted because the tabular values of declination are decreasing with time (winter and spring in the northern hemisphere).

Dec for 1500 UTC = S 10° 04.5' (decreasing)

$d$  Correction = 0.7'

Total Dec = 10° 04.5' – 0.7' = **S 10° 03.8'**

Note – this value can be easily estimated with direct interpolation in most cases as follows:

- a) The declination value for 1500 UTC is S 10° 04.5'
- b) The declination value for 1600 UTC is S 10° 03.6', for a difference of 0.9' (same as the  $d$  value)
- c) The time of observation is 15:48:13, or approximately 15.8 hours, for a difference of 0.8 hours.
- d)  $\frac{0.8 \text{ hours}}{1.0 \text{ hours}} = \frac{x \text{ minutes}}{0.9 \text{ minutes}}$
- e)  $0.8 = \frac{x}{0.9}$
- f)  $x = 0.7' =$  declination correction to be applied.

### **Calculating the Local Hour Angle (LHA) of Any Body**

Local Hour Angle (LHA) defines the angle between the observer and a celestial body. LHA ranges from 0° to 359° 59.9'.

In the western hemisphere, Local Hour Angle (LHA) is equal to Greenwich Hour Angle (GHA) minus the observer's longitude (or DR longitude).

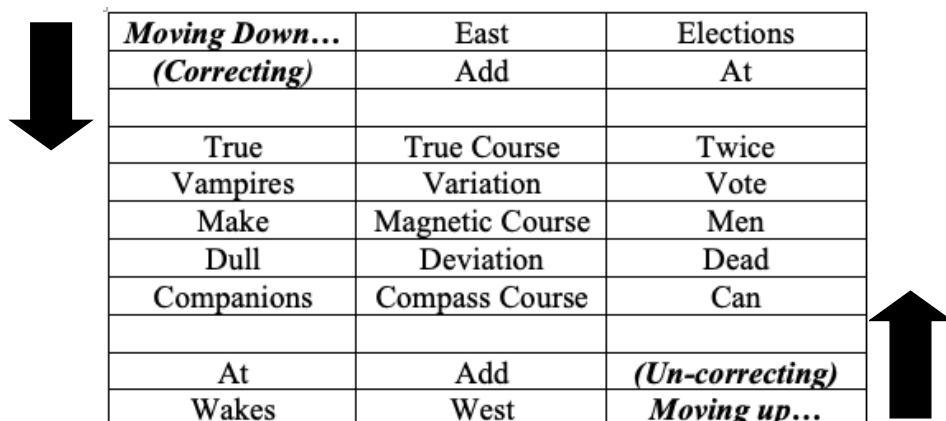
In the eastern hemisphere, LHA is equal to GHA plus the observer's longitude (or DR longitude).

## **Magnetic Compass Problems**



## Magnetic Compass Error Problems

- Terms:
  - True – the true course between two points, as taken from a chart. Written as °T.
  - Variation – the angle between magnetic meridians and geographic meridians at any place expressed in degrees east or west to indicate the direction of magnetic north from true north. This depends on one's location on Earth. Written as °E or °W.
  - Magnetic – bearing relative to magnetic north; compass bearing corrected for deviation. Written as °M.
  - Deviation – the angle between a magnetic meridian and the axis of a compass card, expressed in degrees east or west to quantify the disturbing magnetic influences in the immediate vicinity of the compass. This depends on one's ship heading. Written as °E or °W.
  - Compass – the course indicated on a ship's compass. Written as °psc which means "per steering compass" or "per standard magnetic compass" or "per ship's compass."
- Deviation tables are constructed by "swinging" the ship through a circle and noting true/compass bearings to objects. The table can be entered with either °M or °psc if the values are relatively small. Otherwise it can only be entered with °M and residual deviation is interpolated for entry with °psc. For exam problems, entry into the table from either °M or °psc is sufficient and values can be rounded to the nearest 0.5°.
- Two memory aids are helpful for magnetic compass problems:
  - True Vampires Make Dull Companions (At Wakes).
  - Can Dead Men Vote Twice (At Elections)?
- Below is an example of using the compass correction acronyms:



|                              |                 |                               |
|------------------------------|-----------------|-------------------------------|
| <b><i>Moving Down...</i></b> | East            | Elections                     |
| <b><i>(Correcting)</i></b>   | Add             | At                            |
| True                         | True Course     | Twice                         |
| Vampires                     | Variation       | Vote                          |
| Make                         | Magnetic Course | Men                           |
| Dull                         | Deviation       | Dead                          |
| Companions                   | Compass Course  | Can                           |
| At                           | Add             | <b><i>(Un-correcting)</i></b> |
| Wakes                        | West            | <b><i>Moving up...</i></b>    |

## Magnetic Compass Error Problems

### Course Made Good Problems

COM D1. Your vessel is steering  $195^\circ$  per standard magnetic compass. Variation is  $12^\circ$  west, and deviation is  $4^\circ$  east. What is the true course made good?

Answer:  $187^\circ$  True.

Step 1: Write down the acronym:

T (True Course)

V (Variation)

M (Magnetic Course)

D (Deviation)

C (Compass Course)

AW↓ (This indicates you should add westerly values moving down (correcting), reminding you that the opposite is also true – you should add easterly values when moving up (un-correcting). In this case we will be moving up (un-correcting), so easterly values will be added.

Step 2: Fill in the known values:

T:

V:  $12^\circ$  W

M:

D:  $4^\circ$  E

C:  $195^\circ$  (Steering)

Step 3: Correct or un-correct the compass as required to obtain the magnetic course. In this case, we are moving upwards, or un-correcting, so we will add easterly values and subtract westerly values proceeding **up** the table:

T:

V:  $12^\circ$  W (Given)

M:  $199^\circ$

D:  $4^\circ$  E (Given)

C:  $195^\circ$  (Steering)

Step 4: Determine the true course made good:

**T:  $187^\circ$  T**

V:  $12^\circ$  W (Given)

M:  $199^\circ$  (Calculated)

D:  $4^\circ$  E (Given)

C:  $195^\circ$  (Steering)



## Magnetic Compass Error Problems

COM D2. To clear an obstruction, your vessel must make good a true course of  $330^\circ$  true. Variation in the area is  $15^\circ$  east and the deviation table indicates a value of  $2^\circ$  west for your heading. What is the course to steer per standard magnetic compass?

Answer:  $317^\circ$  per standard magnetic compass.

Step 1: Write down the acronym:

T (True Course)

V (Variation)

M (Magnetic Course)

D (Deviation)

C (Compass Course)

AW↓ (This indicates you should add westerly values moving down (correcting), reminding you that the opposite is also true – you should add easterly values when moving up (un-correcting). In this case we will be moving down (correcting), so westerly values will be added.

Step 2: Fill in the known values:

T:  $330^\circ$  T (Course to make good)

V:  $15^\circ$  E (Given)

M:

D:  $2^\circ$  W (Given)

C:

Step 3: Correct or un-correct the compass as required to obtain the magnetic course. In this case, we are moving downwards, or correcting, so we will add westerly values and subtract easterly values proceeding down the table:

T:  $330^\circ$  T (Course to make good)

V:  $15^\circ$  E (Given)

M:  $315^\circ$  M

D:  $2^\circ$  W (Given)

C:

Step 4: Determine the necessary course to steer:

T:  $330^\circ$  T (Course to make good)

V:  $15^\circ$  E (Given)

M:  $315^\circ$  (Calculated)

D:  $2^\circ$  W (Given)

**C:  $317^\circ$  (Necessary course to steer per standard magnetic compass)**

## Magnetic Compass Error Problems

### Course Made Good with Leeway Problems

COM D3. You desire to make good a true course of  $046^{\circ}$  T. The variation is  $6^{\circ}$  E, magnetic compass deviation is  $12^{\circ}$  W. A northerly wind produces a  $5^{\circ}$  leeway. What is the course to steer per standard magnetic compass to make good the true course?

Answer:  $047^{\circ}$  per steering compass.

Step 1: Write down the acronyms:

T (True Course)

V (Variation)

M (Magnetic Course)

D (Deviation)

C (Compass Course)

AW↓ (Add West)

Step 2: Fill in the known values:

T:  $046^{\circ}$  T (Given – desired)

V:  $6^{\circ}$  E (Given)

M:

D:  $12^{\circ}$  W (Given)

C:

Step 3: Calculate the magnetic course.

T:  $046^{\circ}$  T (Given – desired)

V:  $6^{\circ}$  E (Given)

M:  $040^{\circ}$  M (Calculated)

D:  $12^{\circ}$  W (Given)

C:

Step 4: Calculate the course per steering compass.

T:  $046^{\circ}$  T (Given)

V:  $6^{\circ}$  E (Given)

M:  $040^{\circ}$  M (Calculated)

D:  $12^{\circ}$  W (Given)

C:  $052^{\circ}$  per steering compass (Calculated)

Step 5: Apply leeway to the calculated course to obtain a necessary course to steer.

T:  $046^{\circ}$  T (Given)

V:  $6^{\circ}$  E (Given)

M:  $040^{\circ}$  M (Calculated)

D:  $12^{\circ}$  W (Given)

C:  $052^{\circ}$  per steering compass (Calculated)

Step 6: Subtract  $5^{\circ}$  to account for leeway from a northerly ( $000^{\circ}$  T) wind

**$047^{\circ}$  per steering compass, taking into account leeway.**

## Magnetic Compass Error Problems

### Deviation Table Problems

- See the Gyro Compass Problems section for more detail on gyro compass problems.

COM D4. You swung ship and compared the magnetic compass against the gyro compass to find deviation. Gyro error is  $2^\circ$  E. The variation is  $8^\circ$  W. Find the deviation on a gyro heading of  $196^\circ$  per gyro compass.

| <u>Heading</u> |             | <u>Heading</u> |             | <u>Heading</u> |             |
|----------------|-------------|----------------|-------------|----------------|-------------|
| PSC            | PGC         | PSC            | PGC         | PSC            | PGC         |
| $358.5^\circ$  | $350^\circ$ | $122.5^\circ$  | $110^\circ$ | $239.5^\circ$  | $230^\circ$ |
| $030.5^\circ$  | $020^\circ$ | $152^\circ$    | $140^\circ$ | $269^\circ$    | $260^\circ$ |
| $061.5^\circ$  | $050^\circ$ | $181^\circ$    | $170^\circ$ | $298^\circ$    | $290^\circ$ |
| $092^\circ$    | $080^\circ$ | $210^\circ$    | $200^\circ$ | $327.5^\circ$  | $320^\circ$ |

Answer:  $0.1^\circ$ , rounded to nearest half-degree is  $0.0^\circ$ .

Step 1: Write down the acronyms:

T (True Course)

V (Variation)

M (Magnetic Course)

D (Deviation)

C (Compass Course)

AW↓ (Add West)

Step 2: Fill in the known values in table form for each gyro course bracketing the desired course.

|   | <u><math>170^\circ</math> PGC</u> | <u><math>196^\circ</math> PGC</u> | <u><math>200^\circ</math> PGC</u> |
|---|-----------------------------------|-----------------------------------|-----------------------------------|
| T |                                   |                                   |                                   |
| V | $8^\circ$ W                       | $8^\circ$ W                       | $8^\circ$ W                       |
| M |                                   |                                   |                                   |
| D |                                   |                                   |                                   |
| C | $181^\circ$ PSC                   |                                   | $210^\circ$ PSC                   |
|   |                                   |                                   |                                   |
| G |                                   |                                   |                                   |
| E | $2^\circ$ E                       | $2^\circ$ E                       | $2^\circ$ E                       |
| T |                                   |                                   |                                   |

## Magnetic Compass Error Problems

Step 3: Solve the gyro error portion of the table.

|   | <u>170° PGC</u> | <u>196° PGC</u> | <u>200° PGC</u> |
|---|-----------------|-----------------|-----------------|
| T |                 |                 |                 |
| V | 8° W            | 8° W            | 8° W            |
| M |                 |                 |                 |
| D |                 |                 |                 |
| C | 181° PSC        |                 | 210° PSC        |
| G | 170° PGC        | 196° PGC        | 200° PGC        |
| E | 2° E            | 2° E            | 2° E            |
| T | <b>172° T</b>   | <b>198° T</b>   | <b>202° T</b>   |

Step 4: Transfer the solved gyro error portion of the table (T) to the True Course in the main table. The gyro error portion of the table has been omitted for the remainder of the problem.

|   | <u>170° PGC</u> | <u>196° PGC</u> | <u>200° PGC</u> |
|---|-----------------|-----------------|-----------------|
| T | <b>172° T</b>   | <b>198° T</b>   | <b>202° T</b>   |
| V | 8° W            | 8° W            | 8° W            |
| M |                 |                 |                 |
| D |                 |                 |                 |
| C | 181° PSC        |                 | 210° PSC        |

Step 5: Solve the table for the “Magnetic” course.

|   | <u>170° PGC</u> | <u>196° PGC</u> | <u>200° PGC</u> |
|---|-----------------|-----------------|-----------------|
| T | 172° T          | 198° T          | 202° T          |
| V | 8° W            | 8° W            | 8° W            |
| M | <b>180° M</b>   | <b>206° M</b>   | <b>210° M</b>   |
| D |                 |                 |                 |
| C | 181° PSC        |                 | 210° PSC        |

Step 6: Solve the table for the “Deviation” for the known PGC headings.

|   | <u>170° PGC</u> | <u>196° PGC</u> | <u>200° PGC</u> |
|---|-----------------|-----------------|-----------------|
| T | 172° T          | 198° T          | 202° T          |
| V | 8° W            | 8° W            | 8° W            |
| M | 180° M          | 206° M          | 210° M          |
| D | <b>1° W</b>     |                 | <b>0°</b>       |
| C | 181° PSC        |                 | 210° PSC        |

## Magnetic Compass Error Problems

Step 7: Interpolate the known values of deviation to determine the deviation for the desired PGC heading.

|   | <u>170° PGC</u> | <u>196° PGC</u> | <u>200° PGC</u> |
|---|-----------------|-----------------|-----------------|
| T | 172° T          | 198° T          | 202° T          |
| V | 8° W            | 8° W            | 8° W            |
| M | 180° M          | 206° M          | 210° M          |
| D | 1° W            | <b>TBD - X</b>  | 0°              |
| C | 181° PSC        |                 | 210° PSC        |

Deviation for 170° PGC: 1.0° W

Deviation for 196° PGC: unknown = x

Deviation for 200° PGC: 0.0°

$$200^\circ - 170^\circ = 30^\circ$$

$$200^\circ - 196^\circ = 4^\circ$$

$$1.0^\circ - 0.0^\circ = 1.0^\circ$$

$$\frac{4^\circ}{30^\circ} = \frac{x}{1.0^\circ}$$

**x = 0.133°. Rounded to the nearest half-degree, answer is 0.0°**

## Magnetic Compass Error Problems

### Deviation by Range Problems

COM B1. Your vessel is proceeding down a channel and you see a pair of range lights that are in line dead ahead. The chart indicates that the direction of this pair of lights is  $229^{\circ}$  T, and the variation is  $6^{\circ}$  W. If the heading of your vessel at the time of the sighting was  $232^{\circ}$  per standard magnetic compass, what is the deviation?

- a)  $3^{\circ}$  E - correct
- b)  $9^{\circ}$  E
- c)  $3^{\circ}$  W
- d)  $9^{\circ}$  W

COM B2. Your vessel is proceeding up a channel and you see a pair of range lights that are in line ahead. The chart indicates that the direction of this pair of lights is  $014^{\circ}$  T and the variation is  $11^{\circ}$  E. If the heading of your vessel at the time of the sighting is  $009^{\circ}$  per standard magnetic compass, what is the correct deviation?

- a)  $5^{\circ}$  E
- b)  $5^{\circ}$  W
- c)  $6^{\circ}$  E
- d)  $6^{\circ}$  W - correct

COM B3. Your vessel is proceeding up a channel and you see a pair of range lights in line ahead. The chart indicates that the direction of this pair of lights is  $352^{\circ}$  T and the variation is  $4^{\circ}$  W. If the heading of your vessel at the time of the sighting is  $359^{\circ}$  per standard magnetic compass, what is the correct deviation?

- a)  $3^{\circ}$  W - correct
- b)  $7^{\circ}$  E
- c)  $11^{\circ}$  E
- d)  $11^{\circ}$  W

### Course Made Good with Leeway Problems

COM B4. Your vessel is steering course  $111^\circ$  psc, variation for the area is  $5^\circ$  E, and deviation is  $3^\circ$  W. The wind is from the northwest, producing a  $1^\circ$  leeway. What true course are you making good?

- a)  $108^\circ$  T
- b)  $110^\circ$  T
- c)  $112^\circ$  T
- d)  $114^\circ$  T - correct**

COM B5. Your vessel is steering course  $166^\circ$  psc, variation for the area is  $8^\circ$  W, and deviation is  $3^\circ$  W. The wind is from the WSW, producing a  $2^\circ$  leeway. What true course are you making good?

- a)  $153^\circ$  T - correct**
- b)  $157^\circ$  T
- c)  $175^\circ$  T
- d)  $179^\circ$  T

COM B6. Your vessel is steering course  $299^\circ$  psc, variation for the area is  $7^\circ$  W, and deviation is  $4^\circ$  W. The wind is from the SW, producing a  $3^\circ$  leeway. What is the true course you are making good?

- a)  $291^\circ$  T - correct**
- b)  $296^\circ$  T
- c)  $299^\circ$  T
- d)  $313^\circ$  T

COM B7. You desire to make good  $152^\circ$ . The magnetic compass deviation is  $4^\circ$  E, the variation is  $5^\circ$  E, and the gyro error is  $3^\circ$  E. A southwesterly wind produces a  $4^\circ$  leeway. Which course would you steer per standard compass to make good the true course?

- a)  $137^\circ$  psc
- b)  $141^\circ$  psc
- c)  $143^\circ$  psc
- d)  $147^\circ$  psc - correct**

Com B8. You desire to make good a true course of  $038^\circ$ . The variation is  $5^\circ$  E, magnetic compass deviation is  $4^\circ$  W. A southeasterly wind produces a  $4^\circ$  leeway. What is the course to steer per standard magnetic compass to make the true course good?

- a)  $033^\circ$  psc
- b)  $041^\circ$  psc - correct**
- c)  $043^\circ$  psc
- d)  $047^\circ$  psc

### Deviation Table Problems

COM B9. You swung ship and compared the magnetic compass against the gyrocompass to find deviation. Gyro error is  $2^{\circ}$  E. The variation is  $8^{\circ}$  W. Find the deviation on a magnetic compass heading of  $104^{\circ}$ .

| PSC    | PGC  | PSC    | PGC  | PSC    | PGC  |
|--------|------|--------|------|--------|------|
| 358.5° | 350° | 122.5° | 110° | 239.5° | 230° |
| 030.5° | 020° | 152.0° | 140° | 269.0° | 260° |
| 061.5° | 050° | 181.0° | 170° | 298.0° | 290° |
| 092.0° | 080° | 210.0° | 200° | 327.5° | 320° |

- a)  $1.8^{\circ}$  E
- b)  $2.6^{\circ}$  E
- c)  **$2.2^{\circ}$  W - correct**
- d)  $2.7^{\circ}$  W

COM B10. You swung ship and compared the magnetic compass against the gyrocompass to find deviation. Gyro error is  $2^{\circ}$  E. Variation is  $8^{\circ}$  W. Find the deviation on a magnetic compass heading of  $234^{\circ}$ .

| PSC    | PGC  | PSC    | PGC  | PSC    | PGC  |
|--------|------|--------|------|--------|------|
| 358.5° | 350° | 122.5° | 110° | 239.5° | 230° |
| 030.5° | 020° | 152.0° | 140° | 269.0° | 260° |
| 061.5° | 050° | 181.0° | 170° | 298.0° | 290° |
| 092.0° | 080° | 210.0° | 200° | 327.5° | 320° |

- a)  $2.5^{\circ}$  W
- b)  $2.5^{\circ}$  E
- c)  $1.0^{\circ}$  W
- d)  **$0.5^{\circ}$  E - correct**

COM B11. You swung ship and compared the magnetic compass against the gyrocompass to find deviation. Gyro error is  $2^{\circ}$  W. Variation is  $8^{\circ}$  W. Find the deviation on a true heading of  $236^{\circ}$ .

| PSC    | PGC  | PSC    | PGC  | PSC    | PGC  |
|--------|------|--------|------|--------|------|
| 358.5° | 354° | 122.5° | 114° | 239.5° | 234° |
| 030.5° | 024° | 152.0° | 144° | 269.0° | 264° |
| 061.5° | 054° | 181.0° | 174° | 298.0° | 294° |
| 092.0° | 084° | 210.0° | 204° | 327.5° | 324° |

- a)  $1.0^{\circ}$  W
- b)  **$0.5^{\circ}$  E - correct**
- c)  $1.5^{\circ}$  E
- d) 0.0



## **Gyro Compass Problems**



## Gyro Compass Error Problems

- **Important Note:** Gyro compass error problems are often found as part of other problem types, the below demonstrations are not the only type of gyro related problem you will see on your test!
- “pgc” or “per gyro compass” – the course read off a gyroscopic compass.
- Leeway corrections are always applied into the wind (e.g. steer higher into the wind to counteract the wind).

GYR D1. The track line on a chart is  $274^{\circ}$  T. The gyro error is  $1.5^{\circ}$  E. What course would be steered by gyro compass to make good the desired course?

Answer:  $272.5^{\circ}$  pgc. In this case, the only acronym needed is “G-E-T.” The acronym “G-E-T,” which stands for “Gyro course + Easterly Error = True course” will help to solve these problems. Remember that when moving up the acronym, easterly errors are subtracted.

An alternative memory aid is “Gyro Best, Error West” or “Gyro Least, Error East.” This means that if the gyro value is higher (or “best”), compass error is west. The opposite applies for east errors.

- Step 1: Write down the acronym:  
G: (Gyro Course)  
E: (Add Easterly Error – when moving down the acronym)  
T: (True Course)
- Step 2: Fill in the known values:  
G:  
E:  $1.5^{\circ}$  E (Given)  
T:  $274^{\circ}$  T (Given)
- Step 3: Calculate the gyro course to steer.  
**G:  $272.5^{\circ}$  per gyro compass**  
E:  $1.5^{\circ}$  E (Given)  
T:  $274^{\circ}$  T (Given)

## Gyro Compass Error Problems

GYR D2. The true course between two points is  $057^{\circ}$  T. Your gyrocompass has an error of  $3^{\circ}$  east, and you make an allowance for  $1^{\circ}$  of leeway for a north-northeast wind. Which gyro course should be steered to make good the true course?

- Step 1: Write down the acronym:  
G: (Gyro Course)  
E: (Add Easterly Error – when moving down the acronym)  
T: (True Course)
- Step 2: Fill in the known values:  
G:  
E:  $3^{\circ}$  E (Given)  
T:  $057^{\circ}$  T (Given)
- Step 3: Calculate the gyro course to steer.  
G:  $054^{\circ}$  per gyro compass  
E:  $3^{\circ}$  E (Given)  
T:  $057^{\circ}$  T (Given)
- Step 4: Apply a leeway correction:  
Gyro Course  $054^{\circ}$  pgc  
Leeway  $1^{\circ}$  from the north-northeast.  
Correction  $1^{\circ}$  to port (e.g. into the wind).  
**Gyro course to steer:  $053^{\circ}$  pgc.**

## Gyro Compass Error Problems

**Important Note – Gyro Compass Problems are found as part of many other problem types.**

### Gyro Error by Range Problems

GYR B1. Two beacons form a range in the direction of  $221.5^\circ$  T. The range is seen in line from your vessel bearing  $223^\circ$  per gyro compass. The variation is the area is  $4^\circ$  E. What is the error of your gyro compass?

- a)  **$1.5^\circ$  W - correct**
- b)  $2.5^\circ$  W
- c)  $5.5^\circ$  W
- d)  $2.5^\circ$  E

GYR B2. While your vessel is proceeding down a channel, you notice a range of lights in line with your vessel's mast. If your vessel is on course  $001^\circ$  per gyro compass, and the charted value of the range of lights is  $359^\circ$  T, what is the gyro compass error?

- a)  **$2.0^\circ$  W - correct**
- b)  $1.5^\circ$  E
- c)  $1.5^\circ$  W
- d)  $2.0^\circ$  E

### Course to Steer with Gyro Error Problems

GYR B3. The true course between two points is  $194^\circ$ . Your gyrocompass has an error of  $2^\circ$  W and you make an allowance of  $1^\circ$  leeway for a southeast wind. What gyro course should be steered to make the true course good?

- a)  $193^\circ$  pgc
- b)  $195^\circ$  pgc
- c)  **$197^\circ$  pgc - correct**
- d)  $199^\circ$  pgc

GYR B4. The true course between two points is  $337^\circ$ . Your gyrocompass has an error of  $3^\circ$  E and you make an allowance of  $5^\circ$  leeway for a west wind. Which gyro course should be steered to make the true course good?

- a)  **$329^\circ$  pgc - correct**
- b)  $335^\circ$  pgc
- c)  $339^\circ$  pgc
- d)  $345^\circ$  pgc

GYR B5. The true course between two points is  $078^\circ$ . Your gyrocompass has an error of  $2^\circ$  E. You make an allowance of  $3^\circ$  leeway for a north wind. What gyro course should be steered to make the true course good?

- a)  **$073^\circ$  pgc - correct**
- b)  $075^\circ$  pgc
- c)  $077^\circ$  pgc
- d)  $079^\circ$  pgc

## **Electronic Navigation (Chronometer) Problems**





## Chronometer (Electronic Navigation) Problems

- Although there are dedicated Chronometer (Electronic Navigation) problems you may encounter on your exam, Chronometer problems are most often a portion of other problem types.

### Chronometer Problems as part of other Problem Types

CHR D1. According to your watch, you make an observation of the planet Venus at 15:43:30 Greenwich Mean Time. Your watch is known to be 1 minute and 20 seconds fast. At what time did you actually observe Venus?

Answer: 15:42:10 GMT. In order to correct for a known error, simply add or subtract the error, as appropriate, to the watch time to obtain the actual observed time.

Step 1: Watch Time: 15:43:30 GMT

Step 2: Known Error: 00:01:20 (Fast)

Step 3: Calculation:  $15:43:30 - 00:01:20 = \mathbf{15:42:10 \text{ GMT}}$

### Time Tick Problems

CHR D2. You are taking a time-tick using the 2000 signal from Kauai, Hawaii (WWVH). You hear a series of 1-second dashes followed by a 9-second silent period, then a long 1.3 second dash. At the beginning of the long dash, your comparing watch reads 08h 00m 49s. When compared to the chronometer, the comparing watch reads 08h 01m 33s, and the chronometer reads 08h 00m 56s. What is the chronometer error?

Answer: 0m 12s fast. The portions regarding various sounds and lengths of time are distractor information. Note that the chronometer uses 12-hour clock (am and pm), versus the typical 24-hour clock; it is best to immediately correct all times to the 24 hour system to avoid error.

Step 1: Signal time: 20:00:00

Step 2: Comparing watch time at signal: 08:00:49 pm, or 20:00:49

Step 3: Calculate comparing watch error:  $20:00:00 - 20:00:49 = 00:00:49$  fast.

Step 4: Comparing watch (time 2): 20:01:33

Step 5: Corrected comparing watch (time 2):  $20:01:33 - 00:00:49 = 20:00:44$

Step 6: Chronometer (time 2): 20:00:56

Step 7: Chronometer error calculation:  $20:00:44 - 08:00:56 = \mathbf{00:00:12 \text{ fast}}$

## Chronometer (Electronic Navigation) Problems

### Chronometer Rate Problems (this is the only problem in the database)

CHR D3. On 23 July you take a time tick using the 0900 GMT Capetown broadcast. You hear a repeating series of 59 dots followed by a dash. At the beginning of the fifth dash you start your stopwatch. The chronometer reads 08h 39m 16s at the time the stopwatch reads 01m 42s. The chronometer error at 0900 GMT on 22 July was 22m 24s. What is the chronometer rate?

Answer: Losing 00m 02s daily. The portions regarding various sounds and lengths of time are distractor information. Note that the chronometer has “lost” two seconds from the previous day, so the chronometer’s rate is “losing.” The opposite case would be “gaining.”

Step 1: Signal time: 09:00:00

Step 2: Stopwatch at time of signal: 00:00:00.

Step 3: Stopwatch elapsed time: 00:01:42.

Step 4: Chronometer time after elapsed time: 08:39:16.

Step 5: Chronometer time at time of signal:  $08:39:16 - 00:01:42 = 08:37:34$ .

Step 6: Chronometer error:  $09:00:00 - 08:37:34 = 00:22:26$ .

Step 7: Chronometer error on 22 July: 00:22:24 (Given).

Chronometer error on 23 July: 00:22:26.

Difference/Rate =  $00:22:24 - 00:22:26 = - 00:00:02$  (losing)

## Chronometer (Electronic Navigation) Problems

### Chronometer Problems as a component of other Problems.

CHR B1. According to your watch, you make an observation of the sun at 11:27:35 Greenwich Mean Time. Your watch is known to be 2 minutes and 44 seconds fast. At what time did you actually observe the Sun?

- a) **11:24:51 - correct**
- b) 11:29:51
- c) 11:30:19

CHR B2. According to your watch, you make an observation of the moon at 23:37:12 Greenwich Mean Time. Your watch is known to be 47 seconds slow. At what time did you actually observe the moon?

- a) 23:36:25
- b) **23:27:59 - correct**
- c) 23:28:25

### Time Tick Problems

CHR B3. On 12 November, you are taking a time tick using the 1600 GMT BBC broadcast. You hear five pulses followed by a longer pulse. At the start of the longer pulse, you start a stopwatch. You stop the stopwatch at the same time reading the chronometer, with the following results: stopwatch 03m 19s, chronometer 15h 59m 46s. What is the chronometer error?

- a) 01m 14s slow
- b) 03m 19s fast
- c) **03m 33s slow - correct**
- d) 06m 54s slow

CHR B4. You are taking a time tick using the 2100 signal from Callao, Peru. You hear a series of 1-second dashes followed by a 9 second silent period, then a long 1.3 second dash. At the beginning of the long dash, your comparing watch reads 09h 00m 10s. When compared to the chronometer, the watch reads 09h 01m 20s, and the chronometer reads 08h 59m 22s. What is the chronometer error?

- a) **1m 48 slow - correct**
- b) 0m 38s slow
- c) 1m 10s fast
- d) 0m 10s fast

CHR B5. You are taking a time tick using the 1930 signal from Rio de Janeiro, Brazil. You hear the preparatory signal CQ DE PPE repeated several times followed by a short dash (0.4 sec), 60 dots (0.1 sec each), and another short dash. At the beginning of the last dash, the comparing watch reads 07h 30m 08s. When compared to the chronometer, the watch reads 07h 31m 48s, and the chronometer reads 07h 32m 16s. What is the chronometer error?

- a) 0m 28s slow
- b) 1m 40s slow
- c) 0m 08s fast
- d) 0m 36s fast - correct**

CHR B6. You are taking a time tick using the 1400 signal from Buenos Aires, Argentina. You hear a 0.4 second dash followed by a series of dots noting that the 29<sup>th</sup> dot and the 56<sup>th</sup> to 59<sup>th</sup> dots are omitted. At the start of the following 0.4 second dash (which is followed by an 8 second pulse), the comparing watch reads 01h 59m 57s. When compared to the chronometer, the watch reads 02h 00m 38s, and the chronometer reads 02h 01m 33s. What is the chronometer error?

- a) 0m 03s slow
- b) 0m 41s slow
- c) 0m 52s fast - correct**
- d) 1m 36s fast

CHR B7. You are taking a time tick using the 2000 signal from Kekaha-Kauai, Hawaii (WWVH). You hear a series of 1 second dashes followed by a 9 second silent period, then a long 1.3 second dash. At the beginning of the long dash, your comparing watch reads 07h 59m 54s. When compared to the chronometer, the comparing watch reads 08h 00m 00s, and the chronometer reads 08h 00m 06s. What is the chronometer error?

- a) 0m 06s slow
- b) 0m 06 fast
- c) 0m 12s fast
- d) no error - correct**

## **Estimated Time of Arrival Problems**



## Estimated Time of Arrival Problems

### Normal ETA Problems

- Keeping track of time zones (ZD) is the best way to solve these problems.
- Keeping time in GMT is a good strategy for the transit and then convert it to zone time at the end.
- You can find out how many days are in a month in the Nautical Almanac.

ETA D1. At 0600 zone time, on October 22, you depart Manila, latitude  $14^{\circ} 35.0' \text{ N}$ , longitude  $120^{\circ} 58.0' \text{ E}$  (ZD -8). You are bound for Los Angeles, latitude  $33^{\circ} 46.0' \text{ N}$ , longitude  $118^{\circ} 11.0' \text{ W}$ . You estimate your speed of advance to be 20.2 knots. The distance is 6385.9 miles. What is your estimated zone time of arrival in Los Angeles?

Answer: 1805, 3 November.

- Step 1: Calculate the total time steaming:  
 $6385.9 \text{ nm} \div 20.2 \text{ knots} = 316.13 \text{ hours}.$
- Step 2: Convert the total time steaming into days and hours.  
 $316.13 \text{ hours} = 13.17 \text{ days} = 13 \text{ days, } 4 \text{ hours, } 5 \text{ minutes}.$
- Step 3: Convert departure times to GMT.  
 $0600 \text{ ZT } (-8); 22 \text{ October} = 2200 \text{ GMT; } 21 \text{ October}.$
- Step 4: Add transit time to converted departure time.  
 $2200 \text{ GMT; } 21 \text{ October} + 13 \text{ days, } 4 \text{ hours, } 5 \text{ minutes}$   
 $= 0205 \text{ GMT; } 4 \text{ November}$
- Step 5: Determine the arrival zone descriptor and account for daylight savings time (not necessary in this case).  
 $\text{Arrival longitude} = 118^{\circ} 11.0' \text{ W} = 118.183^{\circ}$   
 $118.183^{\circ} \div 15 = 7.87 = -8 \text{ ZD}$
- Step 6: Correct GMT arrival time to local time zone. It is easy and advisable to “backwards check” your work to ensure a correct answer.  
 $0205 \text{ GMT; } 4 \text{ November} = \mathbf{1805 \text{ ZT; } 3 \text{ November}}$

## Estimated Time of Arrival Problems

### ETA Problems with Delay

- ETA problems with stops (fueling, Panama Canal, etc.) are best accounted for by delaying the initial sailing time.

ETA D2. You are on a voyage from St. John's Canada, to Galveston, Texas. The distance is 2280 miles, and the speed of advance is 15.0 knots. You estimate 16.5 hours for bunkering en route at Ft. Lauderdale, Florida. If you sailed at 1642 hours (ZD +4) 27 February, what was your ETA (ZD +6) at Galveston?

Answer: 1512, 6 March.

- Step 1: Calculate the total time steaming:  
 $2280 \text{ nm} \div 15 \text{ knots} = 152 \text{ hours}.$
- Step 2: Convert the total time steaming into days and hours.  
 $152 \text{ hours} = 6.33 \text{ days} = 6 \text{ days}, 8 \text{ hours}.$
- Step 3: Convert departure time into GMT and account for "departure delay."  
 $1642 \text{ ZT (+4), 27 February} = 2042 \text{ GMT, 27 February}$   
  
 $16:30 \text{ hour delay for bunkering en route.}$   
 $2042 + 1630 = 36:72 = 12:72 + 1 \text{ day} = 13:12 \text{ GMT, 28 February}$   
 $\text{Modified departure time} = 1312 \text{ GMT, 28 February}$
- Step 4: Add transit time to converted departure time.  
 $1312 \text{ GMT, 28 February} + 6 \text{ days}, 8 \text{ hours}$   
 $= 2112 \text{ GMT, 6 March}$
- Step 5: Convert GMT arrival time into zone time (given as +6).  
 $2112 \text{ GMT, 6 March} = \mathbf{1512, 6 \text{ March ZT (+6).}}$



## Estimated Time of Arrival Problems

### Normal ETA Problems

ETA B1. At 0530 zone time on 20 December, you depart Cape Town (ZD -1). You are bound for New York (ZD +5) and you estimate your speed of advance at 25 knots. The distance is 6,762 miles. What is your estimated zone time of arrival in New York?

- a) 1200, 31 December
- b) 1100, 31 December
- c) 0700, 31 December
- d) 0600, 31 December - correct**

ETA B2. Your vessel departs Yokohama from position latitude  $35^{\circ} 27.0'$  N, longitude  $139^{\circ} 39.0'$  E (ZD -9) at 1330 ZT on 23 July. You are bound for Seattle at position latitude  $47^{\circ} 36.0'$  N, longitude  $122^{\circ} 22.0'$  W (ZD -8). The distance by great circle is 4,245 miles and you estimate that you will average 13.6 knots. What is your estimated ZT of arrival?

- a) 0438, 4 August
- b) 2038, 4 August - correct**
- c) 0438, 5 August
- d) 1238, 5 August

ETA B3. On 21 November at 2100 zone time, you depart latitude  $32^{\circ} 12'$  N, longitude  $69^{\circ} 26'$  W en-route to position latitude  $12^{\circ} 05'$  N, longitude  $7^{\circ} 32'$  W. The distance is 3,519 miles and the average speed will be 12.5 knots. What is the zone time of arrival?

- a) 1330, 3 December
- b) 1530, 3 December
- c) 1830, 3 December - correct**
- d) 1530, 4 December

ETA B4. At 0915 zone time on 7 April, you depart San Francisco, latitude  $37^{\circ} 48.5'$  N, longitude  $122^{\circ} 24.0'$  W (ZD -8). You are bound for Kobe, latitude  $34^{\circ} 40.0'$  N, longitude  $135^{\circ} 12.0'$  E. You estimate your speed of advance to be 17 knots. The distance is 4,819 miles. What is your estimated zone time of arrival at Kobe?

- a) 0343, 18 April
- b) 1243, 19 April
- c) 2143, 19 April - correct**
- d) 0443, 20 April

### ETA Problems with Delay

ETA B5. You are on a voyage from Baltimore, MD, to Seattle, WA. The distance from pilot to pilot is 5960 miles. The speed of advance is 16.0 knots. You estimate 16 hours for bunkering at Colon, and 12 hours for the Panama Canal transit. If you take departure at 0824 hours (ZD +5), 18 November, what is your ETA to Seattle (ZD +8)?

- a) 1654, 5 December
- b) 1354, 5 December
- c) 2154, 4 December - correct**
- d) 1354, 4 December

ETA B6. You are on a voyage from Boston, MA to South Pass, LA. The distance is 1870 miles and the speed of advance is 13.6 knots. You estimate 16.5 hours for bunkering in Port Everglades, FL. If you sailed at 0836 (ZD +5), 26 February, what is your ETA at South Pass (ZD +6)?

- a) 2336, 3 March
- b) 1136, 4 March
- c) 1236, 4 March
- d) 1736, 4 March - correct**

ETA B7. You are on a voyage from New York NY to San Francisco CA. The distance from pilot station to pilot station is 5132 miles and the speed of advance is 13.5 knots. You estimate 32 hours for bunkering at Colon and 14 hours for the Panama Canal transit. If you take departure at 0600 hours (ZD +4) on 16 May, what is your ETA at San Francisco (ZD +7)?

- a) 0609, 1 June
- b) 2109, 2 June - correct**
- c) 0009, 2 June
- d) 0409, 2 June

## **Speed by RPM Problems**



## Estimated Time of Arrival Problems

- Required formulas (these must be memorized).

- $Slip = \frac{Engine\ Speed - Observed\ Speed}{Engine\ Speed} \times 100$

- $Efficiency = 100\% - Slip$

- $Speed = \frac{RPM \times 60 \times Pitch \times Efficiency}{6080}$

- Pitch is the distance a propeller will move a ship forward in a fluid with one rotation. It is measured in feet.
- The number 6080 in the third equation comes from the fact that there are 6076 feet in a mile and is necessary because pitch is in terms of feet and necessary for units to cancel, resulting in nautical miles per hour. Generally the figure is rounded to 6080 to aid memorization.
- Revolutions per minute (RPM) is the number of turns a propeller (or shaft) makes in one minute.
- Slip is the difference between the speed of the engine and the speed of the ship. Slip values can be positive or negative and directly correlates to the efficiency of the system. For example, a following current could result in a negative slip, while a positive slip could come from hull fouling or mechanical issues. The “efficiency” figure in the third equation is usually used such that an efficiency of 107% would be noted as 1.07 and an efficiency of 97% would be noted as 0.97.

## Estimated Time of Arrival Problems

### Day's Run Problems

RPM D1. If the pitch of the propeller is 19.7 feet and the revolutions per day are 86,178, calculate the day's run allowing 3% negative slip.

Answer 287.60 nautical miles.

*Step 1: Efficiency = 100% – Slip*

*Step 2: Efficiency = 100% – (–3%)*

*Step 3: Efficiency = 103%*

*Step 4: Efficiency = 1.03*

*Step 5:* After calculating the efficiency, the next step is to calculate the required RPM of the shaft. Since the daily revolutions are given, the “60” in the Speed Equation is not necessary, and instead of “speed,” the answer will be given in “day's run.”

*Step 6: Speed =  $\frac{RPM \times 60 \times Pitch \times Efficiency}{6080}$*

*Step 7: Modified equation to → Day's Run =  $\frac{Revs \times Pitch \times Efficiency}{6080}$*

*Step 8: Day's Run =  $\frac{86,178 \times 19.7ft \times 1.03}{6080}$*

*Step 9: Day's Run =  $\frac{1,748,637.798}{6080}$*

*Step 10: Day's Run = 287.60 miles*

## Estimated Time of Arrival Problems

### Revolutions per Minute Problems

RPM D2. If the speed necessary for reaching port at a designated time is 18.5 knots and the pitch of the propeller is 21.7 feet, how many revolutions per minute will the shaft have to turn assuming a 4% negative slip?

Answer: 83.1 RPM.

Step 1:  $Efficiency = 100\% - Slip$

Step 2:  $Efficiency = 100\% - (-4\%)$

Step 3:  $Efficiency = 104\%$

Step 4:  $Efficiency = 1.04$

Step 5: After calculating the efficiency, the next step is to calculate the required RPM of the shaft.

Step 6:  $Speed = \frac{RPM \times 60 \times Pitch \times Efficiency}{6080}$

Step 7:  $18.5kts = \frac{RPM \times 60 \times 21.7ft \times 1.04}{6080}$

Step 8:  $18.5kts = \frac{RPM \times 1354.08}{6080}$

Step 9:  $112480 = RPM \times 1354.08$

Step 10:  **$RPM = 83.067$**

## Estimated Time of Arrival Problems

### Engine Slip Problems

RPM D3. While turning for 18.0 knots, accounting for current and wind, the ship is observed to make good 17.3 knots. What is the apparent slip of the propeller?

Answer: +3.88%. The reason for multiplying the fractional value by 100 is to obtain an answer in percent form, the standard form for slip calculations. Note that positive slip and negative slip values can occur.

$$\text{Step 1: } \text{Slip} = \frac{\text{Engine Speed} - \text{Observed Speed}}{\text{Engine Speed}} \times 100$$

$$\text{Step 2: } \text{Slip} = \frac{18.0\text{kts} - 17.3\text{kts}}{18.0\text{kts}} \times 100$$

$$\text{Step 3: } \text{Slip} = \frac{0.7\text{kts}}{18.0\text{kts}} \times 100$$

$$\text{Step 4: } \text{Slip} = 0.0388 \times 100 = +\mathbf{3.88\%}$$

RPM D4. The propeller on a vessel has a diameter of 20.6 feet and a pitch of 23.4 feet. What would be the apparent slip if the vessel cruised 538 miles in a 24-hour day (observed distance) at an average RPM of 87?

Answer: -11.59%. The propeller diameter is “distractor” information. The goal is to calculate slip, so the “efficiency” portion of the speed equation is not required.

$$\text{Step 1: } \text{Speed} = \frac{\text{RPM} \times 60 \times \text{Pitch} \times \text{Efficiency}}{6080}$$

$$\text{Step 2: } \text{Speed} = \frac{87\text{RPM} \times 60 \times 23.4\text{ft} \times \text{Efficiency (irrelevant in this case)}}{6080}$$

$$\text{Step 3: } \text{Speed} = \frac{122148}{6080} = 20.09 \text{ knots}$$

Step 4: This gives us our engine speed for the next calculation. In the problem, the vessel cruised 538 miles in a 24-hour day. Therefore, from a basic speed=distance/time calculation, the observed speed is 22.42kts.

$$\text{Step 5: } \text{Slip} = \frac{\text{Engine Speed} - \text{Observed Speed}}{\text{Engine Speed}} \times 100$$

$$\text{Step 6: } \text{Slip} = \frac{20.09\text{kts} - 22.42\text{kts}}{20.09\text{kts}} \times 100$$

$$\text{Step 7: } \text{Slip} = \frac{-2.23\text{kts}}{20.09\text{kts}} \times 100$$

$$\text{Step 8: } \text{Slip} = -0.1159 \times 100 = -\mathbf{11.59\%}$$



## Estimated Time of Arrival Problems

### Speed Problems

RPM D5. You are turning for 90 RPM. The propeller pitch is 24 feet and the slip is -3%. What is the speed of advance?

Answer: 21.9 knots.

Step 1:  $Efficiency = 100\% - Slip$

Step 2:  $Efficiency = 100\% - (-3\%)$

Step 3:  $Efficiency = 103\% = 1.03$

Step 4:  $Speed = \frac{RPM \times 60 \times Pitch \times Efficiency}{6080}$

Step 5:  $Speed = \frac{90RPM \times 60 \times 24ft \times 1.03}{6080}$

Step 6:  $Speed = \frac{133488}{6080} = \mathbf{21.96 \text{ knots}}$

## Speed by RPM Problems

### Day's Run Problems

RPM B1. If the pitch of the propeller is 19.4 feet, and the revolutions per day are 96,713, calculate the day's run allowing 6% positive slip.

- a) 266.4 miles
- b) 290.1 miles - correct**
- c) 308.6 miles
- d) 327.1 miles

RPM B2. If the pitch of the propeller is 21.5 feet, and the revolutions per day are 96,666, calculate the day's run allowing 9% negative slip.

- a) 311.1 miles
- b) 341.8 miles
- c) 357.9 miles
- d) 372.6 miles - correct**

RPM B3. If the pitch of the propeller is 25.1 feet, and the revolutions per day are 91,591, calculate the day's run allowing 7 % positive slip.

- a) 351.6 miles - correct**
- b) 378.1 miles
- c) 390.0 miles
- d) 404.6 miles

### Revolutions per Minute Problems

RPM B4. If the speed necessary for reaching port at a designated time is 12.6 knots and the pitch of the propeller is 13.6 feet, how many revolutions per minute will the shaft have to turn, assuming no slip?

- a) 81
- b) 85
- c) 90
- d) 94 - correct**

RPM B5. If the speed necessary for reaching port at a designated time is 15.7 knots and the pitch of the propeller is 23.4 feet, how many revolutions per minute will the shaft have to turn, assuming a 6% negative slip?

- a) 64 - correct**
- b) 68
- c) 72
- d) 76

RPM B6. If the speed necessary for reaching port at a designated time is 17.8 knots and the pitch of the propeller is 24.7 feet, how many revolutions per minute will the shaft have to turn, assuming a 7% positive slip?

- a) 67
- b) 71
- c) 75
- d) 79 - correct**

RPM B7. If the speed necessary for reaching port at a designated time is 20.7 knots and the pitch of the propeller is 23.8 feet, how many revolutions per minute will the shaft have to turn, assuming a 3% negative slip?

- a) 74
- b) 79
- c) 86 - correct**
- d) 98

### Slip Problems

RPM B8. The propeller of a vessel has a pitch of 19.0 feet. If the vessel traveled 183.5 miles (observed distance) in 24 hours at an average of 44 RPM, what was the slip?

- a) **+7.4% - correct**
- b) -7.4%
- c) +11.6%
- d) -11.6%

RPM B8. The propeller on a vessel has a diameter of 20.2 feet and a pitch of 19.0 feet. What would be the apparent slip if the vessel cruised 367 miles (observed distance) in a 24-hour day at an average RPM of 84?

- a) **+2.9% - correct**
- b) -2.9%
- c) +5.2%
- d) -5.2%

RPM B9. The pitch of the propeller on your vessel is 19' 09". You estimate slip to be -3%. If you averaged 82 RPM for the day's run, how many miles did you steam?

- a) 370.8
- b) 373.6
- c) 393.7
- d) **395.3 - correct**

RPM B10. The propeller on a vessel has a diameter of 24.0 feet and a pitch of 21.3 feet. What would be the slip if the vessel cruised 510 miles in a 24 hour day (observed distance) at an average RPM of 86?

- a) -12.2%
- b) +12.2%
- c) **-17.5% - correct**
- d) +17.5%

RPM B11. Your vessel's propeller has a pitch of 22'06". From 0530, 19 March, to 1930, 20 March, the average RPM was 82. The distance run by observation was 721.5 miles. What was the slip?

- a) +4%
- b) **-4% - correct**
- c) +7%
- d) -7%

### Speed Problems

RPM B12. The speed of advance necessary to reach port at a designated time is 15.8 knots. The pitch of the propeller is 20.75 feet. You estimate positive 5% slip. How many RPM must you turn to make the necessary speed?

- a) 73.5
- b) 76.2
- c) 79.9
- d) **81.2 - correct**

RPM B13. You are turning 100 RPM, with a propeller pitch of 25 feet, and an estimated slip of -5%. What is the speed of advance?

- a) 24.7 kts
- b) 23.5 kts
- c) **25.9 kts - correct**
- d) 22.3 kts

RPM B14. You are turning 82 RPM, with a propeller pitch of 23 feet, and an estimated slip of +6%. What is the speed of advance?

- a) **17.5 kts - correct**
- b) 17.9 kts
- c) 18.4 kts
- d) 19.7 kts



## **Fuel Conservation Problems**





## Fuel Conservation Problems

- Fuel conservation problems may appear in several formats, but they all rely on the same two formulae:

- $$\frac{\text{New Consumption}}{\text{Old Consumption}} = \frac{\text{New Speed}^3}{\text{Old Speed}^3}$$

- $$\frac{\text{New Consumption}}{\text{Old Consumption}} = \frac{\text{New Speed}^2 \times \text{New Distance}}{\text{Old Speed}^2 \times \text{Old Distance}}$$

- Depending on the information given in the problem, sometimes the formula should be modified by setting values to “1”. For example, if no consumption information is given, it is assumed the consumption stays the same and can be set to 1/1. Proceed as normal with the formula from there.

## Fuel Conservation Problems

### Desired Speed (Change Consumption)

CON D1. While steaming 17.5 knots, your vessel consumes 378 barrels of fuel oil per day. In order to reduce consumption to 194 barrels of fuel oil per day, what is the maximum speed the vessel can turn for?

Answer: 14.01 knots. Use equation (1) to solve for the new speed required.

$$\text{Step 1: } \frac{\text{New Consumption}}{\text{Old Consumption}} = \frac{\text{New Speed}^3}{\text{Old Speed}^3}$$

$$\text{Step 2: } \frac{194 \text{ barrels per day}}{378 \text{ barrels per day}} = \frac{\text{New Speed}^3}{(17.5 \text{ kts})^3}$$

$$\text{Step 3: } 0.5132 = \frac{\text{New Speed}^3}{5359.4}$$

$$\text{Step 4: } 2750.4 = \text{New Speed}^3$$

$$\text{Step 5: } \mathbf{14.01 \text{ kts} = \text{New Speed}}$$

### Desired Speed (Remaining Fuel)

CON D2. You have steamed 369 miles at 16 knots and burned 326 barrels of fuel per day. You must decrease your consumption to 212 barrels per day with 271 miles left in your voyage. What must you reduce your speed to in order to burn this amount of fuel?

Answer: 15.1 knots

$$\text{Step 1: } \frac{\text{New Consumption}}{\text{Old Consumption}} = \frac{\text{New Speed}^2 \times \text{New Distance}}{\text{Old Speed}^2 \times \text{Old Distance}}$$

$$\text{Step 2: } \frac{212}{326} = \frac{x^2 \times 271}{16^2 \times 369}$$

$$\text{Step 3: } 0.6503 = \frac{271x^2}{94464}$$

$$\text{Step 4: } 61429.9 = 271x^2$$

$$\text{Step 5: } 226.7 = x^2$$

$$\text{Step 6: } \mathbf{\text{New speed} = 15.06 \text{ knots}}$$

## Fuel Conservation Problems

### Desired Speed (Given Distance)

CON D3. At your current speed of 22 knots you have only enough fuel remaining to travel 440 miles. You must travel 618 miles to reach your destination. What speed should you reduce to in order to reach your destination?

Answer: 18.6 knots. If the consumption is not stated to change in the problem, you can set the value to 1/1 as a constant.

$$\text{Step 1: } \frac{\text{New Consumption}}{\text{Old Consumption}} = \frac{\text{New Speed}^2 \times \text{New Distance}}{\text{Old Speed}^2 \times \text{Old Distance}}$$

$$\text{Step 2: } \frac{1}{1} = \frac{x^2 \times 618}{22^2 \times 440}$$

$$\text{Step 3: } 1 = \frac{618x^2}{212960}$$

$$\text{Step 4: } 212960 = 618x^2$$

$$\text{Step 5: } 344.6 = x^2$$

$$\text{Step 6: } \text{New speed} = 18.6 \text{ knots}$$

### Desired New Consumption (Change Speed)

CON D4. While steaming 14.0 knots, your vessel burns 276 barrels per day. What will be the rate of fuel consumption if you decrease speed to 11.7 knots?

Answer: 161.1 barrels per day

$$\text{Step 1: } \frac{\text{New Consumption}}{\text{Old Consumption}} = \frac{\text{New Speed}^3}{\text{Old Speed}^3}$$

$$\text{Step 2: } \frac{\text{New Consumption}}{276 \text{ barrels per day}} = \frac{(11.7 \text{ kts})^3}{(14.0 \text{ kts})^3}$$

$$\text{Step 3: } \frac{\text{New Consumption}}{276 \text{ barrels per day}} = \frac{1601.613}{2744}$$

$$\text{Step 4: } \frac{\text{New Consumption}}{276 \text{ barrels per day}} = 0.5837$$

$$\text{Step 5: } \text{New Consumption} = 161.1 \text{ barrels per day}$$

## Fuel Conservation Problems

### Desired New Consumption (Remaining Distance)

CON D5. You have steamed 174 miles and consumed 18.0 tons of fuel. If you maintain the same speed, how many tons of fuel will you consume while steaming 416 miles?

Answer: 43.03 tons. Since the speed is to remain the same, you can cancel the terms from the numerator and denominator.

$$\text{Step 1: } \frac{\text{New Consumption}}{\text{Old Consumption}} = \frac{\text{New Speed}^2 \times \text{New Distance}}{\text{Old Speed}^2 \times \text{Old Distance}}$$

$$\text{Step 2: } \frac{\text{New Consumption}}{18.0 \text{ tons per day}} = \frac{\text{Irrelevant Speed}^2 \times 416 \text{ miles}}{\text{Irrelevant Speed}^2 \times 174 \text{ miles}}$$

Step 3: Cancel the speed terms from the numerator and denominator.

$$\text{Step 4: } \frac{\text{New Consumption}}{18.0 \text{ tons per day}} = \frac{416 \text{ miles}}{174 \text{ miles}}$$

$$\text{Step 5: } \frac{\text{New Consumption}}{18.0 \text{ tons per day}} = 2.3908$$

**Step 6: New Consumption = 43.03 tons**

### Desired New Distance

CON D6. You have steamed 607 miles at 17.0 knots and consumed 121 tons of fuel. If you have 479 tons of usable fuel remaining, how far can you steam at 14.5 knots?

Answer: 3302.9 miles

$$\text{Step 1: } \frac{\text{New Consumption}}{\text{Old Consumption}} = \frac{\text{New Speed}^2 \times \text{New Distance}}{\text{Old Speed}^2 \times \text{Old Distance}}$$

$$\text{Step 2: } \frac{479}{121} = \frac{14.5^2 \times x}{17^2 \times 607}$$

$$\text{Step 3: } 3.959 = \frac{210.25 x}{175423}$$

$$\text{Step 4: } 694443 = 210.25x$$

**Step 5: New distance = 3247 miles**

## Fuel Conservation Problems

### Desired Speed (Change Consumption)

CON B1. While steaming 13.5 knots, your vessel consumes 251 barrels of fuel oil per day. In order to reduce consumption to 129 barrels of fuel oil per day, what is the maximum speed the vessel can turn for?

- a) 6.9 kts
- b) 9.7 kts
- c) 10.8 kts - correct
- d) 12.7 kts

CON B2. While steaming at 14.5 knots, your vessel consumes 319 barrels of fuel oil per day. In order to reduce consumption to 217 barrels of fuel oil per day, what is the maximum speed the vessel can turn for?

- a) 9.8 kts
- b) 11.9 kts
- c) 12.8 kts - correct
- d) 13.5 kts

CON B3. While steaming at 15.5 knots, your vessel consumes 333 barrels of fuel oil per day. In order to reduce consumption to 176 barrels of fuel oil per day, what is the maximum speed the vessel can turn for?

- a) 11.3 kts
- b) 12.5 kts - correct
- c) 13.6 kts
- d) 14.8 kts

Desired Speed (Remaining Fuel)

CON B4. You have steamed 449 miles at 19 knots and burning 476 barrels of fuel per day. You must decrease your consumption to 185 barrels per day with 362 miles left in your voyage.

What must you reduce your speed (kts) to in order to burn this amount of fuel?

- a) 13.2 kts - correct
- b) 14.3 kts
- c) 17.1 kts
- d) 18.2 kts

CON B5. You have steamed 499 miles at 21 knots and burning 462 barrels of fuel per day. You must decrease your consumption to 221 barrels per day with 311 miles left in your voyage.

What must you reduce your speed (kts) to in order to burn this amount of fuel?

- a) 17.3 kts
- b) 18.4 kts - correct
- c) 19.1 kts
- d) 20.0 kts

CON B6. At your current speed of 21 knots you only have sufficient fuel to travel 404 miles. You must travel 731 miles to reach your destination. What speed should you travel in order to reach your destination?

- a) 18.9 kts
- b) 17.8 kts
- c) 16.7 kts
- d) 15.6 kts - correct

Desired Speed (Given Distance)

CON B7. Your vessel arrives in port with sufficient fuel to steam 812 miles at 15 knots. If you are unable to take on bunkers at what speed must you proceed to reach your destination, 928 miles distant?

- a) 13.6 kts
- b) 14.0 kts - correct
- c) 15.3 kts
- d) 15.7 kts

CON B8. Your vessel arrives in port with sufficient fuel to steam 726 miles at 16 knots. If you are unable to take on bunkers at what speed must you proceed to reach your destination, 873 miles distant?

- a) 14.6 kts - correct
- b) 15.1 kts
- c) 16.3 kts
- d) 16.8 kts

CON B9. At your current speed of 21 knots you have only enough fuel remaining to travel 404 miles. You must travel 731 miles to reach your destination. What should you reduce your speed to in order to reach your destination?

- a) 18.9 kts
- b) 17.8 kts
- c) 16.7 kts
- d) 15.6 kts – correct

CON B10. At your current speed of 22 knots you have only enough fuel remaining to travel 422 miles. You must travel 844 miles to reach your destination. What should you reduce your speed to in order to reach your destination?

- a) 19.8 kts
- b) 18.4 kts
- c) 17.0 kts
- d) 15.6 kts – correct

Desired New Consumption (Change Speed)

CON B11. Your vessel consumes 274 barrels of fuel per day at a speed of 17.5 knots. What will the fuel consumption be at 13.5 knots?

- a) 126 bbls - correct
- b) 163 bbls
- c) 211 bbls
- d) 253 bbls

CON B12. Your vessel consumes 156 barrels of fuel per day at a speed of 13 knots. What will the fuel consumption be of your vessel at 16 knots?

- a) 192 bbls
- b) 236 bbls
- c) 291 bbls - correct
- d) 315 bbls

CON B13. Your vessel consumes 216 barrels of fuel per day at a speed of 15 knots. What will the fuel consumption be of your vessel at 17.5 knots?

- a) 232 bbls
- b) 252 bbls
- c) 294 bbls
- d) 343 bbls - correct



Desired New Consumption (Remaining Distance)

CON B14. You have steamed 300 miles and consumed 34 tons of fuel. If you maintain the same speed, how many tons of fuel will you consume while steaming 700 miles?

- a) 79.3 tons - correct
- b) 74.3 tons
- c) 68.4 tons
- d) 66.2 tons

CON B15. You have steamed 199 miles and consumed 23 tons of fuel. If you maintain the same speed, how many tons of fuel will you consume while steaming 410 miles?

- a) 32.6 tons
- b) 39.9 tons
- c) 47.4 tons - correct
- d) 97.6 tons

CON B16. You have steamed 916 miles at 13 knots and consumed 166 tons of fuel. If you have to steam 1325 miles to complete the voyage, how many tons of fuel will be consumed while steaming at 14 knots?

- a) 133 tons
- b) 181 tons
- c) 207 tons
- d) 278 tons - correct

CON B17. You have steamed 1175 miles at 19 knots and consumed 257 tons of fuel. If you have to steam 1341 miles to complete the voyage, how many tons of fuel will be consumed while steaming at 18 knots?

- a) 293 tons
- b) 263 tons - correct
- c) 202 tons
- d) 172 tons

### Desired New Distance

CON B18. You have steamed 1124 miles at 21 knots and consumed 326 tons of fuel. If you have 210 tons of usable fuel remaining, how far can you steam at 17 knots?

- a) 1096 miles
- b) 1105 miles - correct
- c) 1218 miles
- d) 1304 miles

CON B19. You have steamed 525 miles at 16 knots and consumed 105 tons of fuel. If you have 308 tons of usable fuel remaining, how far can you steam at 19 knots?

- a) 920 miles
- b) 1092 miles - correct
- c) 1297 miles
- d) 2172 miles

CON B20. You have steamed 918 miles at 15 knots. The total fuel consumed is 183 tons. If you have 200 tons of fuel remaining how far can you steam at 12 knots?

- a) 1021 miles
- b) 1261 miles
- c) 1568 miles - correct
- d) 1960 miles

CON B21. You have steamed 701 miles at 18 knots. The total fuel consumed is 201 tons. If you have 259 tons of fuel remaining how far can you steam at 14.5 knots?

- a) 838 miles
- b) 903 miles
- c) 1392 miles - correct
- d) 1728 miles

CON B22. You have steamed 632 miles at 18.5 knots. The total fuel consumed is 197 tons. If you have 278 tons of fuel remaining how far can you steam at 15 knots?

- a) 681 miles
- b) 892 miles
- c) 1100 miles
- d) 1357 miles - correct

## **Distance Off, Bearing, & Dead Reckoning Problems**



## Distance Off, Bearing, and Dead Reckoning Problems

- Distance off problems can either involve distance when abeam or distance at second bearing. Table 7 in Bowditch provides tabulated results for most cases.
- There are some special case rules to know that may save time during an exam. The most common cases are the 7/10<sup>th</sup>'s rule and the 26.5° - 45° rule:
  - Doubling the Angle on the Bow Rule: when the measured angle of an object doubles, the distance run between the bearings equals the distance from the object at the second bearing.
  - Bow and Beam Rule: When the first bearing is 45° and the second is 90°, the distance run between bearings and distance off are equal.
  - 7/10<sup>th</sup> Rule: When the first bearing is 22.5° and the second is 45°, 0.7 times the distance run equals the distance abeam.
  - 26.5° - 45° Rule: When the first bearing is 26.5° and the second bearing is 45° the distance run equals the distance abeam.
  - 30/60/90 Rule: When the first bearing is 30° and the second is 60°, 0.875 times the distance run equals the distance abeam.
- Some problems are best solved with a Maneuvering Board, such as those involving a course to steer, time abeam a light, or those requiring a course change.

## Distance Off, Bearing, and Dead Reckoning Problems

DIS D1. You are steaming on a course of  $114^{\circ}$  T at 17 knots. At 1122 you observe a lighthouse bearing  $077^{\circ}$  T. At 1133 the lighthouse bears  $051^{\circ}$  T. What is your distance off at the second bearing? What is your distance off when abeam?

Answer: 4.31 miles at second bearing, 3.84 miles when abeam.

Step 1: Create a table of data to determine the difference between ship's course and each bearing.

| Time | Course          | Bearing         | Difference between course and bearing            |
|------|-----------------|-----------------|--------------------------------------------------|
| 1122 | $114^{\circ}$ T | $077^{\circ}$ T | $114^{\circ}$ T – $077^{\circ}$ T = $37^{\circ}$ |
| 1133 | $114^{\circ}$ T | $051^{\circ}$ T | $114^{\circ}$ T – $051^{\circ}$ T = $63^{\circ}$ |

Step 2: Enter Table 7 in Bowditch with the difference between the course and each bearing. Retrieve the tabular data, with bracketing values if exact values are not listed.

a. The bracketing values are:

|              | $36^{\circ}$ | $38^{\circ}$ |
|--------------|--------------|--------------|
| $62^{\circ}$ | 1.34/1.18    | 1.51/1.34    |
| $64^{\circ}$ | 1.25/1.13    | 1.40/1.26    |

b. Interpolate for the desired value to the nearest hundredth.

| Distance of an Object by Two Bearings                          |                                                 |      |              |      |              |      |              |      |              |      |  |
|----------------------------------------------------------------|-------------------------------------------------|------|--------------|------|--------------|------|--------------|------|--------------|------|--|
| Difference between the course and second bearing<br>$^{\circ}$ | Difference between the course and first bearing |      |              |      |              |      |              |      |              |      |  |
|                                                                | $34^{\circ}$                                    |      | $36^{\circ}$ |      | $38^{\circ}$ |      | $40^{\circ}$ |      | $42^{\circ}$ |      |  |
| 44                                                             | 3.22                                            | 2.24 |              |      |              |      |              |      |              |      |  |
| 46                                                             | 2.69                                            | 1.93 | 3.39         | 2.43 |              |      |              |      |              |      |  |
| 48                                                             | 2.31                                            | 1.72 | 2.83         | 2.10 | 3.55         | 2.63 |              |      |              |      |  |
| 50                                                             | 2.03                                            | 1.55 | 2.43         | 1.86 | 2.96         | 2.27 | 3.70         | 2.84 |              |      |  |
| 52                                                             | 1.81                                            | 1.43 | 2.13         | 1.68 | 2.54         | 2.01 | 3.09         | 2.44 | 3.85         | 3.04 |  |
| 54                                                             | 1.63                                            | 1.32 | 1.90         | 1.54 | 2.23         | 1.81 | 2.66         | 2.15 | 3.22         | 2.60 |  |
| 56                                                             | 1.49                                            | 1.24 | 1.72         | 1.42 | 1.99         | 1.65 | 2.33         | 1.93 | 2.77         | 2.29 |  |
| 58                                                             | 1.37                                            | 1.17 | 1.57         | 1.33 | 1.80         | 1.53 | 2.08         | 1.76 | 2.43         | 2.06 |  |
| 60                                                             | 1.28                                            | 1.10 | 1.45         | 1.25 | 1.64         | 1.42 | 1.88         | 1.63 | 2.17         | 1.88 |  |
| 62                                                             | 1.19                                            | 1.05 | 1.34         | 1.18 | 1.51         | 1.34 | 1.72         | 1.52 | 1.96         | 1.73 |  |
| 64                                                             | 1.12                                            | 1.01 | 1.25         | 1.13 | 1.40         | 1.26 | 1.58         | 1.42 | 1.79         | 1.61 |  |
| 66                                                             | 1.06                                            | 0.96 | 1.18         | 1.07 | 1.31         | 1.20 | 1.47         | 1.34 | 1.65         | 1.51 |  |
| 68                                                             | 1.00                                            | 0.93 | 1.11         | 1.03 | 1.23         | 1.14 | 1.37         | 1.27 | 1.53         | 1.42 |  |

|              | $36^{\circ}$     | $37^{\circ}$ | $38^{\circ}$     |
|--------------|------------------|--------------|------------------|
| $62^{\circ}$ | 1.34/1.18        |              | 1.51/1.34        |
| $63^{\circ}$ | <b>1.30/1.16</b> | ?            | <b>1.46/1.30</b> |
| $64^{\circ}$ | 1.25/1.13        |              | 1.40/1.26        |

|              | $36^{\circ}$ | $37^{\circ}$     | $38^{\circ}$ |
|--------------|--------------|------------------|--------------|
| $62^{\circ}$ | 1.34/1.18    |                  | 1.51/1.34    |
| $63^{\circ}$ | 1.30/1.16    | <b>1.38/1.23</b> | 1.46/1.30    |
| $64^{\circ}$ | 1.25/1.13    |                  | 1.40/1.26    |

The interpolated values for  $37^{\circ}$  and  $63^{\circ}$  are 1.38 and 1.23.

## Distance Off, Bearing, and Dead Reckoning Problems

Step 3: Given the time between bearings and the ship speed, determine the distance run.  
Bearing times: 1122 and 1133.  $1133 - 1122 = 11$  minutes run.  
 $11$  minutes =  $0.183$  hours at  $17$  knots =  $3.12$  miles run.

Step 4: Per the instructions in Bowditch for using Table 7, the distance run between bearings multiplied by the first number is equal to the distance at the second bearing, and the distance run multiplied by the second number is equal to the distance abeam.

Distance off at second bearing =  $3.12$  miles run  $\times 1.38 = \mathbf{4.31 \text{ miles}}$

Distance off abeam =  $3.12$  miles run  $\times 1.23 = \mathbf{3.84 \text{ miles}}$

## Distance Off, Bearing, and Dead Reckoning Problems

DIS D2. Your vessel is on course  $237^{\circ}$  T at 18 knots. At 0404 a light bears  $263.5^{\circ}$  T and at 0430 the light bears  $282^{\circ}$  T. At what time and at what distance off will your vessel be when abeam of the light?

Answer: 0456, 7.8 miles.

Step 1: Create a table of data to determine the difference between ship's course and each bearing.

| Time | Course          | Bearing           | Difference between course and bearing                                  |
|------|-----------------|-------------------|------------------------------------------------------------------------|
| 0404 | $237^{\circ}$ T | $263.5^{\circ}$ T | $237^{\circ}$ T – $263.5^{\circ}$ T = <b><math>26.5^{\circ}</math></b> |
| 0430 | $237^{\circ}$ T | $282^{\circ}$ T   | $237^{\circ}$ T – $282^{\circ}$ T = <b><math>45^{\circ}</math></b>     |

Step 2: Because the first bearing is  $26.5^{\circ}$  and the second bearing is  $45^{\circ}$ , this is a special case rule which states that the distance run is equal to the distance abeam.

Step 3: Given the time between bearings and the ship speed, determine the distance run. Bearing times: 0404 and 0430.  $0430 - 0404 = 26$  minutes run.  
 $26$  minutes =  $0.433$  hours at 18 knots = 7.8 miles run.

Step 4: Since the distance run is 7.8 miles, the distance abeam is also **7.8 miles**.

Step 5: When determining the time abeam, since the second bearing is  $45^{\circ}$  and the bearing abeam is  $90^{\circ}$ , the bow and beam rule states that the distance run between bearings and the distance abeam are the same.

- Since we know the distance abeam is 7.8 miles, this also equals the distance run from 0430 until the time abeam.
- Since the time between 0404 and 0430, and the time between 0430 and the time abeam will be the same, the time from 0430 to time abeam will be equal to 26 minutes. Therefore, the time abeam is  $0430 + 26 = \mathbf{0456}$ .



## Distance Off, Bearing, and Dead Reckoning Problems

DIS D2A. Note this problem can also be solved using Table 7 in Bowditch if the special case is not recognized.

Resuming from step 1:

- Step 1: Create a table of data to determine the difference between ship's course and each bearing.

| Time | Course | Bearing  | Difference between course and bearing                      |
|------|--------|----------|------------------------------------------------------------|
| 0404 | 237° T | 263.5° T | $237^\circ \text{ T} - 263.5^\circ \text{ T} = 26.5^\circ$ |
| 0430 | 237° T | 282° T   | $237^\circ \text{ T} - 282^\circ \text{ T} = 45^\circ$     |

- Step 2: Enter Table 7 in Bowditch with the difference between the course and each bearing. Retrieve the tabular data, with bracketing values if exact values are not listed (Table 18 is reproduced in it's entirety at the end of this Part).

| Difference between the course and second bearing<br>° | Difference between the course and first bearing |      |      |      |      |      |      |      |      |      |
|-------------------------------------------------------|-------------------------------------------------|------|------|------|------|------|------|------|------|------|
|                                                       | 20°                                             |      | 22°  |      | 24°  |      | 26°  |      | 28°  |      |
| 30                                                    | 1.97                                            | 0.98 |      |      |      |      |      |      |      |      |
| 32                                                    | 1.64                                            | 0.87 | 2.16 | 1.14 |      |      |      |      |      |      |
| 34                                                    | 1.41                                            | 0.79 | 1.80 | 1.01 | 2.34 | 1.31 |      |      |      |      |
| 36                                                    | 1.24                                            | 0.73 | 1.55 | 0.91 | 1.96 | 1.15 | 2.52 | 1.48 |      |      |
| 38                                                    | 1.11                                            | 0.68 | 1.36 | 0.84 | 1.68 | 1.04 | 2.11 | 1.30 | 2.70 | 1.66 |
| 40                                                    | 1.00                                            | 0.64 | 1.21 | 0.78 | 1.48 | 0.95 | 1.81 | 1.16 | 2.26 | 1.45 |
| 42                                                    | 0.91                                            | 0.61 | 1.10 | 0.73 | 1.32 | 0.88 | 1.59 | 1.06 | 1.94 | 1.30 |
| 44                                                    | 0.84                                            | 0.58 | 1.00 | 0.69 | 1.19 | 0.83 | 1.42 | 0.98 | 1.70 | 1.18 |
| 46                                                    | 0.78                                            | 0.56 | 0.92 | 0.66 | 1.09 | 0.78 | 1.28 | 0.92 | 1.52 | 1.09 |
| 48                                                    | 0.73                                            | 0.54 | 0.85 | 0.64 | 1.00 | 0.74 | 1.17 | 0.87 | 1.37 | 1.02 |

- a. The bracketing values are:

|     | 26°       | 28°       |
|-----|-----------|-----------|
| 44° | 1.42/0.98 | 1.70/1.18 |
| 46° | 1.28/0.92 | 1.52/1.09 |

- b. Interpolate for the desired value to the nearest hundredth.

|     | 26°       | 26.5° | 28°       |
|-----|-----------|-------|-----------|
| 44° | 1.42/0.98 |       | 1.70/1.18 |
| 45° | 1.35/0.95 |       | 1.61/1.14 |
| 46° | 1.28/0.92 |       | 1.52/1.09 |

|     | 26°       | 26.5°     | 28°       |
|-----|-----------|-----------|-----------|
| 44° | 1.42/0.98 |           | 1.70/1.18 |
| 45° | 1.35/0.95 | 1.42/1.00 | 1.61/1.14 |
| 46° | 1.28/0.92 |           | 1.52/1.09 |

The interpolated values for 26.5° and 45° are 1.42 and 1.00.

## Distance Off, Bearing, and Dead Reckoning Problems

Step 3: Given the time between bearings and the ship speed, determine the distance run.  
Bearing times: 0404 and 0430.  $0430 - 0404 = 26$  minutes run.  
 $26 \text{ minutes} = 0.433 \text{ hours at } 18 \text{ knots} = 7.8 \text{ miles run.}$

Step 4: Per the instructions in Bowditch for using Table 7, the distance run between bearings multiplied by the first number is equal to the distance at the second bearing, and the distance run multiplied by the second number is equal to the distance abeam.

Distance off at second bearing =  $7.8 \text{ miles run} \times 1.42 = 11.08 \text{ miles}$   
Distance off abeam =  $7.8 \text{ miles run} \times 1.00 = \mathbf{7.8 \text{ miles}}$

Step 5: Determine the time abeam.

The distance abeam was determined to be 7.8 miles in step 4.

With one bearing at  $45^\circ$  (the original, second bearing), and one bearing at  $90^\circ$  (abeam), this is a 45-45-90 right triangle, and therefore the distance run from the second bearing to the beam bearing and distance abeam are equal, so the distance run is 7.8 miles.

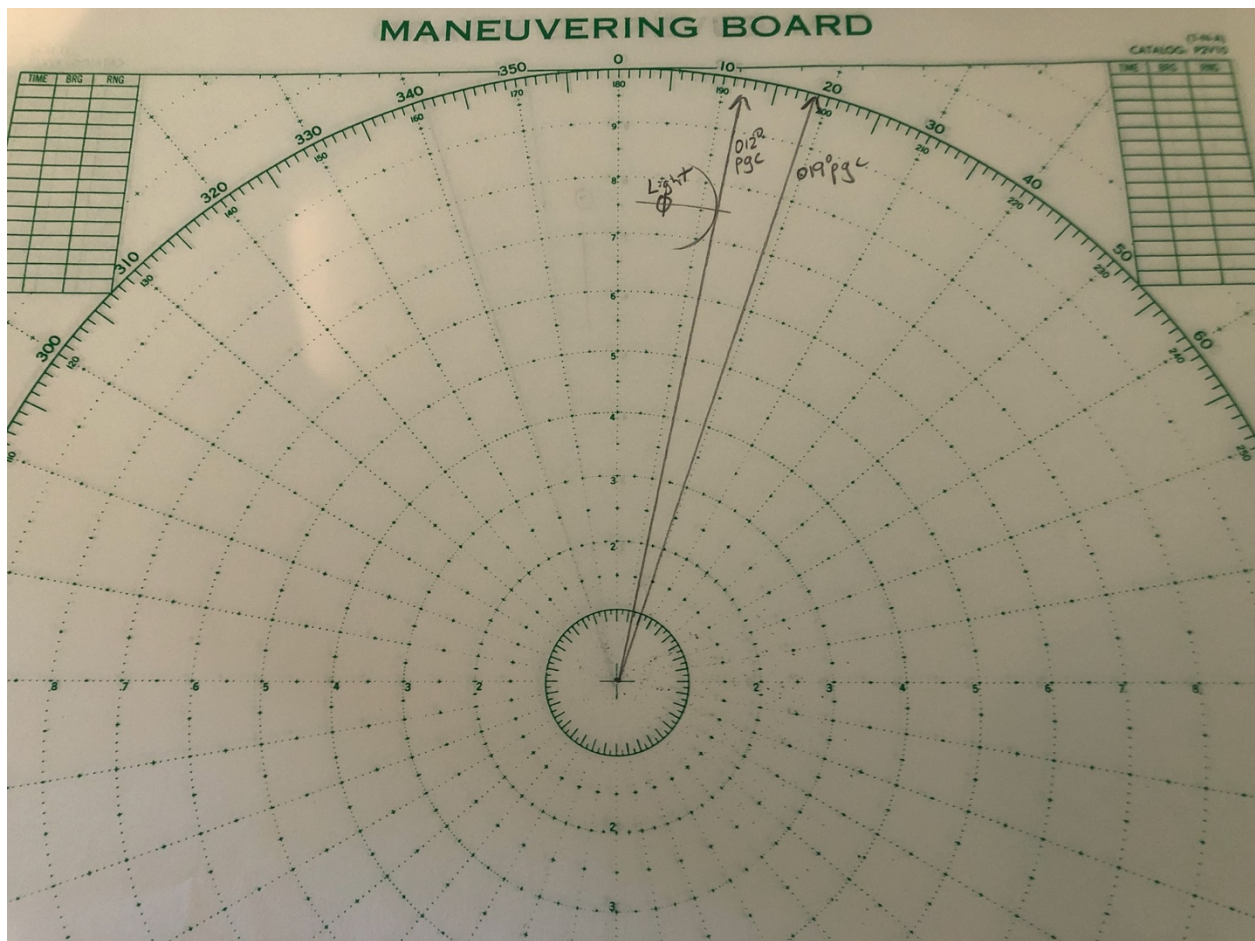
7.8 miles for 18 knots is 0.433 hours, or 26 minutes. The time of second bearing was 0430.  $0430 + 26\text{m} = \mathbf{0456.}$

## Distance Off, Bearing, and Dead Reckoning Problems

DIS 3. While on course  $091^{\circ}$  pgc, a light bears  $014^{\circ}$  off the port bow at a distance of 15.3 miles. What course should you steer to pass 1.5 miles abeam of the light, leaving it to port?

Answer:  $012^{\circ}$  pgc

- Step 1: Plot the initial course on a Maneuvering Board.
- Step 2: Plot the bearing and range to the light.
- Step 3: Plot a circle of 1.5 miles around the light.
- Step 4: Determine the course to steer with a tangent to the circle drawn in step 3.



## Distance Off, Bearing, and Dead Reckoning Problems

DIS 4. You are steering  $231^{\circ}$  T and a light is picked up dead ahead at a distance of 12.3 miles at 0338. You change course to pass the light 4 miles off abeam to starboard. If you are making 16.5 knots, what is your ETA at the position 4 miles off the light?

Answer: 0420

Step 1: Plot the initial course on a Maneuvering Board.

Step 2: Plot the bearing and range to the light.

Step 3: Plot a circle of 4 miles around the light.

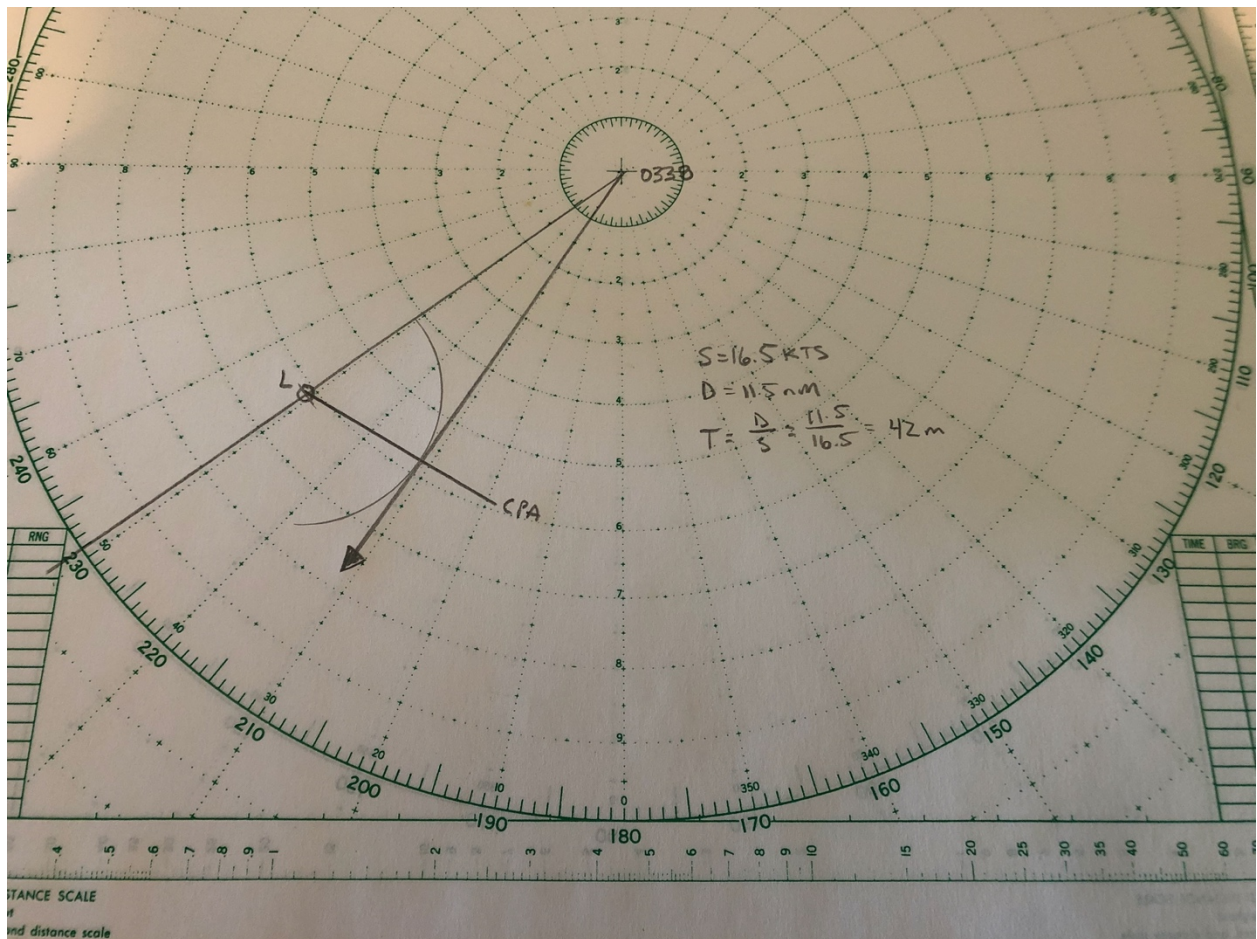
Step 4: Determine the time abeam:

Draw a tangent line from the light to the course and mark it as the CPA.

Measure the distance from the origin to the CPA.

Time =  $D/S = 11.5\text{nm}/16.5\text{kts} = 42$  minutes.

0338 + 42m = **0420**



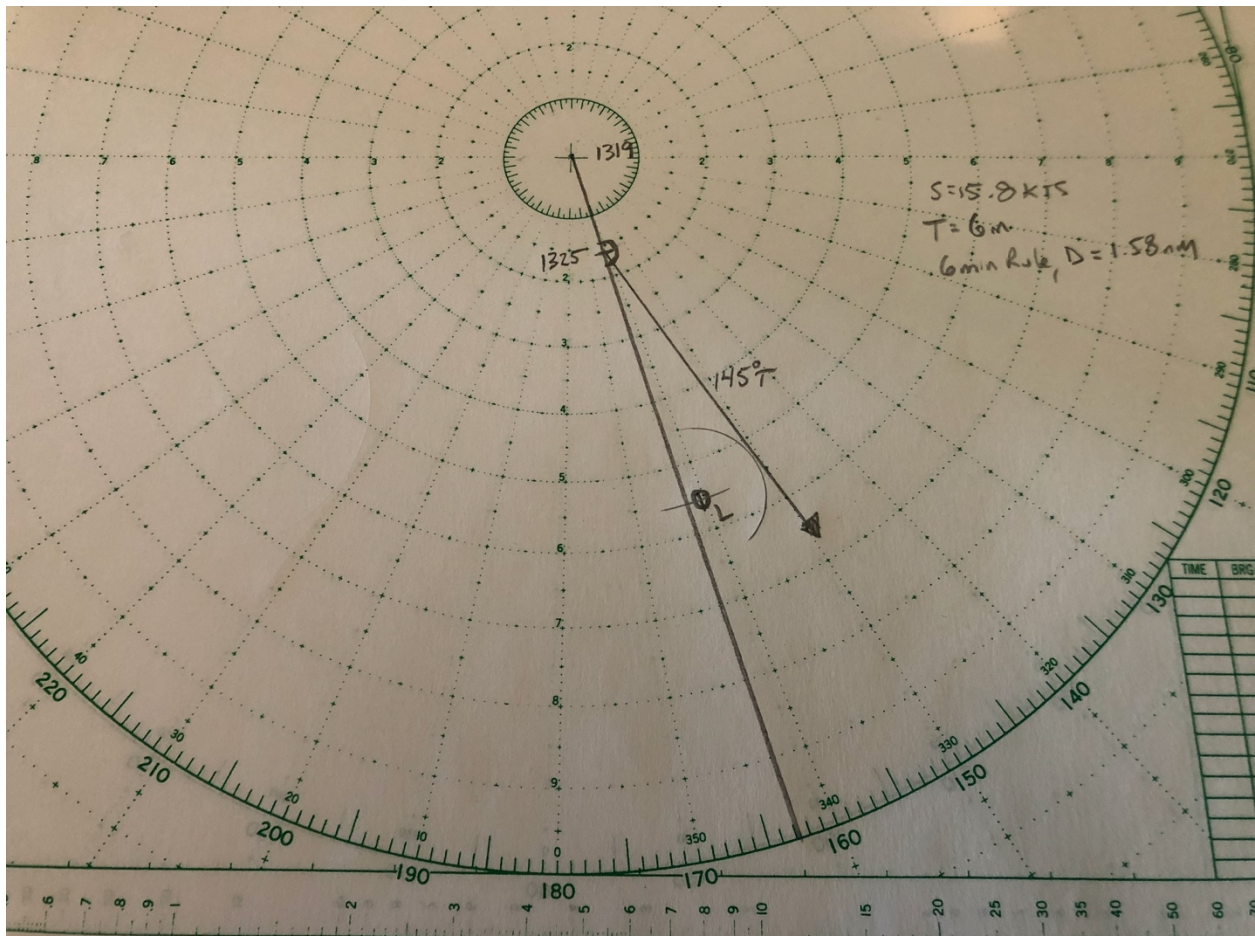


## Distance Off, Bearing, and Dead Reckoning Problems

DIS 5. You are underway on course  $163^{\circ}$  T at a speed of 15.8 knots. You sight a buoy bearing  $161^{\circ}$  T at a radar range of 5.5 miles at 1319. If you change course at 1325, what is the course to steer to leave the buoy abeam to starboard at 1.0 mile?

Answer:  $145^{\circ}$  T

- Step 1: Plot the initial course on a Maneuvering Board.
- Step 2: Plot the bearing and range to the light.
- Step 3: Plot a circle of 1.0 miles around the light.
- Step 4: Determine the distance to the course change and mark the new 1325 position. Using the 6-minute rule, the distance is 1.58nm.
- Step 5: Determine the course to steer with a tangent to the circle drawn in step 3.



## Distance Off Problems

### Distance at Second Bearing (Bowditch Table 7)

DIS B1. You are steaming on a course of  $167^{\circ}$  T at 19.5 knots. At 1837 you observe a lighthouse bearing  $224^{\circ}$  T. At 1904, the lighthouse bears  $268^{\circ}$  T. What is your distance off at the second bearing?

- a) 8.8 miles
- b) 9.5 miles
- c) 10.4 miles - correct**
- d) 11.3 miles

DS B2. You are steaming on course  $198^{\circ}$  T at 18.5 knots. At 0316 you observe a lighthouse bearing  $235^{\circ}$  T. At 0348 the lighthouse bears  $259^{\circ}$  T. What is your distance off at the second bearing?

- a) 14.8 miles - correct**
- b) 15.3 miles
- c) 15.8 miles
- d) 16.3 miles

DIS B3. You are steaming on a course of  $211^{\circ}$  T at 17 knots. At 0417 a light bears  $184^{\circ}$  T, and at 0428 the same light bears  $168^{\circ}$  T. What is the distance off the light at 0428?

- a) 3.4 miles
- b) 4.6 miles
- c) 5.1 miles - correct**
- d) 5.6 miles

Distance Abeam (Bowditch Table 7)

DIS B4. Your vessel is steering  $049^{\circ}$  T at 15 knots. At 1914 a light bears  $078^{\circ}$  T and at 1951 the same light bears  $116^{\circ}$  T. What will be your distance off abeam?

- a) **6.7 miles - correct**
- b) 7.1 miles
- c) 7.5 miles
- d) 8.3 miles

DIS B5. Your vessel is steering  $143^{\circ}$  T at 16 knots. At 2147 a light bears  $106^{\circ}$  T and at 2206 the same light bears  $078^{\circ}$  T. What will be your distance off abeam?

- a) 5.1 miles
- b) 5.4 miles
- c) **5.9 miles - correct**
- d) 6.5 miles

DIS B6. Your vessel is steering  $194^{\circ}$  T at 13 knots. At 0116 a light bears  $243^{\circ}$  T and at 0147 the same light bears  $267^{\circ}$  T. What will be your distance off abeam?

- a) 11.2 miles
- b) 11.6 miles
- c) **12.0 miles - correct**
- d) 12.5 miles

Time and Distance Abeam (26.5° - 45° Special Case)

DIS B7. Your vessel is on a course of 052° T at 16 knots. At 0916 a light bears 078.5° T and at 0927 the light bears 097° T. At what time and at what distance off will your vessel be when abeam of the light?

- a) 0929, 2.0 miles
- b) 0932, 2.3 miles
- c) 0935, 2.6 miles
- d) 0938, 2.9 miles - correct**

DIS B8. Your vessel is on a course of 079° T at 11 knots. At 0152 a light bears 105.5° T, and at 0209, the same light bears 124° T. At what time and at what distance off will your vessel be when abeam of the light?

- a) 0219, 2.3 miles
- b) 0226, 3.1 miles - correct**
- c) 0233, 3.9 miles
- d) 0242, 4.7 miles

DIS B9. Your vessel is on course 237° T at 18 knots. At 0404 a light bears 263.5° T and at 0430 the light bears 282° T. At what time and at what distance off will your vessel be when abeam of the light?

- a) 0448, 6.8 miles
- b) 0452, 7.2 miles
- c) 0456, 7.8 miles - correct**
- d) 0500, 8.4 miles



Time and Distance Abeam (22.5° - 45° Special Case)

DIS B10. Your vessel is on a course of 297° T at 11 knots. At 0019 a light bears 274.5° T and at 0048 the light bears 252° T. At what time and at what distance off will your vessel be when abeam of the light?

- a) 0102, 2.6 miles
- b) 0108, 3.7 miles - correct**
- c) 0057, 4.6 miles
- d) 0117, 5.0 miles

DIS B11. Your vessel is on a course of 144° T at 16 knots. At 0126 a light bears 166.5° T and at 0152 the light bears 189° T. At what time and at what distance off will your vessel be when abeam of the light?

- a) 0205, 4.1 miles
- b) 0210, 4.8 miles - correct**
- c) 0215, 6.0 miles
- d) 0220, 6.4 miles

DIS B12. Your vessel is on a course of 082° T at 19 knots. At 0255 a light bears 059.5° T and at 0312 the light bears 037° T. At what time and at what distance off will your vessel be when abeam of the light?

- a) 0333, 5.1 miles
- b) 0321, 4.7 miles
- c) 0327, 4.3 miles
- d) 0324, 3.8 miles - correct**

### Maneuvering Board Problems (Course to Steer)

DIS B13. While on course  $034^\circ$  pgc, a light bears  $8^\circ$  on the port bow at a distance of 8.8 miles. What course should you steer to pass 2.5 miles abeam of the light leaving it to port?

- a)  $035^\circ$  pgc
- b)  $043^\circ$  pgc - correct**
- c)  $051^\circ$  pgc
- d)  $059^\circ$  pgc

DIS B14. While on course  $066^\circ$  pgc, a light bears  $18^\circ$  on the port bow at a distance of 12.3 miles. What course should you steer to pass 4 miles abeam of the light leaving it to port?

- a)  $067^\circ$  pgc - correct**
- b)  $072^\circ$  pgc
- c)  $079^\circ$  pgc
- d)  $085^\circ$  pgc

DIS B15. While on course  $283^\circ$  pgc, a light bears  $10^\circ$  on the port bow at a distance of 8.3 miles. What course should you steer to pass 3.5 miles abeam of the light leaving it to port?

- a)  $289^\circ$  pgc
- b)  $294^\circ$  pgc
- c)  $298^\circ$  pgc - correct**
- d)  $302^\circ$  pgc

DIS B16. While on course  $159^\circ$  T a light bears  $11^\circ$  on the starboard bow at a distance of 10.6 miles. What course should you steer to pass 2 miles abeam of the light leaving it to starboard?

- a)  $159^\circ$  T - correct**
- b)  $163^\circ$  T
- c)  $167^\circ$  T
- d)  $171^\circ$  T

### Maneuvering Board Problems (Time Abeam)

DIS B17. You are steering  $163^{\circ}$  T and a light is picked up dead ahead at a distance of 11 miles at 0142. You change course to pass the light 2 miles off abeam to starboard. If you are making 13 knots, what is your ETA at the position 2 miles off the light?

- a) 0226
- b) 0229
- c) **0232 - correct**
- d) 0235

DIS B18. You are steering  $115^{\circ}$  T and a light is picked up dead ahead at a distance of 16.7 miles at 0522. You change course to pass the light 3.5 miles off abeam to port. If you are making 12 knots, what is your ETA at the position 3.5 miles off the light?

- a) **0644 - correct**
- b) 0647
- c) 0650
- d) 0653

DIS B19. You are steering  $349^{\circ}$  T and a light is picked up dead ahead at a distance of 17.2 miles at 2122. You change course to pass the light 4.5 miles off abeam to port. If you are making 19.5 knots, what is your ETA at the position 4.5 miles off the light?

- a) 2207
- b) 2210
- c) **2213 - correct**
- d) 2216

### Maneuvering Board Problems (Course Changes)

DIS B20. You are underway on course  $128^{\circ}$  T at a speed of 17.6 knots. You sight a daymark bearing  $126^{\circ}$  T at a radar range of 4.3 miles at 1649. If you change course at 1654, what is the course to steer to leave the buoy abeam to starboard at 0.5 mile?

- a)  **$113^{\circ}$  T - correct**
- b)  $116^{\circ}$  T
- c)  $119^{\circ}$  T
- d)  $121^{\circ}$  T

DIS B21. You are underway on course  $241^{\circ}$  T at a speed of 18.2 knots. You sight a daymark bearing  $241^{\circ}$  T at a radar range of 3.9 miles at 1006. If you change course at 1009, what is the course to steer to leave the buoy abeam to starboard at 1.0 mile?

- a)  $218^{\circ}$  T
- b)  **$222^{\circ}$  T - correct**
- c)  $257^{\circ}$  T
- d)  $260^{\circ}$  T

DIS B22. You are underway on course  $137^{\circ}$  T at a speed of 16.2 knots. You sight a rock bearing  $134^{\circ}$  T at a radar range of 4.6 miles at 1508. If you change course at 1514, what is the course to steer to leave the buoy abeam to port at 1.5 mile?

- a)  **$162^{\circ}$  T - correct**
- b)  $158^{\circ}$  T
- c)  $154^{\circ}$  T
- d)  $151^{\circ}$  T

## **Tide and Tidal Current Problems**



## Tide and Tidal Current Problems

- Tide and current problems were traditionally tested in the Navigation General module but seem to be tested more often in the Navigation Problems section now. You should be prepared to see tide and current problems in either module.
- By using the below “method” for tide and current problems, you can generally stay organized and error trap effectively. This is helpful on a long test when you arrive at an incorrect answer and might save the day. However, there are many ways to complete tide and current problems.
- There are also several varieties of each type of problem. Having a fundamental understanding of tide and current problems will allow you to determine what the problem is asking and how to approach it. See the question bank for representations of all different problem types. For brevity, some are solved here, and some are simply provided with solutions.

### **Tide/Current Problems Method:**

- Step 1: Find the desired station in Tables.
- Step 2: Find the reference station.
- Step 3: Note the times at reference station.
- Step 4: Apply corrections for desired station.
- Step 5: Answer the question, generally using Table 3.

Block 1: Desired Offsets

Block 2: Reference

Block 3: Calculations

Block 4: Answer the Question (e.g. Table 3)

## Tide and Tidal Current Problems

TC D1. What is the height of tide at Three Mile Harbor Entrance, Gardiner's Bay on 14 November at 0700 (+5 ZD)?

Answer: 1.7 feet.

|                     |            |                              |            |
|---------------------|------------|------------------------------|------------|
| <b>Station 1399</b> |            | <b>Reference: New London</b> |            |
| <u>Hig</u>          | <u>Low</u> | <u>High</u>                  | <u>Low</u> |
| +0:21               | +0:02      | 0453                         | 1108       |
| -0.2ft              | 0.0ft      | 2.2ft                        | 0.5ft      |

|                                   |              |                                    |  |
|-----------------------------------|--------------|------------------------------------|--|
| <b>Three Mile Harbor Entrance</b> |              | <b>Desired Time: 0700</b>          |  |
| <u>Hig</u>                        | <u>Low</u>   | Duration of Rise/Fall: 5:56        |  |
| 0453                              | 1108         | Range of Tide: 1.5 ft              |  |
| +0:21                             | +0:02        | Time from H/L: 1:46                |  |
| <b>0514</b>                       | <b>1110</b>  | Correction to <b>High</b> : -0.3ft |  |
| 2.2ft                             | 0.5ft        | 2.0ft – 0.3ft = <b>1.7ft</b>       |  |
| -0.2ft                            | 0.0ft        |                                    |  |
| <b>2.0ft</b>                      | <b>0.5ft</b> |                                    |  |

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- Table 3 is included at the end of this document.

**14 0453 2.2 0.7**  
**M 1108 0.5 0.2**  
**1658 2.2 0.7**  
**2326 0.2 0.1**

| NO.  | PLACE                                    | POSITION |       | DIFFERENCES |           |            |           | RANGES      |     | Mean Tide Level |     |     |
|------|------------------------------------------|----------|-------|-------------|-----------|------------|-----------|-------------|-----|-----------------|-----|-----|
|      |                                          |          |       | Time        |           | Height     |           | Mean Spring |     |                 |     |     |
|      |                                          | Lat.     | Long. | High Water  | Low Water | High Water | Low Water | ft          | ft  |                 |     |     |
|      |                                          |          |       | h. m.       | h. m.     | ft         | ft        |             |     |                 |     |     |
|      |                                          | °        | '     | °           | '         | h. m.      | h. m.     | ft          | ft  | ft              |     |     |
| 1393 | New Suffolk.....                         | 41       | 00    | 72          | 28        | +2 26      | +2 11     | 0.0         | 0.0 | 2.0             | 3.1 | 1.5 |
| 1395 | South Jamesport.....                     | 40       | 56    | 72          | 35        | +2 32      | +2 40     | +0.1        | 0.0 | 2.7             | 3.2 | 1.3 |
| 1397 | Shinnecock Canal.....                    | 40       | 54    | 72          | 30        | +2 33      | +2 31     | -0.2        | 0.0 | 2.4             | 2.9 | 1.2 |
| 1399 | Threemile Harbor ent., Gardiners Bay.... | 41       | 02    | 72          | 11        | +0 21      | +0 02     | -0.2        | 0.0 | 2.4             | 2.9 | 1.2 |
| 1401 | Promised Land, Napeague Bay.....         | 41       | 00    | 72          | 05        | -0 14      | -0 08     | -0.3        | 0.0 | 2.3             | 2.7 | 1.1 |
|      |                                          |          |       |             |           | -0 14      | -0 16     | -0.3        | 0.0 | 1.9             | 2.3 | 0.9 |



## Tide and Tidal Current Problems

TC D2. What is the height of tide at Falkner Island, CT, on 27 April at 1105 DST (+4 ZD)? Answer: 5.2 feet.

- Preliminary calculation: Tide tables are based on ZD +5. 1105 (+4 ZD) is the same as 1005 (+ 5ZD). We will solve the problem for 1005.

|                                                                                                                                                                                                                                                      |                                                                                                                                                                                                                          |
|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| <b>Station 1219</b><br><u>High</u> <u>Low</u><br><br>-0:13                  -0:27<br>-1.3ft                  0.0ft                                                                                                                                   | <b>Reference: Bridgeport</b><br><u>High</u> <u>Low</u><br><br>1115                  0508<br>6.9ft                  -1.2ft                                                                                                |
| <b>Falkner Island</b><br><u>High</u> <u>Low</u><br>1115                  0508<br>-0:13                  -0:27<br><br><b>1102</b> <b>0441</b><br><br>6.9ft                  -1.2ft<br>-1.3ft                  0.0ft<br><br><b>5.6ft</b> <b>-1.2ft</b> | Desired Time: 1005<br><br>Duration of Rise/Fall: 6:21<br>Range of Tide:                  6.8 ft<br>Time from H/L:                  0:57<br><br>Correction to <b>High</b> :    -0.4ft<br><br>5.6ft – 0.4ft = <b>5.2ft</b> |

- Table 3 is included at the end of this document.

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27 0508 -1.2 -0.4  
W 1115 6.9 2.1  
1721 -0.6 -0.2  
2329 7.6 2.3

| NO.                 | PLACE                             | POSITION |       | DIFFERENCES |           |            |           | RANGES      |     | Mean Tide Level |
|---------------------|-----------------------------------|----------|-------|-------------|-----------|------------|-----------|-------------|-----|-----------------|
|                     |                                   | Lat.     | Long. | Time        |           | Height     |           | Mean Spring |     |                 |
|                     |                                   |          |       | High Water  | Low Water | High Water | Low Water | ft          | ft  |                 |
|                     |                                   | °        | '     | h.          | m.        | h.         | m.        | ft          | ft  | ft              |
| on BRIDGEPORT, p.48 |                                   |          |       |             |           |            |           |             |     |                 |
| 1214                | Westbrook, Duck Island Roads..... | 41 16    | 72 28 | -0 23       | -0 34     | -2.6       | 0.0       | 4.1         | 4.7 | 2.0             |
| 1215                | Duck Island.....                  | 41 15    | 72 29 | -0 25       | -0 37     | -2.2       | 0.0       | 4.5         | 5.2 | 2.2             |
| 1217                | Madison.....                      | 41 16    | 72 36 | -0 20       | -0 32     | -1.8       | 0.0       | 4.9         | 5.6 | 2.4             |
| 1219                | Falkner Island.....               | 41 13    | 72 39 | -0 13       | -0 27     | -1.3       | 0.0       | 5.4         | 6.2 | 2.7             |
| 1220                | Sachem Head.....                  | 41 15    | 72 42 | -0 10       | -0 17     | -1.3       | 0.0       | 5.4         | 6.2 | 2.7             |

## Tide and Tidal Current Problems

TC D3. What will be the time after 0800 EST (ZD +5) that the height of tide at South Freeport, ME will be 6.0 feet on 7 November?

Answer: 0952

|                    |            |                            |            |
|--------------------|------------|----------------------------|------------|
| <b>Station 869</b> |            | <b>Reference: Portland</b> |            |
| <u>Hig</u>         | <u>Low</u> | <u>High</u>                | <u>Low</u> |
| +0:12              | +0:10      | 1225                       | 0613       |
| -0.1ft             | 0.0ft      | 10.1ft                     | -0.2ft     |

|                    |               |                                       |  |
|--------------------|---------------|---------------------------------------|--|
| <b>S. Freeport</b> |               | <b>Desired Time: 1005</b>             |  |
| <u>Hig</u>         | <u>Low</u>    | <b>Duration of Rise/Fall: 6:14</b>    |  |
| 1225               | 0613          | <b>Range of Tide: 10.2 ft</b>         |  |
| +0:12              | +0:10         | <b>Correction needed: -4.0</b>        |  |
| <b>1237</b>        | <b>0623</b>   | <b>10.0ft - 4.0ft = 6.0ft</b>         |  |
| 10.1ft             | -0.2ft        | <b>Reverse look up Time H/L: 2:45</b> |  |
| -0.1ft             | 0.0ft         | <b>High: 1237 - 2:45 = 09:52</b>      |  |
| <b>10.0ft</b>      | <b>-0.2ft</b> |                                       |  |
| <b>4.0ft</b>       | <b>6.2ft</b>  | <b>Need Corr</b>                      |  |

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| Time | Height | Time | Height |
|------|--------|------|--------|
| Day  |        | Day  |        |
| h m  | ft m   | h m  | ft m   |

|   |      |      |      |
|---|------|------|------|
| 7 | 0016 | 9.3  | 2.8  |
| M | 0613 | -0.2 | -0.1 |
|   | 1225 | 10.1 | 3.1  |
|   | 1850 | -1.1 | -0.3 |

- Table 3 is included at the end of this document.

| NO. | PLACE                                 | POSITION |       | DIFFERENCES |           |            |           | RANGES      |      | Mean Tide Level |
|-----|---------------------------------------|----------|-------|-------------|-----------|------------|-----------|-------------|------|-----------------|
|     |                                       |          |       | Time        |           | Height     |           |             |      |                 |
|     |                                       | Lat.     | Long. | High Water  | Low Water | High Water | Low Water | Mean Spring |      |                 |
|     |                                       |          |       | h. m.       | h. m.     | ft         | ft        | ft          | ft   | ft              |
| 853 | Small Point Harbor.....               | 43 44    | 69 51 | -0 12       | -0 09     | -0.3       | 0.0       | 8.8         | 10.1 | 4.4             |
| 855 | Cundy Harbor, New Meadows River.....  | 43 47    | 69 54 | -0 01       | -0 02     | -0.2       | 0.0       | 8.9         | 10.2 | 4.4             |
| 857 | Howard Point, New Meadows River.....  | 43 53    | 69 53 | -0 05       | +0 01     | -0.1       | 0.0       | 9.0         | 10.3 | 4.5             |
| 859 | Lowell Cove, Orrs Island.....         | 43 45    | 69 59 | -0 07       | -0 06     | -0.3       | 0.0       | 8.8         | 10.1 | 4.4             |
| 861 | Harpswell Harbor.....                 | 43 46    | 70 00 | -0 05       | -0 05     | -0.1       | 0.0       | 9.0         | 10.4 | 4.5             |
| 863 | South Harpswell, Potts Harbor.....    | 43 44    | 70 01 | +0 02       | +0 01     | -0.2       | 0.0       | 8.9         | 10.2 | 4.4             |
| 865 | Wilson Cove, Middle Bay.....          | 43 49    | 69 59 | +0 02       | +0 02     | 0.0        | 0.0       | 9.1         | 10.5 | 4.5             |
| 867 | Little Flying Point, Maquoit Bay..... | 43 50    | 70 03 | -0 01       | -0 01     | -0.1       | 0.0       | 9.0         | 10.3 | 4.5             |
| 869 | South Freeport.....                   | 43 49    | 70 06 | +0 12       | +0 10     | -0.1       | 0.0       | 9.0         | 10.4 | 4.5             |

## Tide and Tidal Current Problems

TC D4. What is the velocity of the tidal current at a point 2 miles west of Southwest Ledge RI on 7 September at 2330 EDT (ZD +4)?

Answer: 1.3 knots

- Preliminary calculation: Tide tables are based on ZD +5. 2330 (+4 ZD) is the same as 2230 (+5ZD). We will solve the problem for 2230.

|                                                                                                                                                                                                                      |                                                                                                                                                               |
|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------|
| <b>Station 2216</b><br><u>Slack</u> <u>Flood</u> <u>Slack</u> <u>Ebb</u><br><br>+0:02 +0:10      +0:01 -0:41<br>x0.5                      x0.5                                                                       | <b>Reference: The Ræ</b><br><u>Flood</u> <u>Slack</u><br><br>2037                      2342<br>4.3kts                                                         |
| <b>2nm W. SW L edge</b><br><u>Flood</u> <u>Slack</u><br>2037                      2342<br>+0:10                      +0:01<br><br><b>2047                      2343</b><br><br>4.3 kts<br>X0.5<br><br><b>2.15kts</b> | Desired Time: 2230<br><br>Time Slack to Desired: 1:13<br>Time Slack to Max:      2:56<br><br>Correction factor:      0.6<br><br>2.15kts x 0.6 = <b>1.3kts</b> |

- Table 3 is included at the end of this document.

THE RACE, LONG ISLAND SOUND, 1983  
F-Flood, Dir. 295° True    E-Ebb, Dir. 100° True  
**SEPTEMBER**

|   | Slack<br>Water<br>Time | Maximum<br>Current<br>Time Vel. |
|---|------------------------|---------------------------------|
| 7 |                        | 0212 4.8E                       |
| W | 0525                   | 0814 4.2F                       |
|   | 1119                   | 1439 4.7E                       |
|   | 1748                   | 2037 4.3F                       |
|   | 2342                   |                                 |

| NO.  | PLACE                                    | METER<br>DEPTH | POSITION |          | TIME DIFFERENCES        |       |                       |       | SPEED<br>RATIOS |     | AVERAGE SPEEDS AND DIRECTIONS |                  |                          |                |
|------|------------------------------------------|----------------|----------|----------|-------------------------|-------|-----------------------|-------|-----------------|-----|-------------------------------|------------------|--------------------------|----------------|
|      |                                          |                | Lat.     | Long.    | Min.<br>before<br>Flood | Flood | Min.<br>before<br>Ebb | Ebb   | Flood           | Ebb | Minimum<br>before<br>Flood    | Maximum<br>Flood | Minimum<br>before<br>Ebb | Maximum<br>Ebb |
| 2211 | Southwest Ledge.....                     | 15             | 41 07    | 71 42    | -0 33                   | -0 33 | -0 10                 | -0 08 | 0.5             | 0.5 | 0.0                           | 1.5              | 0.0                      | 2.1            |
| 2216 | Southwest Ledge, 2.0 miles west of.....  |                | 41 06.80 | 71 43.00 | +0 02                   | +0 10 | +0 01                 | -0 41 | 0.5             | 0.5 | 0.0                           | 1.5              | 0.0                      | 1.9            |
| 2221 | Watch Hill Point, 2.2 miles east of..... |                | 41 18.16 | 71 48.60 | -0 37                   | -0 08 | +0 35                 | -0 21 | 0.4             | 0.2 | 0.0                           | 1.2              | 0.0                      | 0.7            |

## Tide and Tidal Current Problems

TC D5. Determine the duration of the first PM slack water on 3 March east of the Statue of Liberty, when the current is less than 0.1 knot.

Answer: 13 minutes

|                                                                                                                                                                                                                                                      |  |  |  |                                                                                                                                                                                                                                                                              |  |  |
|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--|--|--|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--|--|
| <b>Station 3446</b><br><u>Slack</u> <u>Flood</u> <u>Slack</u> <u>Ebb</u><br><br>+0:57 +0:58       +0:56 +0:59<br>x0.8                x1.0                                                                                                            |  |  |  | <b>Reference: The Narrows</b><br><u>Flood</u> <u>Slack</u> <u>Ebb</u><br><br>0951 1251 1603<br>1.7kts                2.2kts                                                                                                                                                  |  |  |
| <b>Statue of Liberty, East</b><br><u>Flood</u> <u>Slack</u> <u>Ebb</u><br>0951 1251 1603<br>+0:58 +0:56       +0:59<br><br>1049 1347 1702<br><br>1.7kts                2.2kts<br>x0.8                x1.0<br><br><b>1.4kts                2.2kts</b> |  |  |  | <b>Period of &lt;0.1kts Slack, Table 4</b><br><br>Maximum current average:<br>$(1.4+2.2)/2 = 1.8\text{kts}$<br><br>Table 4:<br>Max                Period of Slack<br>1.5kts                15min<br>2.0kts                11 min<br><br><b>Interpolate answer to 13 min.</b> |  |  |

- Table 4 is included at the end of this document.

THE NARROWS, NEW YORK HARBOR, NEW YORK, 1983  
F-Flood, Dir. 340° True    E-Ebb, Dir. 160° True

MARCH

| Day | Slack Water Time | Maximum Current Time | Vel.  |
|-----|------------------|----------------------|-------|
|     | h.m.             | h.m.                 | knots |
| 3   | 0035             | 0345                 | 2.3E  |
| Th  | 0722             | 0951                 | 1.7F  |
|     | 1251             | 1603                 | 2.2E  |
|     | 1939             | 2220                 | 1.9F  |

| NO.  | PLACE                            | METER DEPTH | POSITION |          | TIME DIFFERENCES  |                 |       |       | SPEED RATIOS |     | AVERAGE SPEEDS AND DIRECTIONS |               |                    |             |
|------|----------------------------------|-------------|----------|----------|-------------------|-----------------|-------|-------|--------------|-----|-------------------------------|---------------|--------------------|-------------|
|      |                                  |             | Lat.     | Long.    | Min. before Flood | Min. before Ebb | Flood | Ebb   | Flood        | Ebb | Minimum before Flood          | Maximum Flood | Minimum before Ebb | Maximum Ebb |
| 3416 | Red Hook Channel.....            |             | 40 40.0  | 74 01.2  | -1 03             | -0 44           | -0 08 | -0 30 | 0.6          | 0.4 | 0.0                           | 1.0           | 0.0                | 0.7         |
| 3426 | Robbins Reef Light, east of..... |             | 40 39.45 | 74 03.48 | +0 16             | +0 16           | +0 02 | +0 24 | 0.8          | 0.8 | 0.0                           | 1.3           | 0.0                | 1.6         |
| 3436 | Red Hook, 1 mile west of.....    |             | 40 40.5  | 74 02.5  | +0 41             | +1 06           | +0 47 | +0 52 | 0.8          | 1.2 | 0.0                           | 1.3           | 0.0                | 2.3         |
| 3446 | Statue of Liberty, east of.....  |             | 40 41.4  | 74 01.8  | +0 57             | +0 58           | +0 56 | +0 59 | 0.8          | 1.0 | 0.0                           | 1.4           | 0.0                | 1.9         |

## Tide and Tidal Current Problems

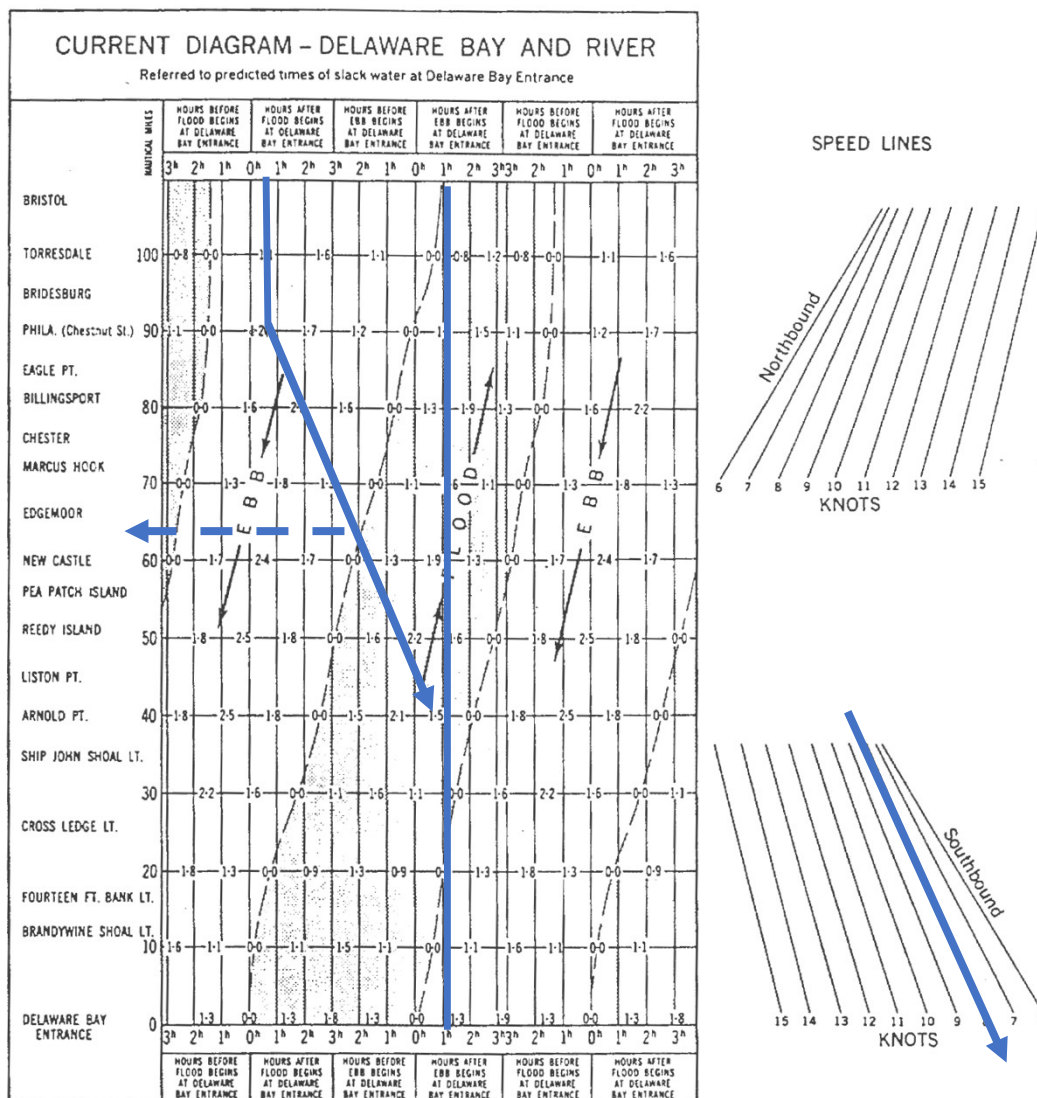
TC D6. The predicted time that the flood begins at the entrance to Delaware Bay is 1526. You are anchored off Chestnut Street in Philadelphia. If you get underway bound for sea (southbound) at 1600 and make turns for 8 knots, at what point will you lose the ebb current?

Answer: Mile 63.

Time flood begins at Delaware Bay Entrance (given): 1526  
Time underway: 1600

Departure time (difference between previous terms): 34m after flood begins at  
Entrance Current Diagram: 8.0 knots southbound.

Use the current diagram with entering arguments of 8 knots southbound, Chester Street, and 34 minutes after the flood begins at Delaware Bay Entrance to find a **solution of mile 63**.



# Tide and Tidal Current Problems

TABLE 3.—HEIGHT OF TIDE AT ANY TIME

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|                                        |       | Time from the nearest high water or low water |              |              |              |              |              |              |              |              |              |              |              |              |              |              |              |
|----------------------------------------|-------|-----------------------------------------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
|                                        |       | <i>h. m.</i>                                  | <i>h. m.</i> | <i>h. m.</i> | <i>h. m.</i> | <i>h. m.</i> | <i>h. m.</i> | <i>h. m.</i> | <i>h. m.</i> | <i>h. m.</i> | <i>h. m.</i> | <i>h. m.</i> | <i>h. m.</i> | <i>h. m.</i> | <i>h. m.</i> | <i>h. m.</i> | <i>h. m.</i> |
| Duration of rise or fall, see footnote | 4 00  | 0 08                                          | 0 15         | 0 24         | 0 32         | 0 40         | 0 48         | 0 56         | 1 04         | 1 12         | 1 20         | 1 28         | 1 36         | 1 44         | 1 52         | 2 00         | 2 08         |
|                                        | 4 20  | 0 09                                          | 0 17         | 0 26         | 0 35         | 0 43         | 0 52         | 1 01         | 1 09         | 1 18         | 1 27         | 1 35         | 1 44         | 1 53         | 2 01         | 2 10         | 2 18         |
|                                        | 4 40  | 0 09                                          | 0 19         | 0 28         | 0 37         | 0 47         | 0 56         | 1 05         | 1 15         | 1 24         | 1 33         | 1 43         | 1 52         | 2 01         | 2 11         | 2 20         | 2 29         |
|                                        | 5 00  | 0 10                                          | 0 20         | 0 30         | 0 40         | 0 50         | 1 00         | 1 10         | 1 20         | 1 30         | 1 40         | 1 50         | 2 00         | 2 10         | 2 20         | 2 30         | 2 40         |
|                                        | 5 20  | 0 11                                          | 0 21         | 0 32         | 0 43         | 0 53         | 1 04         | 1 15         | 1 25         | 1 36         | 1 47         | 1 57         | 2 08         | 2 19         | 2 29         | 2 40         | 2 50         |
|                                        | 5 40  | 0 11                                          | 0 23         | 0 34         | 0 45         | 0 57         | 1 08         | 1 19         | 1 31         | 1 42         | 1 53         | 2 05         | 2 16         | 2 27         | 2 39         | 2 50         | 3 00         |
|                                        | 6 00  | 0 12                                          | 0 24         | 0 36         | 0 48         | 1 00         | 1 12         | 1 24         | 1 36         | 1 48         | 2 00         | 2 12         | 2 24         | 2 36         | 2 48         | 3 00         | 3 12         |
|                                        | 6 20  | 0 13                                          | 0 25         | 0 38         | 0 51         | 1 03         | 1 16         | 1 29         | 1 41         | 1 54         | 2 07         | 2 19         | 2 32         | 2 45         | 2 57         | 3 10         | 3 22         |
|                                        | 6 40  | 0 13                                          | 0 27         | 0 40         | 0 53         | 1 07         | 1 20         | 1 33         | 1 47         | 2 00         | 2 13         | 2 27         | 2 40         | 2 53         | 3 07         | 3 20         | 3 33         |
|                                        | 7 00  | 0 14                                          | 0 28         | 0 42         | 0 56         | 1 10         | 1 24         | 1 38         | 1 52         | 2 06         | 2 20         | 2 34         | 2 48         | 3 02         | 3 16         | 3 30         | 3 44         |
|                                        | 7 20  | 0 15                                          | 0 29         | 0 44         | 0 59         | 1 13         | 1 28         | 1 43         | 1 57         | 2 12         | 2 27         | 2 41         | 2 56         | 3 11         | 3 25         | 3 40         | 3 54         |
|                                        | 7 40  | 0 15                                          | 0 31         | 0 46         | 1 01         | 1 17         | 1 32         | 1 47         | 2 03         | 2 18         | 2 33         | 2 49         | 3 04         | 3 19         | 3 35         | 3 50         | 4 05         |
|                                        | 8 00  | 0 16                                          | 0 32         | 0 48         | 1 04         | 1 20         | 1 36         | 1 52         | 2 08         | 2 24         | 2 40         | 2 56         | 3 12         | 3 28         | 3 44         | 4 00         | 4 16         |
|                                        | 8 20  | 0 17                                          | 0 33         | 0 50         | 1 07         | 1 23         | 1 40         | 1 57         | 2 13         | 2 30         | 2 47         | 3 03         | 3 20         | 3 37         | 3 53         | 4 10         | 4 27         |
|                                        | 8 40  | 0 17                                          | 0 35         | 0 52         | 1 09         | 1 27         | 1 44         | 2 01         | 2 19         | 2 36         | 2 53         | 3 11         | 3 28         | 3 45         | 4 03         | 4 20         | 4 37         |
|                                        | 9 00  | 0 18                                          | 0 36         | 0 54         | 1 12         | 1 30         | 1 48         | 2 06         | 2 24         | 2 42         | 3 00         | 3 18         | 3 36         | 3 54         | 4 12         | 4 30         | 4 48         |
|                                        | 9 20  | 0 19                                          | 0 37         | 0 56         | 1 15         | 1 33         | 1 52         | 2 11         | 2 29         | 2 48         | 3 07         | 3 25         | 3 44         | 4 03         | 4 21         | 4 40         | 4 58         |
|                                        | 9 40  | 0 19                                          | 0 39         | 0 58         | 1 17         | 1 37         | 1 56         | 2 15         | 2 35         | 2 54         | 3 13         | 3 33         | 3 52         | 4 11         | 4 31         | 4 50         | 5 09         |
|                                        | 10 00 | 0 20                                          | 0 40         | 1 00         | 1 20         | 1 40         | 2 00         | 2 20         | 2 40         | 3 00         | 3 20         | 3 40         | 4 00         | 4 20         | 4 40         | 5 00         | 5 20         |
|                                        | 10 20 | 0 21                                          | 0 41         | 1 02         | 1 23         | 1 43         | 2 04         | 2 25         | 2 45         | 3 06         | 3 27         | 3 47         | 4 08         | 4 29         | 4 49         | 5 10         | 5 30         |
|                                        | 10 40 | 0 21                                          | 0 43         | 1 04         | 1 25         | 1 47         | 2 08         | 2 29         | 2 51         | 3 12         | 3 33         | 3 55         | 4 16         | 4 37         | 4 59         | 5 20         | 5 41         |
|                                        |       | Correction to height                          |              |              |              |              |              |              |              |              |              |              |              |              |              |              |              |
|                                        |       | <i>Ft.</i>                                    | <i>Ft.</i>   | <i>Ft.</i>   | <i>Ft.</i>   | <i>Ft.</i>   | <i>Ft.</i>   | <i>Ft.</i>   | <i>Ft.</i>   | <i>Ft.</i>   | <i>Ft.</i>   | <i>Ft.</i>   | <i>Ft.</i>   | <i>Ft.</i>   | <i>Ft.</i>   | <i>Ft.</i>   | <i>Ft.</i>   |
| Range of tide, see footnote            | 0.5   | 0.0                                           | 0.0          | 0.0          | 0.0          | 0.0          | 0.0          | 0.1          | 0.1          | 0.1          | 0.1          | 0.1          | 0.2          | 0.2          | 0.2          | 0.2          | 0.2          |
|                                        | 1.0   | 0.0                                           | 0.0          | 0.0          | 0.0          | 0.1          | 0.1          | 0.1          | 0.2          | 0.2          | 0.2          | 0.3          | 0.3          | 0.4          | 0.4          | 0.4          | 0.5          |
|                                        | 1.5   | 0.0                                           | 0.0          | 0.0          | 0.1          | 0.1          | 0.1          | 0.2          | 0.2          | 0.3          | 0.4          | 0.4          | 0.5          | 0.6          | 0.6          | 0.7          | 0.8          |
|                                        | 2.0   | 0.0                                           | 0.0          | 0.0          | 0.1          | 0.1          | 0.2          | 0.3          | 0.3          | 0.4          | 0.5          | 0.6          | 0.7          | 0.8          | 0.9          | 1.0          | 1.1          |
|                                        | 2.5   | 0.0                                           | 0.0          | 0.1          | 0.1          | 0.2          | 0.2          | 0.3          | 0.4          | 0.5          | 0.6          | 0.7          | 0.9          | 1.0          | 1.1          | 1.2          | 1.3          |
|                                        | 3.0   | 0.0                                           | 0.0          | 0.1          | 0.1          | 0.2          | 0.3          | 0.4          | 0.5          | 0.6          | 0.8          | 0.9          | 1.0          | 1.2          | 1.3          | 1.5          | 1.6          |
|                                        | 3.5   | 0.0                                           | 0.0          | 0.1          | 0.2          | 0.2          | 0.3          | 0.4          | 0.6          | 0.7          | 0.9          | 1.0          | 1.2          | 1.4          | 1.6          | 1.8          | 2.0          |
|                                        | 4.0   | 0.0                                           | 0.0          | 0.1          | 0.2          | 0.3          | 0.4          | 0.5          | 0.7          | 0.8          | 1.0          | 1.2          | 1.4          | 1.6          | 1.8          | 2.0          | 2.2          |
|                                        | 4.5   | 0.0                                           | 0.0          | 0.1          | 0.2          | 0.3          | 0.4          | 0.6          | 0.7          | 0.9          | 1.1          | 1.3          | 1.5          | 1.8          | 2.0          | 2.2          | 2.5          |
|                                        | 5.0   | 0.0                                           | 0.1          | 0.1          | 0.2          | 0.3          | 0.5          | 0.6          | 0.8          | 1.0          | 1.2          | 1.5          | 1.7          | 2.0          | 2.2          | 2.5          | 2.8          |
|                                        | 5.5   | 0.0                                           | 0.1          | 0.1          | 0.2          | 0.4          | 0.5          | 0.7          | 0.9          | 1.1          | 1.4          | 1.6          | 1.9          | 2.2          | 2.5          | 2.8          | 3.0          |
|                                        | 6.0   | 0.0                                           | 0.1          | 0.1          | 0.3          | 0.4          | 0.6          | 0.8          | 1.0          | 1.2          | 1.5          | 1.8          | 2.1          | 2.4          | 2.7          | 3.0          | 3.2          |
|                                        | 6.5   | 0.0                                           | 0.1          | 0.2          | 0.3          | 0.4          | 0.6          | 0.8          | 1.1          | 1.3          | 1.6          | 1.9          | 2.2          | 2.6          | 2.9          | 3.2          | 3.5          |
|                                        | 7.0   | 0.0                                           | 0.1          | 0.2          | 0.3          | 0.5          | 0.7          | 0.9          | 1.2          | 1.4          | 1.8          | 2.1          | 2.4          | 2.8          | 3.1          | 3.5          | 3.8          |
|                                        | 7.5   | 0.0                                           | 0.1          | 0.2          | 0.3          | 0.5          | 0.7          | 1.0          | 1.2          | 1.5          | 1.9          | 2.2          | 2.6          | 3.0          | 3.4          | 3.8          | 4.0          |
|                                        | 8.0   | 0.0                                           | 0.1          | 0.2          | 0.3          | 0.5          | 0.8          | 1.0          | 1.3          | 1.6          | 2.0          | 2.4          | 2.8          | 3.2          | 3.6          | 4.0          | 4.2          |
|                                        | 8.5   | 0.0                                           | 0.1          | 0.2          | 0.4          | 0.6          | 0.8          | 1.1          | 1.4          | 1.8          | 2.1          | 2.5          | 2.9          | 3.4          | 3.8          | 4.2          | 4.5          |
|                                        | 9.0   | 0.0                                           | 0.1          | 0.2          | 0.4          | 0.6          | 0.9          | 1.2          | 1.5          | 1.9          | 2.2          | 2.7          | 3.1          | 3.6          | 4.0          | 4.5          | 4.8          |
|                                        | 9.5   | 0.0                                           | 0.1          | 0.2          | 0.4          | 0.6          | 0.9          | 1.2          | 1.6          | 2.0          | 2.4          | 2.8          | 3.3          | 3.8          | 4.3          | 4.8          | 5.0          |
|                                        | 10.0  | 0.0                                           | 0.1          | 0.2          | 0.4          | 0.7          | 1.0          | 1.3          | 1.7          | 2.1          | 2.5          | 3.0          | 3.5          | 4.0          | 4.5          | 5.0          | 5.2          |
|                                        | 10.5  | 0.0                                           | 0.1          | 0.3          | 0.5          | 0.7          | 1.0          | 1.3          | 1.7          | 2.2          | 2.6          | 3.1          | 3.6          | 4.2          | 4.7          | 5.2          | 5.5          |
|                                        | 11.0  | 0.0                                           | 0.1          | 0.3          | 0.5          | 0.7          | 1.1          | 1.4          | 1.8          | 2.3          | 2.8          | 3.3          | 3.8          | 4.4          | 4.9          | 5.5          | 5.8          |
|                                        | 11.5  | 0.0                                           | 0.1          | 0.3          | 0.5          | 0.8          | 1.1          | 1.5          | 1.9          | 2.4          | 2.9          | 3.4          | 4.0          | 4.6          | 5.1          | 5.8          | 6.0          |
|                                        | 12.0  | 0.0                                           | 0.1          | 0.3          | 0.5          | 0.8          | 1.1          | 1.5          | 2.0          | 2.5          | 3.0          | 3.6          | 4.1          | 4.8          | 5.4          | 6.0          | 6.2          |
|                                        | 12.5  | 0.0                                           | 0.1          | 0.3          | 0.5          | 0.8          | 1.2          | 1.6          | 2.1          | 2.6          | 3.1          | 3.7          | 4.3          | 5.0          | 5.6          | 6.2          | 6.5          |
|                                        | 13.0  | 0.0                                           | 0.1          | 0.3          | 0.6          | 0.9          | 1.2          | 1.7          | 2.2          | 2.7          | 3.2          | 3.9          | 4.5          | 5.1          | 5.8          | 6.5          | 6.8          |
|                                        | 13.5  | 0.0                                           | 0.1          | 0.3          | 0.6          | 0.9          | 1.3          | 1.7          | 2.2          | 2.8          | 3.4          | 4.0          | 4.7          | 5.3          | 6.0          | 6.8          | 7.0          |
|                                        | 14.0  | 0.0                                           | 0.2          | 0.3          | 0.6          | 0.9          | 1.3          | 1.8          | 2.3          | 2.9          | 3.5          | 4.2          | 4.8          | 5.5          | 6.3          | 7.0          | 7.2          |
|                                        | 14.5  | 0.0                                           | 0.2          | 0.4          | 0.6          | 1.0          | 1.4          | 1.9          | 2.4          | 3.0          | 3.6          | 4.3          | 5.0          | 5.7          | 6.5          | 7.2          | 7.5          |
|                                        | 15.0  | 0.0                                           | 0.2          | 0.4          | 0.6          | 1.0          | 1.4          | 1.9          | 2.5          | 3.1          | 3.8          | 4.4          | 5.2          | 5.9          | 6.7          | 7.5          | 7.8          |
|                                        | 15.5  | 0.0                                           | 0.2          | 0.4          | 0.7          | 1.0          | 1.5          | 2.0          | 2.6          | 3.2          | 3.9          | 4.6          | 5.4          | 6.1          | 6.9          | 7.8          | 8.0          |
|                                        | 16.0  | 0.0                                           | 0.2          | 0.4          | 0.7          | 1.1          | 1.5          | 2.1          | 2.6          | 3.3          | 4.0          | 4.7          | 5.5          | 6.3          | 7.2          | 8.0          | 8.2          |
|                                        | 16.5  | 0.0                                           | 0.2          | 0.4          | 0.7          | 1.1          | 1.6          | 2.1          | 2.7          | 3.4          | 4.1          | 4.9          | 5.7          | 6.5          | 7.4          | 8.2          | 8.5          |
|                                        | 17.0  | 0.0                                           | 0.2          | 0.4          | 0.7          | 1.1          | 1.6          | 2.2          | 2.8          | 3.5          | 4.2          | 5.0          | 5.9          | 6.7          | 7.6          | 8.5          | 8.8          |
|                                        | 17.5  | 0.0                                           | 0.2          | 0.4          | 0.8          | 1.2          | 1.7          | 2.2          | 2.9          | 3.6          | 4.4          | 5.2          | 6.0          | 6.9          | 7.8          | 8.8          | 9.0          |
|                                        | 18.0  | 0.0                                           | 0.2          | 0.4          | 0.8          | 1.2          | 1.7          | 2.3          | 3.0          | 3.7          | 4.5          | 5.3          | 6.2          | 7.1          | 8.1          | 9.0          | 9.2          |
|                                        | 18.5  | 0.1                                           | 0.2          | 0.5          | 0.8          | 1.2          | 1.8          | 2.4          | 3.1          | 3.8          | 4.6          | 5.5          | 6.4          | 7.3          | 8.3          | 9.2          | 9.5          |
|                                        | 19.0  | 0.1                                           | 0.2          | 0.5          | 0.8          | 1.3          | 1.9          | 2.4          | 3.1          | 3.9          | 4.8          | 5.6          | 6.6          | 7.5          | 8.5          | 9.5          | 9.8          |
|                                        | 19.5  | 0.1                                           | 0.2          | 0.5          | 0.8          | 1.3          | 1.9          | 2.5          | 3.2          | 4.0          | 4.9          | 5.8          | 6.7          | 7.7          | 8.7          | 9.8          | 10.0         |
|                                        | 20.0  | 0.1                                           | 0.2          | 0.5          | 0.9          | 1.3          | 1.9          | 2.6          | 3.3          | 4.1          | 5.0          | 5.9          | 6.9          | 7.9          | 9.0          | 10.0         |              |

Obtain from the predictions the high water and low water, one of which is before and the other after the time for which the height is required. The difference between the times of occurrence of these tides is the duration of rise or fall, and the difference between their heights is the range of tide for the above table. Find the difference between the nearest high or low water and the time for which the height is required.

Enter the table with the duration of rise or fall, printed in heavy-faced type, which most nearly agrees with the actual value, and on that horizontal line find the time from the nearest high or low water which agrees most nearly with the corresponding actual difference. The correction sought is in the column directly below, on the line with the range of tide.

When the nearest tide is high water, subtract the correction.

When the nearest tide is low water, add the correction.

# Tide and Tidal Current Problems

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TABLE 3.—VELOCITY OF CURRENT AT ANY TIME

| TABLE A                                    |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
|--------------------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Interval between slack and maximum current |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| Interval between slack and desired time    |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
|                                            | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. |
|                                            | 1 20  | 1 40  | 2 00  | 2 20  | 2 40  | 3 00  | 3 20  | 3 40  | 4 00  | 4 20  | 4 40  | 5 00  | 5 20  | 5 40  |
| h. m.                                      | f.    | f.    | f.    | f.    | f.    | f.    | f.    | f.    | f.    | f.    | f.    | f.    | f.    | f.    |
| 0 20                                       | 0.4   | 0.3   | 0.3   | 0.2   | 0.2   | 0.2   | 0.2   | 0.1   | 0.1   | 0.1   | 0.1   | 0.1   | 0.1   | 0.1   |
| 0 40                                       | 0.7   | 0.6   | 0.5   | 0.4   | 0.4   | 0.3   | 0.3   | 0.3   | 0.3   | 0.2   | 0.2   | 0.2   | 0.2   | 0.2   |
| 1 00                                       | 0.9   | 0.8   | 0.7   | 0.6   | 0.6   | 0.5   | 0.5   | 0.4   | 0.4   | 0.4   | 0.3   | 0.3   | 0.3   | 0.3   |
| 1 20                                       | 1.0   | 1.0   | 0.9   | 0.8   | 0.7   | 0.6   | 0.6   | 0.5   | 0.5   | 0.5   | 0.4   | 0.4   | 0.4   | 0.4   |
| 1 40                                       | ----- | 1.0   | 1.0   | 0.9   | 0.8   | 0.7   | 0.7   | 0.6   | 0.6   | 0.5   | 0.5   | 0.4   | 0.4   | 0.4   |
| 2 00                                       | ----- | ----- | 1.0   | 1.0   | 0.9   | 0.9   | 0.8   | 0.8   | 0.7   | 0.7   | 0.6   | 0.6   | 0.6   | 0.5   |
| 2 20                                       | ----- | ----- | ----- | 1.0   | 1.0   | 0.9   | 0.9   | 0.8   | 0.8   | 0.7   | 0.7   | 0.7   | 0.6   | 0.6   |
| 2 40                                       | ----- | ----- | ----- | ----- | 1.0   | 1.0   | 1.0   | 0.9   | 0.9   | 0.8   | 0.8   | 0.7   | 0.7   | 0.7   |
| 3 00                                       | ----- | ----- | ----- | ----- | ----- | 1.0   | 1.0   | 1.0   | 0.9   | 0.9   | 0.8   | 0.8   | 0.8   | 0.7   |
| 3 20                                       | ----- | ----- | ----- | ----- | ----- | ----- | 1.0   | 1.0   | 1.0   | 0.9   | 0.9   | 0.9   | 0.8   | 0.8   |
| 3 40                                       | ----- | ----- | ----- | ----- | ----- | ----- | ----- | 1.0   | 1.0   | 1.0   | 0.9   | 0.9   | 0.9   | 0.9   |
| 4 00                                       | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | 1.0   | 1.0   | 1.0   | 1.0   | 0.9   | 0.9   |
| 4 20                                       | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | 1.0   | 1.0   | 1.0   | 1.0   | 0.9   |
| 4 40                                       | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | 1.0   | 1.0   | 1.0   | 1.0   |
| 5 00                                       | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | 1.0   | 1.0   | 1.0   |
| 5 20                                       | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | 1.0   | 1.0   |
| 5 40                                       | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | 1.0   |

| TABLE B                                    |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
|--------------------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Interval between slack and maximum current |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| Interval between slack and desired time    |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
|                                            | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. |
|                                            | 1 20  | 1 40  | 2 00  | 2 20  | 2 40  | 3 00  | 3 20  | 3 40  | 4 00  | 4 20  | 4 40  | 5 00  | 5 20  | 5 40  |
| h. m.                                      | f.    | f.    | f.    | f.    | f.    | f.    | f.    | f.    | f.    | f.    | f.    | f.    | f.    | f.    |
| 0 20                                       | 0.5   | 0.4   | 0.4   | 0.3   | 0.3   | 0.3   | 0.3   | 0.3   | 0.2   | 0.2   | 0.2   | 0.2   | 0.2   | 0.2   |
| 0 40                                       | 0.8   | 0.7   | 0.6   | 0.5   | 0.5   | 0.5   | 0.4   | 0.4   | 0.4   | 0.4   | 0.3   | 0.3   | 0.3   | 0.3   |
| 1 00                                       | 0.9   | 0.8   | 0.8   | 0.7   | 0.7   | 0.6   | 0.6   | 0.5   | 0.5   | 0.5   | 0.4   | 0.4   | 0.4   | 0.4   |
| 1 20                                       | 1.0   | 1.0   | 0.9   | 0.8   | 0.8   | 0.7   | 0.7   | 0.6   | 0.6   | 0.6   | 0.5   | 0.5   | 0.5   | 0.5   |
| 1 40                                       | ----- | 1.0   | 1.0   | 0.9   | 0.9   | 0.8   | 0.8   | 0.7   | 0.7   | 0.6   | 0.6   | 0.6   | 0.6   | 0.6   |
| 2 00                                       | ----- | ----- | 1.0   | 1.0   | 0.9   | 0.9   | 0.9   | 0.8   | 0.8   | 0.7   | 0.7   | 0.7   | 0.7   | 0.6   |
| 2 20                                       | ----- | ----- | ----- | 1.0   | 1.0   | 1.0   | 0.9   | 0.9   | 0.8   | 0.8   | 0.8   | 0.7   | 0.7   | 0.7   |
| 2 40                                       | ----- | ----- | ----- | ----- | 1.0   | 1.0   | 1.0   | 0.9   | 0.9   | 0.9   | 0.8   | 0.8   | 0.8   | 0.7   |
| 3 00                                       | ----- | ----- | ----- | ----- | ----- | 1.0   | 1.0   | 1.0   | 0.9   | 0.9   | 0.9   | 0.9   | 0.8   | 0.8   |
| 3 20                                       | ----- | ----- | ----- | ----- | ----- | ----- | 1.0   | 1.0   | 1.0   | 1.0   | 0.9   | 0.9   | 0.9   | 0.8   |
| 3 40                                       | ----- | ----- | ----- | ----- | ----- | ----- | ----- | 1.0   | 1.0   | 1.0   | 1.0   | 0.9   | 0.9   | 0.9   |
| 4 00                                       | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | 1.0   | 1.0   | 1.0   | 1.0   | 0.9   | 0.9   |
| 4 20                                       | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | 1.0   | 1.0   | 1.0   | 1.0   | 0.9   |
| 4 40                                       | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | 1.0   | 1.0   | 1.0   | 1.0   |
| 5 00                                       | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | 1.0   | 1.0   | 1.0   |
| 5 20                                       | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | 1.0   | 1.0   |
| 5 40                                       | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | 1.0   |

Use table A for all places except those listed below for table B.  
 Use table B for Cape Cod Canal, Hell Gate, Chesapeake and Delaware Canal and all stations in table 2 which are referred to them.

1. From predictions find the time of slack water and the time and velocity of maximum current (flood or ebb), one of which is immediately before and the other after the time for which the velocity is desired.
2. Find the interval of time between the above slack and maximum current, and enter the top of table A or B with the interval which most nearly agrees with this value.
3. Find the interval of time between the above slack and the time desired, and enter the side of table A or B with the interval which most nearly agrees with this value.
4. Find, in the table, the factor corresponding to the above two intervals, and multiply the maximum velocity by this factor. The result will be the approximate velocity at the time desired.



# Tide and Tidal Current Problems

## *Duration of weak current near time of slack water*

TABLE A

| Maximum<br>current | Period with a velocity not more than— |                |                |                |                |
|--------------------|---------------------------------------|----------------|----------------|----------------|----------------|
|                    | 0.1 knot                              | 0.2 knot       | 0.3 knot       | 0.4 knot       | 0.5 knot       |
| <i>Knots</i>       | <i>Minutes</i>                        | <i>Minutes</i> | <i>Minutes</i> | <i>Minutes</i> | <i>Minutes</i> |
| 1.0                | 23                                    | 46             | 70             | 94             | 120            |
| 1.5                | 15                                    | 31             | 46             | 62             | 78             |
| 2.0                | 11                                    | 23             | 35             | 46             | 58             |
| 3.0                | 8                                     | 15             | 23             | 31             | 38             |
| 4.0                | 6                                     | 11             | 17             | 23             | 29             |
| 5.0                | 5                                     | 9              | 14             | 18             | 23             |
| 6.0                | 4                                     | 8              | 11             | 15             | 19             |
| 7.0                | 3                                     | 7              | 10             | 13             | 16             |
| 8.0                | 3                                     | 6              | 9              | 11             | 14             |
| 9.0                | 3                                     | 5              | 8              | 10             | 13             |
| 10.0               | 2                                     | 5              | 7              | 9              | 11             |



## Tide and Tidal Current Problems

### Tide Problems

TC B1. Determine the height of the tide at 2045 EST (ZD +5) at Augusta, ME, on 8 March 1983.

- a) 1.4 feet (0.5 meter)
- b) 1.9 feet (0.6 meter) - correct**
- c) 2.3 feet (0.7 meter)
- d) 2.6 feet (0.8 meter)

TC B2. What will be the height of tide at Three Mile Harbor Entrance, Gardiner's Bay, NY, at 0700 (ZD +5) on 14 November 1983?

- a) 1.1 feet
- b) 1.7 feet - correct**
- c) 1.9 feet
- d) 2.2 feet

TC B3. On 10 August 1983 you will dock near Days Point, Weehawken, on the Hudson River at 1800 DST (ZD +4). The charted depth alongside the pier is 24 feet (7.3 meters). What will be the depth of water when you dock?

- a) 23.5 feet (7.1 m)
- b) 23.9 feet (7.2m) - correct**
- c) 24.9 feet (7.5m)
- d) 26.3 feet (8.0m)

TC B4. You are to sail from Elizabethport, NJ on 22 May 1983 with a maximum draft of 28 feet. You will pass over an obstruction with a charted depth of 27 feet. The steaming time from Elizabethport to the obstruction is 1h 40m. What is the earliest time (ZD +4) you can sail on the afternoon of 22 May and pass over the obstruction with 3 feet of clearance?

- a) 1407 - correct**
- b) 1331
- c) 1303
- d) 1242

TC B5. What will be the time after 1000 EST (ZD +5), on 4 March 1983, that the height of the tide at City Island, NY, will be 2.4 feet?

- a) 1228 - correct**
- b) 1240
- c) 1244
- d) 1248

### Tidal Current Problems

TC B6. What is the predicted velocity of the tidal current 2 miles west of Southwest Ledge for 2330 DST (ZD +4) on 7 September 1983?

- a) **1.3 knots - correct**
- b) 1.6 knots
- c) 1.9 knots
- d) 2.2 knots

TC B7. What will be the direction and velocity of the tidal current at Provincetown Harbor, MA at 1045 DST (ZD +4) on 5 May 1983?

- a) 0.0 knot at 135° T
- b) 0.2 knot at 135° T
- c) **0.4 knot at 315° T - correct**
- d) 0.6 knot at 315° T

TC B8. What is the period of time from around 1008 EST (ZD +4) at Canapipsit Channel, MA on 7 August 1983, in which the current does not exceed 0.4 knots?

- a) 0945 to 1031
- b) 0950 to 1026
- c) **0955 to 1021 - correct**
- d) 1000 to 1024

TC B9. The predicted time that the flood begins at the entrance to Delaware Bay is 1526. You are anchored off Chestnut Street in Philadelphia. If you get underway bound for sea at 1600 and turn for 8 knots, at what point will you lose the ebb current?

- a) Billingsport
- b) Marcus Hook
- c) **Mile 63 - correct**
- d) Mile 52

TC B10. Determine the duration of the first PM slack water on 3 March, 1983, east of the Statue of Liberty, when the current is less than 0.1 knot?

- a) 10 minutes
- b) **13 minutes - correct**
- c) 16 minutes
- d) 19 minutes

TC B11. Determine the time after 0300 CST (ZD +6) when the velocity of the tidal current will be 0.5 knot on 16 April 1983 at Port Arthur Canal Entrance, TX.

- a) 0436
- b) 0507 - correct**
- c) 0538
- d) 0554

TC B12. You are bound for the Chelsea docks in the Hudson River. The Captain wants to arrive at the docks at the first slack water on 28 July 1983. You are keeping daylight saving time. What time should you be at the docks?

- a) 0215 - correct**
- b) 0530
- c) 0811
- d) 0911



## **Amplitude Problems**



## Amplitude Problems

- Amplitude problems involve calculating the bearing at which an object *should* rise or set, and then comparing the calculation to actual observation in order to determine compass error. Amplitude is the easiest means of determining gyro error at sea, and can involve the sun, moon, or planets and stars.
- **Declination** - the angular distance north or south of the celestial equator, or the latitude of the point on earth directly beneath a celestial object. For example, if the sun's declination is  $10^{\circ}$  N, the sun is directly overhead at  $10^{\circ}$  N.
- **Amplitude** – the angular distance north or south of the equator of a celestial body on the horizon. Amplitudes are named based on the direction of the object and the difference from the equator. For example, if the sunset is observed at  $280^{\circ}$  T, the amplitude of the sun is W  $10^{\circ}$  N. If the sunrise is observed at  $080^{\circ}$  T, the amplitude of the sun is E  $10^{\circ}$  N. Amplitudes are found in Table 22 or Table 27 of Bowditch (depending on version used).
- **Horizon** – There are several different versions of “horizon” in celestial navigation. The simplest calculations are made when objects are on the “celestial” horizon as follows:
  - Sun – ideally when the sun's lower limb is  $\frac{2}{3}$  of a sun diameter (20 arc minutes) above the visual horizon.
  - Stars and Planets – ideally when the object is one sun diameter (30 arc minutes) above the visual horizon.
  - Moon – ideally when the upper limb of the moon is on the visual horizon.
- When objects are not on the “celestial” horizon, corrections must be made using Table 23 or Table 28 in Bowditch (depending on the version used). This correction has different rules depending on the body, season, and location.

## Amplitude Problems

### Amplitude Problems of the Sun on the Celestial Horizon

AMP D1. It is 20 May. You have taken an observation of the rising sun when its lower limb is approximately 2/3 of a sun's diameter above the horizon (in other words the sun's center is on the celestial horizon). The time of observation is 1000 UTC. Your latitude is 36° N.

- What is the amplitude of the sun?
- What true bearing should the sunrise be observed?
- If you actually observe the sun rising at 068° T, what is the gyro error?

Answers:

- E 25° N
- 065° T
- 3° W

| G.M.T. | SUN    |      |      |      |
|--------|--------|------|------|------|
|        | G.H.A. |      | Dec. |      |
| 20 00  | 180    | 53.7 | N19  | 54.8 |
| 01     | 195    | 53.7 | 55.3 |      |
| 02     | 210    | 53.6 | 55.8 |      |
| 03     | 225    | 53.6 | 56.3 |      |
| 04     | 240    | 53.6 | 56.9 |      |
| 05     | 255    | 53.5 | 57.4 |      |
| 06     | 270    | 53.5 | N19  | 57.9 |
| 07     | 285    | 53.5 | 58.4 |      |
| W 08   | 300    | 53.4 | 59.0 |      |
| E 09   | 315    | 53.4 | 19   | 59.5 |
| D 10   | 330    | 53.4 | 20   | 00.0 |
| N 11   | 345    | 53.3 | 00.5 |      |
| E 12   |        |      |      |      |

Step 1: Determine the declination of the sun for the time of observation using the Nautical Almanac.  
The declination at 1000 UTC is N 20° 00'.

Step 2: Determine the ship's latitude at the time of observation.  
Latitude – 36° N (given)

Step 3: Enter Table 22/27 in Bowditch with declination and latitude to determine the amplitude.  
Declination: 20°  
Latitude: 36°

| Amplitudes |             |      |      |      |      |      |      |      |      |      |      |      |      |          |
|------------|-------------|------|------|------|------|------|------|------|------|------|------|------|------|----------|
| Latitude   | Declination |      |      |      |      |      |      |      |      |      |      |      |      | Latitude |
|            | 18°0        | 18°5 | 19°0 | 19°5 | 20°0 | 20°5 | 21°0 | 21°5 | 22°0 | 22°5 | 23°0 | 23°5 | 24°0 |          |
| 0          | 18.0        | 18.5 | 19.0 | 19.5 | 20.0 | 20.5 | 21.0 | 21.5 | 22.0 | 22.5 | 23.0 | 23.5 | 24.0 | 0        |
| 10         | 18.3        | 18.8 | 19.3 | 19.8 | 20.3 | 20.8 | 21.3 | 21.8 | 22.4 | 22.9 | 23.4 | 23.9 | 24.4 | 10       |
| 15         | 18.7        | 19.2 | 19.7 | 20.2 | 20.7 | 21.3 | 21.8 | 22.3 | 22.8 | 23.3 | 23.9 | 24.4 | 24.9 | 15       |
| 20         | 19.2        | 19.7 | 20.3 | 20.8 | 21.3 | 21.9 | 22.4 | 23.0 | 23.5 | 24.0 | 24.6 | 25.1 | 25.6 | 20       |
| 25         | 19.9        | 20.5 | 21.1 | 21.6 | 22.2 | 22.7 | 23.3 | 23.9 | 24.4 | 25.0 | 25.5 | 26.1 | 26.7 | 25       |
| 30         | 20.9        | 21.5 | 22.1 | 22.7 | 23.3 | 23.9 | 24.4 | 25.0 | 25.6 | 26.2 | 26.8 | 27.4 | 28.0 | 30       |
| 32         | 21.4        | 22.0 | 22.6 | 23.2 | 23.8 | 24.4 | 25.0 | 25.6 | 26.2 | 26.8 | 27.4 | 28.0 | 28.7 | 32       |
| 34         | 21.9        | 22.5 | 23.1 | 23.7 | 24.4 | 25.0 | 25.6 | 26.2 | 26.9 | 27.5 | 28.1 | 28.7 | 29.4 | 34       |
| 36         | 22.5        | 23.1 | 23.7 | 24.4 | 25.0 | 25.7 | 26.3 | 26.9 | 27.6 | 28.2 | 28.9 | 29.5 | 30.2 | 36       |
| 38         | 23.1        | 23.7 | 24.4 | 25.1 | 25.7 | 26.4 | 27.1 | 27.7 | 28.4 | 29.1 | 29.7 | 30.4 | 31.1 | 38       |

Step 4: Answer required questions.

- Amplitude = E 25° N**
- Standard sunrise is 090° T. In the northern hemisphere in spring and summer, the sun rises north of east (e.g. the declination is North). Therefore, the calculated sunrise is 090° - 25° = **065° T**
- If the sun is observed rising at 068° T, while the calculated sunrise is 065° T, the gyro error is 068° - 065° = 3°. To determine the direction of error, use the mnemonic "Gyro Best, Error West, Gyro Least, Error East." In this case, the gyro is higher (best) than the observation, so the error is **3° W**.



## Amplitude Problems

AMP D2. On 24 August in DR position latitude  $26^{\circ} 49.4' \text{ N}$ , longitude  $146^{\circ} 19.4' \text{ E}$ , you observe an amplitude of the Sun. The Sun's center is on the celestial horizon and bears  $084^{\circ} \text{ psc}$ . The chronometer reads 07h 55m 06s and is 01m 11s fast. Variation in the area is  $15^{\circ} \text{ W}$ . What is the deviation of the magnetic compass?

Answer:  $8.2^{\circ} \text{ E}$  deviation.

- Step 1: Determine the actual time of observation.  
 07:55:06 chronometer time of observation  
 00:01:11 fast on GMT  
 07:55:06 – 00:01:11 = 07:53:55 correct chronometer time

$146^{\circ} 19.4' \text{ E}$  corresponds to a zone time of (-10). Since the approximate zone time is 07:53, the correct GMT is actually 19:53:55, on the 23<sup>rd</sup> of August.

- Step 2: Determine the declination of the sun for the time of observation using the Nautical Almanac.

The declination at 19:53:55 is not given in the Nautical Almanac and must be interpolated.

The base value for 1900 is  $\text{N } 11^{\circ} 17.0'$  and decreasing.

The  $d$  value for 23-25 August is 0.9.

| SUN               |        |      |      |      |
|-------------------|--------|------|------|------|
| G.M.T.            | G.H.A. |      | Dec. |      |
| 18                | 89     | 22.5 | N 11 | 17.8 |
| 19                | 104    | 22.6 |      | 17.0 |
| 20                | 119    | 22.8 |      | 16.1 |
| 21                | 134    | 23.0 | ..   | 15.3 |
| 22                | 149    | 23.1 |      | 14.4 |
| 23                | 164    | 23.3 |      | 13.6 |
| S.D. 15.8 $d$ 0.9 |        |      |      |      |

Enter the Increments and Corrections Page in the Nautical Almanac with the daily  $d$  value and a time of 53 minutes, 55 seconds (the difference between the base declination and the observation time).

Given a  $d$  value of 0.9, the declination correction factor is 0.8.

Since the declination is decreasing from hour to hour, the corrected declination for 24 August at 19:53:55 is  $\text{N } 11^{\circ} 17.0' - 0.8' = \text{N } 11^{\circ} 16.2'$

| <sup>m</sup><br>53 | SUN<br>PLANETS | ARIES   | MOON    | $v$<br>or<br>Corr <sup>n</sup><br>$d$ | $v$<br>or<br>Corr <sup>n</sup><br>$d$ | $v$<br>or<br>Corr <sup>n</sup><br>$d$ |
|--------------------|----------------|---------|---------|---------------------------------------|---------------------------------------|---------------------------------------|
| 00                 | 13 15.0        | 13 17.2 | 12 38.8 | 0.0 0.0                               | 6.0 5.4                               | 12.0 10.7                             |
| 01                 | 13 15.3        | 13 17.4 | 12 39.0 | 0.1 0.1                               | 6.1 5.4                               | 12.1 10.8                             |
| 02                 | 13 15.5        | 13 17.7 | 12 39.3 | 0.2 0.2                               | 6.2 5.5                               | 12.2 10.9                             |
| 03                 | 13 15.8        | 13 17.9 | 12 39.5 | 0.3 0.3                               | 6.3 5.6                               | 12.3 11.0                             |
| 04                 | 13 16.0        | 13 18.2 | 12 39.7 | 0.4 0.4                               | 6.4 5.7                               | 12.4 11.1                             |
| 05                 | 13 16.3        | 13 18.4 | 12 40.0 | 0.5 0.4                               | 6.5 5.8                               | 12.5 11.1                             |
| 06                 | 13 16.5        | 13 18.7 | 12 40.2 | 0.6 0.5                               | 6.6 5.9                               | 12.6 11.2                             |
| 07                 | 13 16.8        | 13 18.9 | 12 40.5 | 0.7 0.6                               | 6.7 6.0                               | 12.7 11.3                             |
| 08                 | 13 17.0        | 13 19.2 | 12 40.7 | 0.8 0.7                               | 6.8 6.1                               | 12.8 11.4                             |
| 09                 | 13 17.3        | 13 19.4 | 12 40.9 | 0.9 0.8                               | 6.9 6.2                               | 12.9 11.5                             |

- Step 3: Determine the ship's latitude at the time of observation.  
 Latitude –  $26^{\circ} 49.4' \text{ N}$  (given)

## Amplitude Problems

Step 4: Enter Table 22/27 in Bowditch with declination (in tenths notation) and latitude to determine the amplitude.

Declination: N 11° 16.2' = N 11.3°

Latitude: 26° 49.4' N = 26.8° N

| Amplitudes |             |     |     |     |      |      |      |      |      |      |      |      |      |          |
|------------|-------------|-----|-----|-----|------|------|------|------|------|------|------|------|------|----------|
| Latitude   | Declination |     |     |     |      |      |      |      |      |      |      |      |      | Latitude |
|            | 6°0         | 6°5 | 7°0 | 7°5 | 8°0  | 8°5  | 9°0  | 9°5  | 10°0 | 10°5 | 11°0 | 11°5 | 12°0 |          |
| °          | °           | °   | °   | °   | °    | °    | °    | °    | °    | °    | °    | °    | °    | °        |
| 0          | 6.0         | 6.5 | 7.0 | 7.5 | 8.0  | 8.5  | 9.0  | 9.5  | 10.0 | 10.5 | 11.0 | 11.5 | 12.0 | 0        |
| 10         | 6.1         | 6.6 | 7.1 | 7.6 | 8.1  | 8.6  | 9.1  | 9.6  | 10.2 | 10.7 | 11.2 | 11.7 | 12.2 | 10       |
| 15         | 6.2         | 6.7 | 7.2 | 7.8 | 8.3  | 8.8  | 9.3  | 9.8  | 10.4 | 10.9 | 11.4 | 11.9 | 12.4 | 15       |
| 20         | 6.4         | 6.9 | 7.5 | 8.0 | 8.5  | 9.0  | 9.6  | 10.1 | 10.6 | 11.2 | 11.7 | 12.2 | 12.8 | 20       |
| 25         | 6.6         | 7.2 | 7.7 | 8.3 | 8.8  | 9.4  | 9.9  | 10.5 | 11.0 | 11.6 | 12.2 | 12.7 | 13.3 | 25       |
| 30         | 6.9         | 7.5 | 8.1 | 8.7 | 9.2  | 9.8  | 10.4 | 11.0 | 11.6 | 12.1 | 12.7 | 13.3 | 13.9 | 30       |
| 32         | 7.1         | 7.7 | 8.3 | 8.9 | 9.4  | 10.0 | 10.6 | 11.2 | 11.8 | 12.4 | 13.0 | 13.6 | 14.2 | 32       |
| 34         | 7.2         | 7.8 | 8.5 | 9.1 | 9.7  | 10.3 | 10.9 | 11.5 | 12.1 | 12.7 | 13.3 | 13.9 | 14.5 | 34       |
| 36         | 7.4         | 8.0 | 8.7 | 9.3 | 9.9  | 10.5 | 11.1 | 11.8 | 12.4 | 13.0 | 13.6 | 14.3 | 14.9 | 36       |
| 38         | 7.6         | 8.3 | 8.9 | 9.5 | 10.2 | 10.8 | 11.5 | 12.1 | 12.7 | 13.4 | 14.0 | 14.7 | 15.3 | 38       |

- a) Since the entering values are not whole numbers of declination or latitude, interpolation is required. Locate the bracketing values.

|                       | Declination 11.0° | <b>Declination 11.3°</b> | Declination 11.5° |
|-----------------------|-------------------|--------------------------|-------------------|
| Latitude 25°          | 12.2°             |                          | 12.7°             |
| <b>Latitude 26.8°</b> |                   | <b>Unknown value</b>     |                   |
| Latitude 30°          | 12.7°             |                          | 13.3°             |

- b) Interpolate the bracketing values four ways to the nearest tenth.

|                       | Declination 10.5° | <b>Declination 10.9°</b> | Declination 11° |
|-----------------------|-------------------|--------------------------|-----------------|
| Latitude 25°          | 12.2°             | <b>12.6°</b>             | 12.7°           |
| <b>Latitude 26.8°</b> | <b>12.4°</b>      | <b>Unknown value</b>     | <b>12.9°</b>    |
| Latitude 30°          | 12.7°             | <b>13.2°</b>             | 13.3°           |

- c) Solve the interpolation for the desired value.

|                       | Declination 10.5° | <b>Declination 10.9°</b> | Declination 11° |
|-----------------------|-------------------|--------------------------|-----------------|
| Latitude 25°          | 12.2°             | 12.6°                    | 12.7°           |
| <b>Latitude 26.8°</b> | 12.4°             | <b>12.8°</b>             | 12.9°           |
| Latitude 30°          | 12.7°             | 13.2°                    | 13.3°           |

*\*Note that the amplitude can also be solved directly using the instructions in the Bowditch table 22/27 explanation.*

$$\sin(\text{Amplitude}) = \sec(\text{Latitude}) \times \sin(\text{Declination})$$

-or-

$$\sin(\text{Amplitude}) = \frac{\sin(\text{Declination})}{\cos(\text{Latitude})}$$

## Amplitude Problems

Step 5: Answer required questions.

Since the calculated amplitude is  $12.8^\circ$ , the sun is rising, and the season is summer in the northern hemisphere (e.g. the declination of the body is north), the correct notation for the amplitude is E  $12.8^\circ$  N, and the calculated compass bearing to sunrise should be:

$$090^\circ - 12.8^\circ = 77.2^\circ \text{ T}$$

Therefore, using a compass correction formula, the deviation of the compass is calculated as:

T:  $77.2^\circ$  T (Bearing to sunrise)

V:  $15^\circ$  W (Given)

M:  $092.2^\circ$  (Calculated)

D:

C:  $084^\circ$  psc (Given)

**Deviation =  $8.2^\circ$  E**

## Amplitude Problems

### Amplitude Problems of the Sun on the Visible Horizon

AMP D3. It is 18 August. You have taken an observation of the rising sun when its center is on the visible horizon. The time of observation is 1500 UTC. Your latitude is 52° N.

- What is the amplitude of the sun?
- What true bearing should the sunrise be observed?
- If you actually observe the sun rising at 065° pgc, what is the gyro error?

Answers:

- Amplitude: E 21.4° N
- True bearing: 068.6° T
- Gyro error: 2.6° E

| SUN    |        |      |      |      |
|--------|--------|------|------|------|
| G.M.T. | G.H.A. |      | Dec. |      |
|        |        |      |      |      |
| 12     | 359    | 03.3 | N13  | 02.5 |
| 13     | 14     | 03.4 |      | 01.7 |
| 14     | 29     | 03.6 |      | 00.8 |
| 15     | 44     | 03.7 | 13   | 00.0 |
| 16     | 59     | 03.8 | 12   | 59.2 |
| 17     | 74     | 04.0 |      | 58.4 |

- Step 1: Determine the declination of the sun for the time of observation using the Nautical Almanac.  
The declination at 1500 UTC is N 13° 00'.

- Step 2: Determine the ship's latitude at the time of observation.  
Latitude – 52° N (given)

- Step 3: Enter Table 23/28 in Bowditch with declination and latitude to determine a correction due to the object's location on the visible horizon.

| Correction of Amplitude as Observed on the Visible Horizon |     |     |     |     |     |     |     |     |     |     |     |     |    | Latitude |
|------------------------------------------------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----|----------|
| Declination                                                |     |     |     |     |     |     |     |     |     |     |     |     |    |          |
| 0°                                                         | 2°  | 4°  | 6°  | 8°  | 10° | 12° | 14° | 16° | 18° | 20° | 22° | 24° |    |          |
| °                                                          | °   | °   | °   | °   | °   | °   | °   | °   | °   | °   | °   | °   | °  |          |
| 0.0                                                        | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0  |          |
| 0.1                                                        | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 10 |          |
| 0.2                                                        | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 15 |          |
| 0.3                                                        | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 20 |          |
| 0.3                                                        | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.4 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 25 |          |
| 0.4                                                        | 0.4 | 0.4 | 0.4 | 0.5 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.5 | 0.5 | 30 |          |
| 0.4                                                        | 0.4 | 0.4 | 0.4 | 0.4 | 0.5 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.5 | 0.5 | 32 |          |
| 0.5                                                        | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 34 |          |
| 0.5                                                        | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.6 | 0.5 | 0.6 | 0.6 | 36 |          |
| 0.6                                                        | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 38 |          |
| 0.6                                                        | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.7 | 0.7 | 40 |          |
| 0.6                                                        | 0.6 | 0.6 | 0.6 | 0.6 | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 | 42 |          |
| 0.7                                                        | 0.7 | 0.7 | 0.7 | 0.6 | 0.6 | 0.7 | 0.7 | 0.7 | 0.8 | 0.8 | 0.8 | 0.9 | 44 |          |
| 0.7                                                        | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.9 | 0.9 | 46 |          |
| 0.8                                                        | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.9 | 0.9 | 1.0 | 1.0 | 48 |          |
| 0.8                                                        | 0.8 | 0.8 | 0.8 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 1.0 | 1.0 | 1.0 | 50 |          |
| 0.8                                                        | 0.8 | 0.8 | 0.8 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 1.0 | 1.1 | 1.1 | 1.1 | 51 |          |
| 0.9                                                        | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 1.0 | 1.0 | 1.0 | 1.1 | 1.1 | 1.1 | 52 |          |
| 0.9                                                        | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 1.0 | 1.0 | 1.0 | 1.1 | 1.2 | 1.2 | 53 |          |
| 1.0                                                        | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.1 | 1.1 | 1.1 | 1.2 | 1.2 | 1.3 | 54 |          |

The correction is 1.0° (interpolated between the tabular values for 12° and 14° declination).

- Step 4: Enter Table 22/27 in Bowditch with declination and latitude to determine the amplitude.  
Declination: 13°  
Latitude: 52°

- a) This yields an amplitude of 21.4° or (E 21.4° N).

| Amplitudes |             |      |      |      |      |      |      |      |      |      |      |      |      |          |
|------------|-------------|------|------|------|------|------|------|------|------|------|------|------|------|----------|
| Latitude   | Declination |      |      |      |      |      |      |      |      |      |      |      |      | Latitude |
|            | 12°0        | 12°5 | 13°0 | 13°5 | 14°0 | 14°5 | 15°0 | 15°5 | 16°0 | 16°5 | 17°0 | 17°5 | 18°0 |          |
|            | °           | °    | °    | °    | °    | °    | °    | °    | °    | °    | °    | °    | °    |          |
| 0          | 12.0        | 12.5 | 13.0 | 13.5 | 14.0 | 14.5 | 15.0 | 15.5 | 16.0 | 16.5 | 17.0 | 17.5 | 18.0 | 0        |
| 10         | 12.2        | 12.7 | 13.2 | 13.7 | 14.2 | 14.7 | 15.2 | 15.7 | 16.3 | 16.8 | 17.3 | 17.8 | 18.3 | 10       |
| 15         | 12.4        | 12.9 | 13.5 | 14.0 | 14.5 | 15.0 | 15.5 | 16.1 | 16.6 | 17.1 | 17.6 | 18.1 | 18.7 | 15       |
| 20         | 12.8        | 13.3 | 13.9 | 14.4 | 14.9 | 15.5 | 16.0 | 16.5 | 17.1 | 17.6 | 18.1 | 18.7 | 19.2 | 20       |
| 25         | 13.3        | 13.8 | 14.4 | 14.9 | 15.5 | 16.0 | 16.6 | 17.1 | 17.7 | 18.3 | 18.8 | 19.4 | 19.9 | 25       |
| 30         | 13.9        | 14.5 | 15.1 | 15.6 | 16.2 | 16.8 | 17.4 | 18.0 | 18.6 | 19.1 | 19.7 | 20.3 | 20.9 | 30       |
| 32         | 14.2        | 14.8 | 15.4 | 16.0 | 16.6 | 17.2 | 17.8 | 18.4 | 19.0 | 19.6 | 20.2 | 20.8 | 21.4 | 32       |
| 34         | 14.5        | 15.1 | 15.7 | 16.4 | 17.0 | 17.6 | 18.2 | 18.8 | 19.4 | 20.0 | 20.7 | 21.3 | 21.9 | 34       |
| 36         | 14.9        | 15.5 | 16.1 | 16.8 | 17.4 | 18.0 | 18.7 | 19.3 | 19.9 | 20.6 | 21.2 | 21.8 | 22.5 | 36       |
| 38         | 15.3        | 15.9 | 16.6 | 17.2 | 17.9 | 18.5 | 19.2 | 19.8 | 20.5 | 21.1 | 21.8 | 22.4 | 23.1 | 38       |
| 40         | 15.7        | 16.4 | 17.1 | 17.7 | 18.4 | 19.1 | 19.7 | 20.4 | 21.1 | 21.8 | 22.4 | 23.1 | 23.8 | 40       |
| 41         | 16.0        | 16.7 | 17.3 | 18.0 | 18.7 | 19.4 | 20.1 | 20.8 | 21.4 | 22.1 | 22.8 | 23.5 | 24.2 | 41       |
| 42         | 16.2        | 16.9 | 17.6 | 18.3 | 19.0 | 19.7 | 20.4 | 21.1 | 21.8 | 22.5 | 23.2 | 23.9 | 24.6 | 42       |
| 43         | 16.5        | 17.2 | 17.9 | 18.6 | 19.3 | 20.0 | 20.7 | 21.4 | 22.1 | 22.9 | 23.6 | 24.3 | 25.0 | 43       |
| 44         | 16.8        | 17.5 | 18.2 | 18.9 | 19.7 | 20.4 | 21.1 | 21.8 | 22.5 | 23.3 | 24.0 | 24.7 | 25.4 | 44       |
| 45         | 17.1        | 17.8 | 18.5 | 19.3 | 20.0 | 20.7 | 21.5 | 22.2 | 22.9 | 23.7 | 24.4 | 25.2 | 25.9 | 45       |
| 46         | 17.4        | 18.2 | 18.9 | 19.6 | 20.4 | 21.1 | 21.9 | 22.6 | 23.4 | 24.1 | 24.9 | 25.7 | 26.4 | 46       |
| 47         | 17.7        | 18.5 | 19.3 | 20.0 | 20.8 | 21.5 | 22.3 | 23.1 | 23.8 | 24.6 | 25.4 | 26.2 | 26.9 | 47       |
| 48         | 18.1        | 18.9 | 19.6 | 20.4 | 21.2 | 22.0 | 22.8 | 23.5 | 24.3 | 25.1 | 25.9 | 26.7 | 27.5 | 48       |
| 49         | 18.5        | 19.3 | 20.1 | 20.8 | 21.6 | 22.4 | 23.2 | 24.0 | 24.8 | 25.7 | 26.5 | 27.3 | 28.1 | 49       |
| 50         | 18.9        | 19.7 | 20.5 | 21.3 | 22.1 | 22.9 | 23.7 | 24.6 | 25.4 | 26.2 | 27.1 | 27.9 | 28.7 | 50       |
| 51         | 19.3        | 20.1 | 20.9 | 21.8 | 22.6 | 23.4 | 24.3 | 25.1 | 26.0 | 26.8 | 27.7 | 28.5 | 29.4 | 51       |
| 52         | 19.7        | 20.6 | 21.4 | 22.3 | 23.1 | 24.0 | 24.9 | 25.7 | 26.6 | 27.5 | 28.3 | 29.2 | 30.1 | 52       |
| 53         | 20.2        | 21.1 | 21.9 | 22.8 | 23.7 | 24.6 | 25.5 | 26.4 | 27.3 | 28.2 | 29.1 | 30.0 | 30.9 | 53       |
| 54         | 20.7        | 21.6 | 22.5 | 23.4 | 24.3 | 25.2 | 26.1 | 27.0 | 28.0 | 28.9 | 29.8 | 30.8 | 31.7 | 54       |

## Amplitude Problems

Step 5: Answer required questions.

- a) Due to the object being on the visible horizon, the observation must be corrected.
- Correction from Table 23/28 =  $1.0^\circ$
  - The correction must be applied to the observation (not the amplitude) *away from the elevated (nearest) pole*.
  - In this case, the ship is in the northern hemisphere, so the elevated pole is north. The initial observation is  $065^\circ$  pgc.
  - The corrected observation is  $065^\circ \text{ pgc} + 1.0^\circ = 066^\circ \text{ pgc}$ .
- b) Standard sunrise is  $090^\circ$  T. In the northern hemisphere in spring and summer, the sun rises north of east. Therefore, using the amplitude (E  $21.4^\circ$  N) the calculated sunrise is  $090^\circ - 21.4^\circ = \mathbf{68.6^\circ \text{ T}}$
- c) If the sun (corrected) is observed rising at  $066^\circ$  pgc, while the calculated sunrise is  $68.6^\circ$  T, the gyro error is  $68.6^\circ - 66^\circ = 2.6^\circ$ .
- d) To determine the direction of error, use the mnemonic "Gyro Best, Error West, Gyro Least, Error East." In this case, the gyro is lower (least) than the observation, so the error is  $\mathbf{2.6^\circ \text{ E}}$ .

## Amplitude Problems

AMP D4. On 11 May, in DR position latitude  $37^{\circ} 06.0' \text{ N}$ , longitude  $45^{\circ} 45.0' \text{ W}$ , you observe an amplitude of the Sun. The Sun's center is on the visible horizon and bears  $089^{\circ}$  psc. The chronometer reads 07h 57m 06s and is 1m 48s slow. Variation is  $20.0^{\circ} \text{ W}$ . What is the deviation?

Answer:  $2.3^{\circ} \text{ W}$  deviation.

- Step 1: Determine the actual time of observation.  
 07:57:06 chronometer time of observation  
 00:01:48 slow on GMT  
 07:57:06 + 00:01:48 = 07:58:54 correct chronometer time

$45^{\circ} 45.0' \text{ W}$  corresponds to a zone time of (+3) and the correct GMT is 07:58:54.

- Step 2: Determine the declination of the sun for the time of observation using the Nautical Almanac.

The declination at 07:58:54 is not given in the Nautical Almanac and must be interpolated.

The base value for 0700 is  $\text{N } 17^{\circ} 52.5'$  and increasing.

The  $d$  value for 10-12 May is 0.6.

Enter the Increments and Corrections Page in the Nautical Almanac with the daily  $d$  value and a time of 58 minutes (the difference between the base declination and the observation time).

| SUN               |        |      |          |
|-------------------|--------|------|----------|
| G.M.T.            | G.H.A. |      | Dec.     |
| 06                | 270    | 55.2 | N17 51.8 |
| 07                | 285    | 55.2 | 52.5     |
| 08                | 300    | 55.2 | 53.1     |
| S.D. 15.9 $d$ 0.6 |        |      |          |

| <sup>s</sup><br>58 | SUN<br>PLANETS | ARIES   | MOON    | $\frac{v}{d}$ or Corr <sup>n</sup> | $\frac{v}{d}$ or Corr <sup>n</sup> | $\frac{v}{d}$ or Corr <sup>n</sup> |
|--------------------|----------------|---------|---------|------------------------------------|------------------------------------|------------------------------------|
| 00                 | 14 30.0        | 14 32.4 | 13 50.4 | 0.0 0.0                            | 6.0 5.9                            | 12.0 11.7                          |
| 01                 | 14 30.3        | 14 32.6 | 13 50.6 | 0.1 0.1                            | 6.1 5.9                            | 12.1 11.8                          |
| 02                 | 14 30.5        | 14 32.9 | 13 50.8 | 0.2 0.2                            | 6.2 6.0                            | 12.2 11.9                          |
| 03                 | 14 30.8        | 14 33.1 | 13 51.1 | 0.3 0.3                            | 6.3 6.1                            | 12.3 12.0                          |
| 04                 | 14 31.0        | 14 33.4 | 13 51.3 | 0.4 0.4                            | 6.4 6.2                            | 12.4 12.1                          |
| 05                 | 14 31.3        | 14 33.6 | 13 51.6 | 0.5 0.5                            | 6.5 6.3                            | 12.5 12.2                          |
| 06                 | 14 31.5        | 14 33.9 | 13 51.8 | 0.6 0.6                            | 6.6 6.4                            | 12.6 12.3                          |
| 07                 | 14 31.8        | 14 34.1 | 13 52.0 | 0.7 0.7                            | 6.7 6.5                            | 12.7 12.4                          |
| 08                 | 14 32.0        | 14 34.4 | 13 52.3 | 0.8 0.8                            | 6.8 6.6                            | 12.8 12.5                          |
| 09                 | 14 32.3        | 14 34.6 | 13 52.5 | 0.9 0.9                            | 6.9 6.7                            | 12.9 12.6                          |

Given a  $d$  value of 0.6, the declination correction factor is 0.6.

Since the declination is increasing from hour to hour, the corrected declination for 11 May at 07:58:54 is  $\text{N } 17^{\circ} 52.5' + 0.6' = \underline{\text{N } 17^{\circ} 53.1'}$

- Step 3: Determine the ship's latitude at the time of observation.  
 Latitude –  $37^{\circ} 06' \text{ N}$  (given)
- Step 4: Since the body is observed on the visible horizon, enter Table 23/28 in Bowditch to obtain the Visible Horizon Correction.

## Amplitude Problems

| Correction of Amplitude as Observed on the Visible Horizon |     |     |     |     |     |     |     |     |     |     |     |     |          |
|------------------------------------------------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----------|
| Declination                                                |     |     |     |     |     |     |     |     |     |     |     |     | Latitude |
| 0°                                                         | 2°  | 4°  | 6°  | 8°  | 10° | 12° | 14° | 16° | 18° | 20° | 22° | 24° |          |
| °                                                          | °   | °   | °   | °   | °   | °   | °   | °   | °   | °   | °   | °   | °        |
| 0.0                                                        | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0        |
| 0.1                                                        | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 10       |
| 0.2                                                        | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 15       |
| 0.3                                                        | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 20       |
| 0.3                                                        | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.4 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 25       |
| 0.4                                                        | 0.4 | 0.4 | 0.4 | 0.4 | 0.5 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.5 | 0.5 | 30       |
| 0.4                                                        | 0.4 | 0.4 | 0.4 | 0.4 | 0.5 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.5 | 0.5 | 32       |
| 0.5                                                        | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 34       |
| 0.5                                                        | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.6 | 0.5 | 0.6 | 0.6 | 36       |
| 0.6                                                        | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 38       |

By visual inspection, the correction is  $0.6^\circ$ .

Per the instructions at the bottom of the table, for the Sun, the correction is always applied away from the elevated pole and it is applied to the observed bearing and not to the Amplitude. Since the observer is in the northern hemisphere, the north pole is the elevated pole. Since the Sun is rising, the correction should be added.

Observed:  $089^\circ$  psc

Table 23/28 Correction:  $+0.6^\circ$

Total:  $089^\circ + 0.6^\circ = \underline{089.6^\circ}$  psc

Step 5: Enter Table 22/27 in Bowditch with declination (in tenths notation) and latitude to determine the amplitude.

Declination: N  $17^\circ 53.1'$  = N  $17.9^\circ$

Latitude:  $37^\circ 06.0'$  N =  $37.1^\circ$  N

| Amplitudes |             |      |      |      |      |      |      |      |      |      |      |      |      |          |
|------------|-------------|------|------|------|------|------|------|------|------|------|------|------|------|----------|
| Latitude   | Declination |      |      |      |      |      |      |      |      |      |      |      |      | Latitude |
|            | 12°0        | 12°5 | 13°0 | 13°5 | 14°0 | 14°5 | 15°0 | 15°5 | 16°0 | 16°5 | 17°0 | 17°5 | 18°0 |          |
| °          | °           | °    | °    | °    | °    | °    | °    | °    | °    | °    | °    | °    | °    | °        |
| 0          | 12.0        | 12.5 | 13.0 | 13.5 | 14.0 | 14.5 | 15.0 | 15.5 | 16.0 | 16.5 | 17.0 | 17.5 | 18.0 | 0        |
| 10         | 12.2        | 12.7 | 13.2 | 13.7 | 14.2 | 14.7 | 15.2 | 15.7 | 16.3 | 16.8 | 17.3 | 17.8 | 18.3 | 10       |
| 15         | 12.4        | 12.9 | 13.5 | 14.0 | 14.5 | 15.0 | 15.5 | 16.1 | 16.6 | 17.1 | 17.6 | 18.1 | 18.7 | 15       |
| 20         | 12.8        | 13.3 | 13.9 | 14.4 | 14.9 | 15.5 | 16.0 | 16.5 | 17.1 | 17.6 | 18.1 | 18.7 | 19.2 | 20       |
| 25         | 13.3        | 13.8 | 14.4 | 14.9 | 15.5 | 16.0 | 16.6 | 17.1 | 17.7 | 18.3 | 18.8 | 19.4 | 19.9 | 25       |
| 30         | 13.9        | 14.5 | 15.1 | 15.6 | 16.2 | 16.8 | 17.4 | 18.0 | 18.6 | 19.1 | 19.7 | 20.3 | 20.9 | 30       |
| 32         | 14.2        | 14.8 | 15.4 | 16.0 | 16.6 | 17.2 | 17.8 | 18.4 | 19.0 | 19.6 | 20.2 | 20.8 | 21.4 | 32       |
| 34         | 14.5        | 15.1 | 15.7 | 16.4 | 17.0 | 17.6 | 18.2 | 18.8 | 19.4 | 20.0 | 20.7 | 21.3 | 21.9 | 34       |
| 36         | 14.9        | 15.5 | 16.1 | 16.8 | 17.4 | 18.0 | 18.7 | 19.3 | 19.9 | 20.6 | 21.2 | 21.8 | 22.5 | 36       |
| 38         | 15.3        | 15.9 | 16.6 | 17.2 | 17.9 | 18.5 | 19.2 | 19.8 | 20.5 | 21.1 | 21.8 | 22.4 | 23.1 | 38       |

## Amplitude Problems

- a) Since the entering values are not whole numbers of declination or latitude, interpolation is required. Locate the bracketing values.

|      |      |
|------|------|
| 21.8 | 22.5 |
| 22.4 | 23.1 |

|                       | Declination 17.5° | <b>Declination 17.9°</b> | Declination 18.0° |
|-----------------------|-------------------|--------------------------|-------------------|
| Latitude 36°          | 21.8°             |                          | 22.5°             |
| <b>Latitude 37.1°</b> |                   | <b>Unknown value</b>     |                   |
| Latitude 38°          | 22.4°             |                          | 23.1°             |

- b) Interpolate the bracketing values four ways to the nearest tenth.

|                       | Declination 17.5° | <b>Declination 17.9°</b> | Declination 18.0° |
|-----------------------|-------------------|--------------------------|-------------------|
| Latitude 36°          | 21.8°             | <b>22.4°</b>             | 22.5°             |
| <b>Latitude 37.1°</b> | <b>22.0°</b>      | <b>Unknown value</b>     | <b>22.6°</b>      |
| Latitude 38°          | 22.4°             | <b>23.0°</b>             | 23.1°             |

- c) Solve the final interpolation for the desired value.

|                       | Declination 17.5° | <b>Declination 17.9°</b> | Declination 18.0° |
|-----------------------|-------------------|--------------------------|-------------------|
| Latitude 36°          | 21.8°             | 22.4°                    | 22.5°             |
| <b>Latitude 37.1°</b> | 22.0°             | <b>22.7°</b>             | 22.6°             |
| Latitude 38°          | 22.4°             | 23.0°                    | 23.1°             |

\*Note that the amplitude can also be solved directly using the instructions in the Bowditch table 22/27 explanation.

$$\sin(\text{Amplitude}) = \sec(\text{Latitude}) \times \sin(\text{Declination})$$

-or-

$$\sin(\text{Amplitude}) = \left( \frac{\sin(\text{Declination})}{\cos(\text{Latitude})} \right)$$

Step 6: Answer required questions.

Since the calculated amplitude is 22.7°, the sun is rising, and the season is spring in the northern hemisphere, the correct notation for the amplitude is E 22.7° N, and the calculated compass bearing to sunrise should be:  
 $090^\circ - 22.7^\circ = 67.3^\circ \text{ T}$

Therefore, using a compass correction formula, the deviation of the compass is calculated as:

T: 67.3° T (Bearing to sunrise)

V: 20° W (Given)

M: 087.3° (Calculated)

D:

C: 089.6° psc (Given and then corrected for visible horizon using Table 23/28)

**Deviation = 2.3° W**



## Amplitude Problems

### Amplitude Problems of the Moon

- **Celestial Horizon:** Moon amplitude problems are calculated exactly like Sun problems when the moon is on the celestial horizon (e.g. when the upper limb is on the visible horizon).
- **Visible Horizon:** When the Moon's center is on the visible horizon, a correction is required. Moon amplitude problems are calculated differently than Sun problems when a Table 23/28 correction is required. Instead of the correction being applied away from the elevated pole (like the sun), the correction is applied such that half of the value is applied toward the elevated pole.

AMP D5. At 1524 ZT on 14 June in DR position latitude  $30^{\circ} 51' N$ , longitude  $30^{\circ} 02' W$ , you observe an amplitude of the Moon. The center of the Moon is on the visible horizon and bears  $103.9$  pgc. The variation is  $10^{\circ} W$ . What is the gyro error?

Answer:  $2.0^{\circ} E$ .

- Step 1: Determine the actual time of observation.  
1524 chronometer time of observation

$30^{\circ} 02' W$  corresponds to a zone time of (+2), and the correct GMT is 1724.

- Step 2: Determine the declination of the Moon for the time of observation using the Nautical Almanac.

The declination at 1724 is not given in the Nautical Almanac and must be interpolated.

The base value for 1700 is  $S 13^{\circ} 22.6'$  and increasing.  
The  $d$  value for the hour is  $14.7$ .

Enter the Increments and Corrections Page in the Nautical Almanac with the daily  $d$  value and a time of 24 minutes (the difference between the base declination and the observation time).

Given a  $d$  value of  $14.7$  the declination correction is  $6.0'$ .

Since the declination is increasing from hour to hour, the corrected declination for 14 June at 1724 is  $S 13^{\circ} 22.6' + 6.0' = \underline{S 13^{\circ} 28.6'}$

| G.M.T. | SUN      |      |      | MOON     |       |           |     |      |
|--------|----------|------|------|----------|-------|-----------|-----|------|
|        | G.H.A.   | Dec. |      | G.H.A.   | $\nu$ | Dec.      | $d$ | H.P. |
| 12     | 359 57.5 | N 23 | 16.3 | 214 55.5 | 14.4  | S 12 40.0 | 8.6 | 54.0 |
| 13     | 14 57.4  | 16.5 |      | 229 28.9 | 14.5  | 12 48.6   | 8.6 | 54.0 |
| 14     | 29 57.2  | 16.6 |      | 244 02.4 | 14.3  | 12 57.2   | 8.5 | 54.1 |
| 15     | 44 57.1  | 16.7 |      | 258 35.7 | 14.4  | 13 05.7   | 8.5 | 54.1 |
| 16     | 59 57.0  | 16.8 |      | 273 09.1 | 14.3  | 13 14.2   | 8.4 | 54.1 |
| 17     | 74 56.8  | 16.9 |      | 287 42.4 | 14.2  | 13 22.6   | 8.4 | 54.1 |

## Amplitude Problems

Step 3: Determine the ship's latitude at the time of observation.

Latitude – 30° 51' N (given)

Step 4: Since the body is observed on the visible horizon, enter Table 23/28 in Bowditch to obtain the Visible Horizon Correction for the Moon.

| Correction of Amplitude as Observed on the Visible Horizon |     |     |     |     |     |     |     |     |     |     |     |     |          |
|------------------------------------------------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----------|
| Declination                                                |     |     |     |     |     |     |     |     |     |     |     |     | Latitude |
| 0°                                                         | 2°  | 4°  | 6°  | 8°  | 10° | 12° | 14° | 16° | 18° | 20° | 22° | 24° |          |
| °                                                          | °   | °   | °   | °   | °   | °   | °   | °   | °   | °   | °   | °   | °        |
| 0.0                                                        | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0        |
| 0.1                                                        | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 10       |
| 0.2                                                        | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 15       |
| 0.3                                                        | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 20       |
| 0.3                                                        | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.4 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 25       |
| 0.4                                                        | 0.4 | 0.4 | 0.4 | 0.5 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.5 | 0.5 | 30       |
| 0.4                                                        | 0.4 | 0.4 | 0.4 | 0.5 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.5 | 0.5 | 0.5 | 32       |
| 0.5                                                        | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 34       |
| 0.5                                                        | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.6 | 0.5 | 0.6 | 0.6 | 0.6 | 36       |
| 0.6                                                        | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 38       |

By visual inspection, the correction is 0.4°.

Per the instructions at the bottom of the table, for the Moon, the correction is always divided in 2 and applied toward the elevated pole. Since the observer is in the northern hemisphere, the north pole is the elevated pole. Since the Moon is rising, the correction should be subtracted.

Observed: 103.9° pgc  
 Table 23 Correction: - 0.2°  
 Total: 103.9° - 0.2° = 103.7°  
 pgc

Step 5: Enter Table 22/27 in Bowditch with declination (in tenths notation) and latitude to determine the amplitude.  
 Declination: S 13° 26.0' = N 13.4°  
 Latitude: 30° 51' N = 30.9° N

| Amplitudes |             |      |      |      |      |      |      |      |      |      |      |      |      |          |
|------------|-------------|------|------|------|------|------|------|------|------|------|------|------|------|----------|
| Latitude   | Declination |      |      |      |      |      |      |      |      |      |      |      |      | Latitude |
|            | 12°0        | 12°5 | 13°0 | 13°5 | 14°0 | 14°5 | 15°0 | 15°5 | 16°0 | 16°5 | 17°0 | 17°5 | 18°0 |          |
| °          | °           | °    | °    | °    | °    | °    | °    | °    | °    | °    | °    | °    | °    | °        |
| 0          | 12.0        | 12.5 | 13.0 | 13.5 | 14.0 | 14.5 | 15.0 | 15.5 | 16.0 | 16.5 | 17.0 | 17.5 | 18.0 | 0        |
| 10         | 12.2        | 12.7 | 13.2 | 13.7 | 14.2 | 14.7 | 15.2 | 15.7 | 16.3 | 16.8 | 17.3 | 17.8 | 18.3 | 10       |
| 15         | 12.4        | 12.9 | 13.5 | 14.0 | 14.5 | 15.0 | 15.5 | 16.1 | 16.6 | 17.1 | 17.6 | 18.1 | 18.7 | 15       |
| 20         | 12.8        | 13.3 | 13.9 | 14.4 | 14.9 | 15.5 | 16.0 | 16.5 | 17.1 | 17.6 | 18.1 | 18.7 | 19.2 | 20       |
| 25         | 13.3        | 13.8 | 14.4 | 14.9 | 15.5 | 16.0 | 16.6 | 17.1 | 17.7 | 18.3 | 18.8 | 19.4 | 19.9 | 25       |
| 30         | 13.9        | 14.5 | 15.1 | 15.6 | 16.2 | 16.8 | 17.4 | 18.0 | 18.6 | 19.1 | 19.7 | 20.3 | 20.9 | 30       |
| 32         | 14.2        | 14.8 | 15.4 | 16.0 | 16.6 | 17.2 | 17.8 | 18.4 | 19.0 | 19.6 | 20.2 | 20.8 | 21.4 | 32       |
| 34         | 14.5        | 15.1 | 15.7 | 16.4 | 17.0 | 17.6 | 18.2 | 18.8 | 19.4 | 20.0 | 20.7 | 21.3 | 21.9 | 34       |
| 36         | 14.9        | 15.5 | 16.1 | 16.8 | 17.4 | 18.0 | 18.7 | 19.3 | 19.9 | 20.6 | 21.2 | 21.8 | 22.5 | 36       |
| 38         | 15.3        | 15.9 | 16.6 | 17.2 | 17.9 | 18.5 | 19.2 | 19.8 | 20.5 | 21.1 | 21.8 | 22.4 | 23.1 | 38       |

## Amplitude Problems

- a) Since the entering values are not whole numbers of declination or latitude, interpolation is required. Locate the bracketing values.

|      |      |
|------|------|
| 15.1 | 15.6 |
| 15.4 | 16.0 |

|                       | Declination 13.0° | <b>Declination 13.4°</b> | Declination 13.5° |
|-----------------------|-------------------|--------------------------|-------------------|
| Latitude 30°          | 15.1°             |                          | 15.6°             |
| <b>Latitude 30.9°</b> |                   | <b>Unknown value</b>     |                   |
| Latitude 32°          | 15.4°             |                          | 16.0°             |

- b) Interpolate the bracketing values four ways to the nearest tenth.

|                       | Declination 13.0° | <b>Declination 13.4°</b> | Declination 13.5° |
|-----------------------|-------------------|--------------------------|-------------------|
| Latitude 30°          | 15.1°             | <b>15.5°</b>             | 15.6°             |
| <b>Latitude 30.9°</b> | <b>15.2°</b>      | <b>Unknown value</b>     | <b>15.8°</b>      |
| Latitude 32°          | 15.4°             | <b>15.9°</b>             | 16.0°             |

- c) Solve the interpolation for the desired value.

|                       | Declination 13.0° | <b>Declination 13.4°</b> | Declination 13.5° |
|-----------------------|-------------------|--------------------------|-------------------|
| Latitude 30°          | 15.1°             | 15.5°                    | 15.6°             |
| <b>Latitude 30.9°</b> | 15.2°             | <b>15.7°</b>             | 15.8°             |
| Latitude 32°          | 15.4°             | 15.9°                    | 16.0°             |

*\*Note that the amplitude can also be solved directly using the instructions in the Bowditch table 22 explanation.*

$$\sin(\text{Amplitude}) = \sec(\text{Latitude}) \times \sin(\text{Declination})$$

-or-

$$\sin(\text{Amplitude}) = \left( \frac{\sin(\text{Declination})}{\cos(\text{Latitude})} \right)$$

Step 6: Answer required questions.

Since the calculated amplitude is 15.7°, the Moon is rising, and the declination is south, the correct notation for the amplitude is E 15.7° S, and the calculated compass bearing to moonrise should be:

$$090^\circ + 15.7^\circ = 105.7^\circ \text{ T}$$

Therefore, using a gyro error calculation, the gyro error is:

G: 103.7° pgc (Given)

E:

T: 105.7° T (Calculated)

**Gyro Error = 2.0° E**

## Amplitude Problems

### Amplitude Problems of Planets

- Amplitudes of Planets are completed in the same manner as those for the sun. Planets are on the celestial horizon when they are approximately one sun diameter above the visible horizon.

AMP D6. At 2043 ZT on 13 October in DR position latitude  $43^{\circ} 57.3' S$ , longitude  $147^{\circ} 16.0' E$ , you observe an amplitude of Venus. The planet is about one sun's diameter above the horizon and bears  $236.2^{\circ}$  pgc. The variation is  $15^{\circ} E$ . What is the gyro error?

Answer:  $0.0^{\circ}$ .

Step 1: Determine the actual time of observation.  
2043 chronometer time of observation

$147^{\circ} 16.0' E$  corresponds to a zone time of  $(-10)$ , and the correct GMT is 1043 on 13 October.

Step 2: Determine the declination of the planet for the time of observation using the Nautical Almanac.

The declination at 1043 is not given in the Nautical Almanac and must be interpolated.

The base value for 1000 is  $S 23^{\circ} 36.3'$  and increasing.

The  $d$  value for 13 October is 0.6.

|            | ARIES  |      | VENUS $-3.8$ |          |
|------------|--------|------|--------------|----------|
| G.M.T.     | G.H.A. |      | G.H.A.       | Dec.     |
| 06         | 111    | 42.7 | 229 23.3     | S23 33.7 |
| 07         | 126    | 45.2 | 244 22.8     | 34.3     |
| 08         | 141    | 47.7 | 259 22.3     | 35.0     |
| 09         | 156    | 50.1 | 274 21.8     | 35.6     |
| 10         | 171    | 52.6 | 289 21.3     | 36.3     |
| 11         | 186    | 55.1 | 304 20.8     | 36.9     |
| <hr/>      |        |      |              |          |
|            | h m    |      | v            | d        |
| Ver. Pass. | 22     | 26.5 | $-0.5$       | 0.6      |

| <sup>m</sup><br>43 | SUN<br>PLANETS | ARIES   | MOON    | $\frac{v}{d}$ or Corr <sup>n</sup> | $\frac{v}{d}$ or Corr <sup>n</sup> | $\frac{v}{d}$ or Corr <sup>n</sup> |
|--------------------|----------------|---------|---------|------------------------------------|------------------------------------|------------------------------------|
| s                  | o' "           | o' "    | "' "    | "' "                               | "' "                               | "' "                               |
| 00                 | 10 45.0        | 10 46.8 | 10 15.6 | 0.0 0.0                            | 6.0 4.4                            | 12.0 8.7                           |
| 01                 | 10 45.3        | 10 47.0 | 10 15.9 | 0.1 0.1                            | 6.1 4.4                            | 12.1 8.8                           |
| 02                 | 10 45.5        | 10 47.3 | 10 16.1 | 0.2 0.1                            | 6.2 4.5                            | 12.2 8.8                           |
| 03                 | 10 45.8        | 10 47.5 | 10 16.3 | 0.3 0.2                            | 6.3 4.6                            | 12.3 8.9                           |
| 04                 | 10 46.0        | 10 47.8 | 10 16.6 | 0.4 0.3                            | 6.4 4.6                            | 12.4 9.0                           |
| 05                 | 10 46.3        | 10 48.0 | 10 16.8 | 0.5 0.4                            | 6.5 4.7                            | 12.5 9.1                           |
| 06                 | 10 46.5        | 10 48.3 | 10 17.0 | 0.6 0.4                            | 6.6 4.8                            | 12.6 9.1                           |
| 07                 | 10 46.8        | 10 48.5 | 10 17.3 | 0.7 0.5                            | 6.7 4.9                            | 12.7 9.2                           |
| 08                 | 10 47.0        | 10 48.8 | 10 17.5 | 0.8 0.6                            | 6.8 4.9                            | 12.8 9.3                           |
| 09                 | 10 47.3        | 10 49.0 | 10 17.8 | 0.9 0.7                            | 6.9 5.0                            | 12.9 9.4                           |

Enter the Increments and Corrections Page in the Nautical Almanac with the daily  $d$  value and a time of 43 minutes (the difference between the base declination and the observation time).

Given a  $d$  value of 0.6 the declination correction is  $0.4'$ .

Since the declination is increasing from hour to hour, the corrected declination for 13 October at 1043 is  $S 23^{\circ} 36.3' + 0.4' = \underline{S 23^{\circ} 36.7'}$

## Amplitude Problems

Step 3: Determine the ship's latitude at the time of observation.

Latitude – 43° 57.3' S (given)

Step 4: Enter Table 22 in Bowditch with declination (in tenths notation) and latitude to determine the amplitude.

Declination: S 23° 36.7' = S 23.6°

Latitude: 43° 57.3' S = 43.96° S

- a) Since the entering values are not whole numbers of declination or latitude, interpolation is required.

| Latitude | Declination |      |      |      |      |      |      |      |      |      |      |      |      |    | Latitude |
|----------|-------------|------|------|------|------|------|------|------|------|------|------|------|------|----|----------|
|          | 18°0        | 18°5 | 19°0 | 19°5 | 20°0 | 20°5 | 21°0 | 21°5 | 22°0 | 22°5 | 23°0 | 23°5 | 24°0 |    |          |
|          | *           | *    | *    | *    | *    | *    | *    | *    | *    | *    | *    | *    | *    |    |          |
| 0        | 18.0        | 18.5 | 19.0 | 19.5 | 20.0 | 20.5 | 21.0 | 21.5 | 22.0 | 22.5 | 23.0 | 23.5 | 24.0 | 0  |          |
| 10       | 18.3        | 18.8 | 19.3 | 19.8 | 20.3 | 20.8 | 21.3 | 21.8 | 22.4 | 22.9 | 23.4 | 23.9 | 24.4 | 10 |          |
| 15       | 18.7        | 19.2 | 19.7 | 20.2 | 20.7 | 21.3 | 21.8 | 22.3 | 22.8 | 23.3 | 23.9 | 24.4 | 24.9 | 15 |          |
| 20       | 19.2        | 19.7 | 20.3 | 20.8 | 21.3 | 21.9 | 22.4 | 23.0 | 23.5 | 24.0 | 24.6 | 25.1 | 25.6 | 20 |          |
| 25       | 19.9        | 20.5 | 21.1 | 21.6 | 22.2 | 22.7 | 23.3 | 23.9 | 24.4 | 25.0 | 25.5 | 26.1 | 26.7 | 25 |          |
| 30       | 20.9        | 21.5 | 22.1 | 22.7 | 23.3 | 23.9 | 24.4 | 25.0 | 25.6 | 26.2 | 26.8 | 27.4 | 28.0 | 30 |          |
| 32       | 21.4        | 22.0 | 22.6 | 23.2 | 23.8 | 24.4 | 25.0 | 25.6 | 26.2 | 26.8 | 27.4 | 28.0 | 28.7 | 32 |          |
| 34       | 21.9        | 22.5 | 23.1 | 23.7 | 24.4 | 25.0 | 25.6 | 26.2 | 26.9 | 27.5 | 28.1 | 28.7 | 29.4 | 34 |          |
| 36       | 22.5        | 23.1 | 23.7 | 24.4 | 25.0 | 25.7 | 26.3 | 26.9 | 27.6 | 28.2 | 28.9 | 29.5 | 30.2 | 36 |          |
| 38       | 23.1        | 23.7 | 24.4 | 25.1 | 25.7 | 26.4 | 27.1 | 27.7 | 28.4 | 29.1 | 29.7 | 30.4 | 31.1 | 38 |          |
| 40       | 23.8        | 24.5 | 25.2 | 25.8 | 26.5 | 27.2 | 27.9 | 28.6 | 29.3 | 30.0 | 30.7 | 31.4 | 32.1 | 40 |          |
| 41       | 24.2        | 24.9 | 25.6 | 26.3 | 26.9 | 27.6 | 28.3 | 29.1 | 29.8 | 30.5 | 31.2 | 31.9 | 32.6 | 41 |          |
| 42       | 24.6        | 25.3 | 26.0 | 26.7 | 27.4 | 28.1 | 28.8 | 29.5 | 30.3 | 31.0 | 31.7 | 32.5 | 33.2 | 42 |          |
| 43       | 25.0        | 25.7 | 26.4 | 27.2 | 27.9 | 28.6 | 29.3 | 30.1 | 30.8 | 31.6 | 32.3 | 33.0 | 33.8 | 43 |          |
| 44       | 25.4        | 26.2 | 26.9 | 27.6 | 28.4 | 29.1 | 29.9 | 30.6 | 31.4 | 32.1 | 32.9 | 33.7 | 34.4 | 44 |          |

- b) Locate the bracketing values.

|      |      |
|------|------|
| 33.0 | 33.8 |
| 33.7 | 34.4 |

|                        | Declination 23.5° | Declination 23.6°    | Declination 24° |
|------------------------|-------------------|----------------------|-----------------|
| Latitude 43°           | 33.0°             |                      | 33.8°           |
| <b>Latitude 43.95°</b> |                   | <b>Unknown value</b> |                 |
| Latitude 44°           | 33.7°             |                      | 34.4°           |

- c) Interpolate the bracketing values four ways to the nearest tenth.

|                        | Declination 23.5° | Declination 23.6°    | Declination 24° |
|------------------------|-------------------|----------------------|-----------------|
| Latitude 43°           | 33.0°             | <b>33.2°</b>         | 33.8°           |
| <b>Latitude 43.95°</b> | <b>33.7°</b>      | <b>Unknown value</b> | <b>34.4°</b>    |
| Latitude 44°           | 33.7°             | <b>33.8°</b>         | 34.4°           |

- d) Solve the interpolation for the desired value.

|                        | Declination 23.5° | Declination 23.6° | Declination 24° |
|------------------------|-------------------|-------------------|-----------------|
| Latitude 43°           | 33.0°             | 33.2°             | 33.8°           |
| <b>Latitude 43.95°</b> | 33.7°             | <b>33.8°</b>      | 34.4°           |
| Latitude 44°           | 33.7°             | 33.8°             | 34.4°           |

*\*Note that the amplitude can also be solved directly using the instructions in the Bowditch table 22 explanation.*

$$\sin(\text{Amplitude}) = \sec(\text{Latitude}) \times \sin(\text{Declination})$$

-or-

$$\sin(\text{Amplitude}) = \left( \frac{\sin(\text{Declination})}{\cos(\text{Latitude})} \right)$$

## Amplitude Problems

Step 5: Answer required questions.

Since the calculated amplitude is  $33.8^\circ$ , the planet is setting, and the declination is south, the correct notation for the amplitude is W  $33.8^\circ$  S, and the calculated compass bearing to planet-set should be:

$$270^\circ - 33.8^\circ = 236.2^\circ \text{ T}$$

Therefore, using a gyro error calculation, the gyro error is:

G:  $236.2^\circ$  pgc (Given)

E:

T:  $236.2^\circ$  T (Calculated)

**Gyro Error =  $0.0^\circ$**

## Amplitude Problems

### Basic Concept Problems (non-USCG exams)

AMP B1. Using the Amplitude Table in Bowditch, you have determined that the calculated amplitude of the sun is 10 degrees. It is August 15<sup>th</sup> and you are in the northern hemisphere. What is the calculated bearing of sunrise and sunset?

**Answer: Sunrise – 080° T, Sunset – 280° T.**

AMP B2. Using the Amplitude Table in Bowditch, you have determined that the calculated amplitude of the sun is 3 degrees. It is October 23<sup>rd</sup> and you are in the northern hemisphere. What is the calculated bearing of sunrise and sunset?

**Answer: Sunrise – 093° T, Sunset 267° T.**

AMP B3. Using the Amplitude Table in Bowditch, you have determined that the calculated amplitude of the sun is 20 degrees. It is August 15<sup>th</sup> and you are in the southern hemisphere. What is the calculated bearing of sunrise and sunset?

**Answer: Sunrise – 070° T, Sunset – 290° T.**

AMP B4. Your latitude is 10N. The declination of the sun is 12 degrees. What is the amplitude of the sun?

**Answer: 12.2 degrees.**

### Amplitudes of the Sun (Celestial Horizon)

AMP B5. On 10 August your vessel's 0426 zone time DR position is latitude  $52^{\circ} 07' N$ , longitude  $142^{\circ} 16' E$ , when an amplitude of the Sun is observed. The Sun's lower limb is about 20 minutes of arc above the visible horizon and bears  $074.5^{\circ}$  per standard compass. Variation in the area is  $12^{\circ} W$ . The chronometer reads 07h 24m 19s and is 2m 34s fast. Which of the following is the deviation of the standard compass?

- a)  $0.0^{\circ}$
- b)  $1.3^{\circ} W$
- c)  **$1.3^{\circ} E$  – correct**
- d)  $2.3^{\circ} W$

AMP B6. On 10 February in DR position latitude  $25^{\circ} 32.0' N$ , longitude  $135^{\circ} 15.0' E$ , you observe an amplitude of the Sun. The Sun's center is on the celestial horizon and bears  $109^{\circ}$  psc. The chronometer reads 09h 43m 25s and is 3m 20s fast. Variation in the area is  $4.5^{\circ} W$ . What is the deviation of the standard magnetic compass?

- a)  **$1.6^{\circ} E$  – correct**
- b)  $2.9^{\circ} W$
- c)  $10.5^{\circ} E$
- d)  $30.5^{\circ} W$

AMP B7. On 11 January, your vessel's 0655 zone time DR position is latitude  $24^{\circ} 30' N$ , longitude  $122^{\circ} 02' W$ , when an amplitude of the Sun is observed. The Sun's center is on the celestial horizon and bears  $101^{\circ}$  per standard compass. Variation in the area is  $11.6^{\circ} E$ . The chronometer reads 02h 52m 48s and is 2m 12s slow. What is the deviation of the standard compass?

- a)  **$1.4^{\circ} E$  – correct**
- b)  $1.4^{\circ} W$
- c)  $4.6^{\circ} E$
- d)  $4.6^{\circ} W$

AMP B8. On 17 April your vessel's position is latitude  $21^{\circ} 00' S$ , longitude  $78^{\circ} 30' W$ , when an amplitude of the Sun is observed. The Sun's center is on the celestial horizon and bears  $082.7^{\circ}$  per standard magnetic compass. Variation in the area is  $2.0^{\circ} W$ . The chronometer reads 10h 59m 24s and is 01m 24s fast. What is the deviation on the compass?

- a)  **$2.0^{\circ} W$ - correct**
- b)  $3.0^{\circ} W$
- c)  $2.5^{\circ} E$
- d)  $3.0^{\circ} E$



### Amplitudes of the Sun (Visible Horizon)

AMP B9. On 10 June your vessel's 0519 zone time DR position is latitude  $27^{\circ} 07.0' N$ , longitude  $92^{\circ} 10.0' W$ , when an amplitude of the Sun is observed. The Sun's center is on the visible horizon and bears  $063.6^{\circ}$  per standard magnetic compass. The variation in the area is  $4.8^{\circ} E$ . The chronometer reads 11h 17m 32s and is 1m 18s slow. What is the deviation of the compass?

- a)  $5.6^{\circ} E$
- b)  $4.8^{\circ} E$
- c)  $4.2^{\circ} W$
- d)  **$4.8^{\circ} W$ - correct**

AMP B10. On 16 April in DR position latitude  $28^{\circ} 07.0' N$ , longitude  $81^{\circ} 47.0' W$ , you observe an amplitude of the Sun. The Sun's center is on the visible horizon and bears  $073.5^{\circ}$  psc. The chronometer reads 10h 53m 41s and is 2m 23s slow. Variation in the area is  $11^{\circ} E$ . What is the deviation of the magnetic compass?

- a)  $4.5^{\circ} E$
- b)  $4.9^{\circ} W$
- c)  $6.1^{\circ} E$
- d)  **$6.5^{\circ} W$ - correct**

AMP B11. On 5 September in DR position latitude  $23^{\circ} 17.0' S$ , longitude  $154^{\circ} 35.0' E$ , you observe an amplitude of the Sun. The Sun's center is on the visible horizon and bears  $275^{\circ}$  per standard magnetic compass. The chronometer reads 7h 49m 26s and is 1m 52s fast. Variation in the area is  $3^{\circ} W$ . What is the deviation of the standard magnetic compass?

- a)  $2.1^{\circ} E$
- b)  $2.4^{\circ} W$
- c)  **$5.1^{\circ} E$ - correct**
- d)  $5.4^{\circ} W$

AMP B12. On 20 June your vessel's 1955 ZT DR position is latitude  $52^{\circ} 38.9' N$ , longitude  $3^{\circ} 42.7' E$ , when an amplitude of the Sun is observed. The Sun's center is on the visible horizon and bears  $311^{\circ}$  per gyrocompass. Variation in the area is  $6^{\circ} W$ . At the time of the observation, the helmsman noted that she was heading  $352^{\circ}$  per gyrocompass and  $358^{\circ}$  per steering compass. What is the gyro error and deviation for that heading?

- a)  $1.3^{\circ} W$  gyro error,  $1.3^{\circ} E$  deviation
- b)  $0.0^{\circ}$  gyro error,  $0.0^{\circ}$  deviation
- c)  $1.3^{\circ} W$  gyro error,  $1.3^{\circ} W$  deviation
- d)  **$1.3^{\circ} E$  gyro error,  $1.3^{\circ} E$  deviation – correct**

### Amplitudes of the Moon

AMP B13. At 1502 ZT on 4 August, in DR position latitude  $11^{\circ} 21.6' S$ , longitude  $088^{\circ} 14.3' E$ , you observe an amplitude of the Moon. The upper limb of the Moon is on the visible horizon and bears  $289^{\circ}$  psc. The variation is  $15^{\circ} W$ . What is the deviation?

- a)  $1.1^{\circ} E$
- b)  $1.1^{\circ} W$  – correct**
- c)  $1.9^{\circ} E$
- d)  $1.9^{\circ} W$

AMP B14. At 1318 ZT on 10 September, in DR position latitude  $24^{\circ} 05.8' N$ , longitude  $058^{\circ} 08.3' E$ , you observe an amplitude of the Moon. The upper limb of the Moon is on the visible horizon and bears  $254^{\circ}$  psc. Variation is  $2^{\circ} W$ . What is the deviation?

- a)  $8.0^{\circ} W$
- b)  $8.0^{\circ} E$
- c)  $4.0^{\circ} W$  – correct**
- d)  $4.0^{\circ} E$

AMP B15. At 1337 ZT on July 17, in DR position latitude  $30^{\circ} 56.8' S$ , longitude  $039^{\circ} 36.5' W$ , you observe an amplitude of the Moon. The upper limb of the Moon is on the visible horizon bearing  $263^{\circ}$  psc. The variation is  $20^{\circ} W$ . What is the deviation?

- a)  $2.6^{\circ} E$
- b)  $2.6^{\circ} W$
- c)  $3.6^{\circ} E$  – correct**
- d)  $3.6^{\circ} W$

AMP B16. At 1542 ZT on 23 October, in DR position latitude  $37^{\circ} 28.5' N$ , longitude  $156^{\circ} 17.3' E$ , you observe an amplitude of the Moon. The center of the Moon is on the visible horizon and bears  $282.5^{\circ}$  psc. The variation is  $0.0^{\circ}$ . What is the deviation?

- a)  $2.2^{\circ} E$  – correct**
- b)  $2.2^{\circ} W$
- c)  $1.2^{\circ} E$
- d)  $1.2^{\circ} W$

AMP B17. At 1523 ZT on 14 June, in DR position latitude  $31^{\circ} 58' S$ , longitude  $48^{\circ} 42' W$ , you observe an amplitude of the Moon. The center of the Moon is on the visible horizon and bears  $118^{\circ}$  psc. The variation is  $10^{\circ} W$ . What is the deviation?

- a)  $2.5^{\circ} W$
- b)  $2.1^{\circ} W$  – correct**
- c)  $1.7^{\circ} W$
- d)  $1.7^{\circ} E$

### Amplitudes of Planets

AMP B18. At 2048 ZT on 13 October, you are in DR position latitude  $44^{\circ} 02.8' S$ , longitude  $146^{\circ} 58.3' E$  when you observe an amplitude of Venus. The planet is about one Sun's diameter above the visible horizon and bears  $222.2^{\circ}$  psc. The variation is  $15^{\circ} E$ . What is the deviation?

- a)  $0.0^{\circ}$
- b)  $1.1^{\circ} E$
- c)  **$1.0^{\circ} W$  – correct**
- d)  $1.5^{\circ} W$

AMP B19. At 2232 ZT on 14 July you are in DR position latitude  $33^{\circ} 52' S$ , longitude  $150^{\circ} 03' W$  when you observe an amplitude of Jupiter. The planet is about one Sun's diameter above the visible horizon and bears  $268.5^{\circ}$  pgc. The variation is  $15^{\circ} E$ . What is the gyro error?

- a)  **$1.0^{\circ} E$  - correct**
- b)  $0.5^{\circ} E$
- c)  $0.0^{\circ}$
- d)  $0.5^{\circ} W$

AMP B20. At 2234 ZT on 14 July you are in DR position latitude  $34^{\circ} 03' N$ , longitude  $150^{\circ} 16' W$ , when you observe an amplitude of Saturn. The planet is about one Sun's diameter above the visible horizon and bears  $272.1^{\circ}$  pgc. The variation is  $14^{\circ} E$ . What is the gyro error?

- a)  $0.5^{\circ} W$
- b)  $0.5^{\circ} E$
- c)  **$1.5^{\circ} W$  - correct**
- d)  $2.5^{\circ} E$

AMP B21. At 2237 ZT on 14 July, you are in DR position latitude  $33^{\circ} 57' N$ , longitude  $150^{\circ} 32' W$  when you observe an amplitude of Saturn. The planet is about one Sun's diameter above the visible horizon and bears  $258.6^{\circ}$  psc. The variation is  $14^{\circ} E$ . What is the deviation?

- a)  **$2.0^{\circ} W$  – correct**
- b)  $1.0^{\circ} W$
- c)  $0.0^{\circ}$
- d)  $1.0^{\circ} E$



## **Azimuth Problems**



## Azimuth Problems

- “Azimuth” is the horizontal direction of a celestial point from a terrestrial point, expressed as an angular distance from a reference direction (usually 0°N). Most commonly it is measured using an azimuth ring on a compass repeater when making an observation of a celestial body.
- Azimuth problems generally involve determining the tabulated or computed azimuth value and comparing it to a gyro compass or a steering compass to determine compass error.
- To reduce the size of the sight reduction tables, some azimuth values that are repeated are eliminated from the tables, requiring an azimuth adjustment based on the rules found at the top or bottom of the tables. However, the azimuth rules may modify this azimuth value to a final azimuth (Zn) using the rules  $360^\circ - Z$ ,  $180^\circ - Z$ , or  $180^\circ + Z$  in some cases.
- Azimuth values can be determined using tables or solved directly with the formula:

$$\circ \quad \tan Z = \left( \frac{\cos d \sin LHA}{(\cos L)(\sin d) - (\sin L)(\cos d)(\cos LHA)} \right), \text{ where:}$$

LHA is local hour angle  
L is latitude  
d is declination

## Azimuth Problems

### Azimuth of the Sun Problems

AZI D1. On 17 June, your 0815 zone time DR position is latitude  $25^{\circ} 27.0' N$ , longitude  $47^{\circ} 16.0' W$ . At that time, you observe the Sun bearing  $079.5^{\circ}$  per standard magnetic compass. The chronometer reads 11h 15m 03s, and the chronometer error is 01m 15s fast. The variation is  $3^{\circ}$  E. What is the deviation of the standard magnetic compass?

Answer:  $3.6^{\circ} W$

Step 1: Determine the correct chronometer time of the sight.

Chronometer: 11h 15m 03s

Chronometer error: 01m 15s fast

Correct chronometer time: 11h 15m 03s – 1m 15s = 11h 13m 48s

Step 2: Determine the GMT of the sight.

Ship time: 0815

Chronometer time: 11h 13m 48s

DR Longitude:  $47^{\circ} 16' W$  – corresponds to (+3 ZD)

GMT of sight: 11:13:48, 17 June

Step 3: Determine the declination of the Sun.

Declination (hours):  $N 23^{\circ} 23.1'$  (d number 0.1')

Declination (increment): 0

Declination (total):  $N 23^{\circ} 23.1'$

Step 4: Determine the GHA of the Sun.

GHA (hours):  $344^{\circ} 48.1'$

GHA (increment):  $3^{\circ} 27.0'$

GHA (total):  $348^{\circ} 15.1'$

Step 5: Determine the LHA of the Sun.

GHA (Sun):  $348^{\circ} 15.1'$

DR Longitude:  $47^{\circ} 16.0' W$  (subtract west, add east)

LHA (Sun):  $348^{\circ} 15.1' - 47^{\circ} 16.0' W = \underline{300^{\circ} 59.1'}$

| G.M.T. | SUN          |       |
|--------|--------------|-------|
|        | G.H.A.       | Dec.  |
| 17 00  | 179 49.6 N23 | 22.3  |
| 01     | 194 49.4     | 22.3  |
| 02     | 209 49.3     | 22.4  |
| 03     | 224 49.2     | 22.5  |
| 04     | 239 49.0     | 22.6  |
| 05     | 254 48.9     | 22.6  |
| 06     | 269 48.8 N23 | 22.7  |
| 07     | 284 48.6     | 22.8  |
| 08     | 299 48.5     | 22.9  |
| 09     | 314 48.4     | 22.9  |
| 10     | 329 48.2     | 23.0  |
| 11     | 344 48.1     | 23.1  |
| 12     | 359 48.0 N23 | 23.1  |
| 13     | 14 47.8      | 23.2  |
| 14     | 29 47.7      | 23.3  |
| 15     | 44 47.5      | 23.3  |
| 16     | 59 47.4      | 23.4  |
| 17     | 74 47.3      | 23.5  |
| 18     | 89 47.1 N23  | 23.5  |
| 19     | 104 47.0     | 23.6  |
| 20     | 119 46.9     | 23.7  |
| 21     | 134 46.7     | 23.7  |
| 22     | 149 46.6     | 23.8  |
| 23     | 164 46.5     | 23.8  |
|        | S.D. 15.8    | d 0.1 |

| m  | SUN     | ARIES  | MOON   | $\bar{v}$ or Corr <sup>n</sup> | $\bar{v}$ or Corr <sup>n</sup> | $\bar{v}$ or Corr <sup>n</sup> |
|----|---------|--------|--------|--------------------------------|--------------------------------|--------------------------------|
| 13 | PLANETS |        |        | d                              | d                              | d                              |
| s  | ° ' "   | ° ' "  | ° ' "  | ' "                            | ' "                            | ' "                            |
| 00 | 3 15.0  | 3 15.5 | 3 06.1 | 0.0 0.0                        | 6.0 1.4                        | 12.0 2.7                       |
| 01 | 3 15.3  | 3 15.8 | 3 06.4 | 0.1 0.0                        | 6.1 1.4                        | 12.1 2.7                       |
| 02 | 3 15.5  | 3 16.0 | 3 06.6 | 0.2 0.0                        | 6.2 1.4                        | 12.2 2.7                       |
| 03 | 3 15.8  | 3 16.3 | 3 06.8 | 0.3 0.1                        | 6.3 1.4                        | 12.3 2.8                       |
| 04 | 3 16.0  | 3 16.5 | 3 07.1 | 0.4 0.1                        | 6.4 1.4                        | 12.4 2.8                       |
| 45 | 3 26.3  | 3 26.8 | 3 16.9 | 4.5 1.0                        | 10.5 2.4                       | 16.5 3.7                       |
| 46 | 3 26.5  | 3 27.1 | 3 17.1 | 4.6 1.0                        | 10.6 2.4                       | 16.6 3.7                       |
| 47 | 3 26.8  | 3 27.3 | 3 17.3 | 4.7 1.1                        | 10.7 2.4                       | 16.7 3.8                       |
| 48 | 3 27.0  | 3 27.6 | 3 17.6 | 4.8 1.1                        | 10.8 2.4                       | 16.8 3.8                       |
| 49 | 3 27.3  | 3 27.8 | 3 17.8 | 4.9 1.1                        | 10.9 2.5                       | 16.9 3.8                       |



# Azimuth Problems

Step 6: Enter HO229 with whole values of latitude, declination (same in this case), and LHA. By increasing the value of each argument by 1 whole increment, triple interpolate for the exact values of each for the desired time/location.

|                 | Base Value | Base Z | Next incremental Z | Difference in Z | Increment | Correction<br>(Diff Z x Increment) / 60 |
|-----------------|------------|--------|--------------------|-----------------|-----------|-----------------------------------------|
| Latitude – N    | 25°        |        |                    |                 | 27.0'     |                                         |
| Declination - N | 23°        |        |                    |                 | 23.1'     |                                         |
| LHA             | 300°       |        |                    |                 | 59.1'     |                                         |

|             | Base Value | Base Z | Next incremental Z | Difference in Z | Increment | Correction<br>(Diff Z x Increment) / 60 |
|-------------|------------|--------|--------------------|-----------------|-----------|-----------------------------------------|
| Latitude    | 25°        | 78.7°  |                    |                 | 27.0'     |                                         |
| Declination | 23°        | 78.7°  |                    |                 | 23.1'     |                                         |
| LHA         | 300°       | 78.7°  |                    |                 | 59.1'     |                                         |

| 60°, 300° L.H.A. |                     |                     |                     | LATITUDE SAME NA    |      |                     |                     |
|------------------|---------------------|---------------------|---------------------|---------------------|------|---------------------|---------------------|
| Dec.             | 23°                 | 24°                 | 25°                 | 26°                 | Dec. | 23°                 | 24°                 |
| 0                | 27 24.2 +26.2 102.7 | 27 10.7 +27.3 103.2 | 26 56.8 +28.2 103.7 | 26 42.3 +29.2 104.2 | 0    | 28 18.0 +26.4 103.2 | 28 04.0 +27.5 103.7 |
| 1                | 27 50.4 +25.7 101.7 | 27 38.0 +26.7 102.2 | 27 25.0 +27.8 102.7 | 27 11.5 +28.9 103.2 | 1    | 28 44.4 +26.0 102.2 | 28 31.5 +27.0 102.7 |
| 2                | 28 16.1 +25.3 100.7 | 28 04.7 +26.4 101.2 | 27 52.8 +27.4 101.7 | 27 40.4 +28.4 102.2 | 2    | 29 10.4 +25.4 101.2 | 28 58.5 +26.5 101.7 |
| 3                | 28 41.4 +24.8 99.6  | 28 31.1 +25.8 100.2 | 28 20.2 +26.9 100.7 | 28 08.8 +27.9 101.2 | 3    | 29 35.8 +25.0 100.1 | 29 25.0 +26.0 100.7 |
| 4                | 29 06.2 +24.3 98.6  | 28 56.9 +25.4 99.1  | 28 47.1 +26.5 99.7  | 28 36.7 +27.8 100.2 | 4    | 30 00.8 +24.4 99.1  | 29 51.0 +25.6 99.6  |
| 5                | 29 30.5 +23.8 97.6  | 29 22.3 +25.0 98.1  | 29 13.6 +26.0 98.7  | 29 04.3 +27.0 99.2  | 5    | 30 25.2 +24.0 98.0  | 30 16.6 +25.0 98.6  |
| 6                | 29 54.3 +23.4 96.5  | 29 47.3 +24.4 97.1  | 29 39.6 +25.5 97.6  | 29 31.3 +26.6 98.2  | 6    | 30 49.2 +23.4 97.0  | 30 41.6 +24.6 97.5  |
| 7                | 30 17.7 +22.7 95.4  | 30 11.7 +23.9 96.0  | 30 05.1 +25.0 96.6  | 29 57.9 +26.1 97.2  | 7    | 31 12.6 +22.9 95.9  | 31 06.2 +24.0 96.5  |
| 8                | 30 40.4 +22.3 94.4  | 30 35.6 +23.4 94.9  | 30 30.1 +24.5 95.5  | 30 24.0 +25.6 96.1  | 8    | 31 35.5 +22.3 94.8  | 31 30.2 +23.4 95.4  |
| 9                | 31 02.7 +21.7 93.3  | 30 59.0 +22.8 93.9  | 30 54.6 +24.0 94.5  | 30 49.6 +25.1 95.1  | 9    | 31 57.8 +21.8 93.7  | 31 53.6 +22.9 94.3  |
| 10               | 31 24.4 +21.2 92.2  | 31 21.8 +22.3 92.8  | 31 18.6 +23.4 93.4  | 31 14.7 +24.5 94.0  | 10   | 32 19.6 +21.2 92.6  | 32 16.5 +22.4 93.2  |
| 11               | 31 45.6 +20.5 91.1  | 31 44.1 +21.7 91.7  | 31 42.0 +22.9 92.3  | 31 39.2 +24.0 92.9  | 11   | 32 40.8 +20.6 91.5  | 32 38.9 +21.7 92.1  |
| 12               | 32 06.1 +20.0 90.0  | 32 05.8 +21.2 90.6  | 32 04.9 +22.3 91.2  | 32 03.2 +23.5 91.9  | 12   | 33 01.4 +20.0 90.4  | 33 00.6 +21.2 91.0  |
| 13               | 32 26.1 +19.4 88.9  | 32 27.0 +20.6 89.5  | 32 27.2 +21.7 90.1  | 32 26.7 +22.9 90.8  | 13   | 33 21.4 +19.3 89.2  | 33 21.8 +20.6 89.9  |
| 14               | 32 45.5 +18.8 87.7  | 32 47.6 +20.0 88.4  | 32 48.9 +21.2 89.0  | 32 49.6 +22.3 89.7  | 14   | 33 40.7 +18.8 88.1  | 33 42.4 +19.9 88.8  |
| 15               | 33 04.3 +18.2 86.6  | 33 07.6 +19.3 87.3  | 33 10.1 +20.5 87.9  | 33 11.9 +21.7 88.6  | 15   | 33 59.5 +18.1 87.0  | 34 02.3 +19.3 87.6  |
| 16               | 33 22.5 +17.6 85.5  | 33 26.9 +18.8 86.1  | 33 30.6 +20.0 86.8  | 33 33.6 +21.2 87.5  | 16   | 34 17.6 +17.5 85.8  | 34 21.6 +18.7 86.5  |
| 17               | 33 40.1 +16.9 84.3  | 33 45.7 +18.1 85.0  | 33 50.6 +19.3 85.7  | 33 54.8 +20.5 86.3  | 17   | 34 35.1 +16.8 84.7  | 34 40.3 +18.0 85.3  |
| 18               | 33 57.0 +16.3 83.2  | 34 03.8 +17.5 83.8  | 34 09.9 +18.6 84.5  | 34 15.3 +19.8 85.2  | 18   | 34 51.9 +16.1 83.5  | 34 58.3 +17.3 84.2  |
| 19               | 34 13.3 +15.6 82.0  | 34 21.3 +16.8 82.7  | 34 28.5 +18.1 83.4  | 34 35.1 +19.2 84.0  | 19   | 35 08.0 +15.4 82.3  | 35 15.6 +16.7 83.0  |
| 20               | 34 28.9 +14.9 80.8  | 34 38.1 +16.1 81.5  | 34 46.6 +17.3 82.2  | 34 54.3 +18.6 82.9  | 20   | 35 23.4 +14.7 81.1  | 35 32.3 +16.0 81.8  |
| 21               | 34 43.8 +14.2 79.7  | 34 54.2 +15.5 80.3  | 35 03.9 +16.7 81.0  | 35 12.9 +17.9 81.7  | 21   | 35 38.1 +14.1 79.9  | 35 48.3 +15.2 80.6  |
| 22               | 34 58.0 +13.6 78.5  | 35 09.7 +14.7 79.2  | 35 20.8 +16.0 79.9  | 35 30.8 +17.2 80.6  | 22   | 35 52.2 +13.3 78.7  | 36 03.5 +14.6 79.5  |
| 23               | 35 11.6 +12.8 77.3  | 35 24.4 +14.1 78.0  | 35 36.6 +15.3 78.7  | 35 48.0 +16.5 79.4  | 23   | 36 05.5 +12.6 77.5  | 36 18.1 +13.8 78.2  |
| 24               | 35 24.4 +12.2 76.1  | 35 38.5 +13.4 76.8  | 35 51.9 +14.6 77.5  | 36 04.5 +15.8 78.2  | 24   | 36 18.1 +11.8 76.3  | 36 31.9 +13.1 77.0  |

| 59°, 301° L.H.A. |                     |                     |                     | LATITUDE SAME NA    |      |                     |                     |
|------------------|---------------------|---------------------|---------------------|---------------------|------|---------------------|---------------------|
| Dec.             | 23°                 | 24°                 | 25°                 | 26°                 | Dec. | 23°                 | 24°                 |
| 0                | 28 18.0 +26.4 103.2 | 28 04.0 +27.5 103.7 | 27 49.5 +28.5 104.2 | 27 34.5 +29.5 104.8 | 0    | 28 18.0 +26.4 103.2 | 28 04.0 +27.5 103.7 |
| 1                | 28 44.4 +26.0 102.2 | 28 31.5 +27.0 102.7 | 28 18.0 +28.0 103.3 | 28 04.0 +29.0 103.8 | 1    | 28 44.4 +26.0 102.2 | 28 31.5 +27.0 102.7 |
| 2                | 29 10.4 +25.4 101.2 | 28 58.5 +26.5 101.7 | 28 46.0 +27.6 102.2 | 28 33.0 +28.6 102.8 | 2    | 29 10.4 +25.4 101.2 | 28 58.5 +26.5 101.7 |
| 3                | 29 35.8 +25.0 100.1 | 29 25.0 +26.0 100.7 | 29 13.6 +27.1 101.2 | 29 01.6 +28.2 101.8 | 3    | 29 35.8 +25.0 100.1 | 29 25.0 +26.0 100.7 |
| 4                | 30 00.8 +24.4 99.1  | 29 51.0 +25.6 99.6  | 29 40.7 +26.6 100.2 | 29 29.8 +27.7 100.8 | 4    | 30 00.8 +24.4 99.1  | 29 51.0 +25.6 99.6  |
| 5                | 30 25.2 +24.0 98.0  | 30 16.6 +25.0 98.6  | 30 07.3 +26.1 99.2  | 29 57.5 +27.2 99.7  | 5    | 30 25.2 +24.0 98.0  | 30 16.6 +25.0 98.6  |
| 6                | 30 49.2 +23.4 97.0  | 30 41.6 +24.6 97.5  | 30 33.4 +25.7 98.1  | 30 24.7 +26.7 98.7  | 6    | 30 49.2 +23.4 97.0  | 30 41.6 +24.6 97.5  |
| 7                | 31 12.6 +22.9 95.9  | 31 06.2 +24.0 96.5  | 30 59.1 +25.1 97.1  | 30 51.4 +26.2 97.7  | 7    | 31 12.6 +22.9 95.9  | 31 06.2 +24.0 96.5  |
| 8                | 31 35.5 +22.3 94.8  | 31 30.2 +23.4 95.4  | 31 24.2 +24.6 96.0  | 31 17.6 +25.7 96.6  | 8    | 31 35.5 +22.3 94.8  | 31 30.2 +23.4 95.4  |
| 9                | 31 57.8 +21.8 93.7  | 31 53.6 +22.9 94.3  | 31 48.8 +24.0 94.9  | 31 43.3 +25.2 95.6  | 9    | 31 57.8 +21.8 93.7  | 31 53.6 +22.9 94.3  |
| 10               | 32 19.6 +21.2 92.6  | 32 16.5 +22.4 93.2  | 32 12.8 +23.5 93.9  | 32 08.5 +24.6 94.5  | 10   | 32 19.6 +21.2 92.6  | 32 16.5 +22.4 93.2  |
| 11               | 32 40.8 +20.6 91.5  | 32 38.9 +21.7 92.1  | 32 36.3 +22.9 92.8  | 32 33.1 +24.0 93.4  | 11   | 32 40.8 +20.6 91.5  | 32 38.9 +21.7 92.1  |
| 12               | 33 01.4 +20.0 90.4  | 33 00.6 +21.2 91.0  | 32 59.2 +22.4 91.7  | 32 57.1 +23.5 92.3  | 12   | 33 01.4 +20.0 90.4  | 33 00.6 +21.2 91.0  |
| 13               | 33 21.4 +19.3 89.2  | 33 21.8 +20.6 89.9  | 33 21.6 +21.7 90.6  | 33 20.6 +22.9 91.2  | 13   | 33 21.4 +19.3 89.2  | 33 21.8 +20.6 89.9  |
| 14               | 33 40.7 +18.8 88.1  | 33 42.4 +19.9 88.8  | 33 43.3 +21.1 89.4  | 33 43.5 +22.3 90.1  | 14   | 33 40.7 +18.8 88.1  | 33 42.4 +19.9 88.8  |
| 15               | 33 59.5 +18.1 87.0  | 34 02.3 +19.3 87.6  | 34 04.4 +20.5 88.3  | 34 05.8 +21.7 89.0  | 15   | 33 59.5 +18.1 87.0  | 34 02.3 +19.3 87.6  |
| 16               | 34 17.6 +17.5 85.8  | 34 21.6 +18.7 86.5  | 34 24.9 +19.9 87.2  | 34 27.5 +21.1 87.9  | 16   | 34 17.6 +17.5 85.8  | 34 21.6 +18.7 86.5  |
| 17               | 34 35.1 +16.8 84.7  | 34 40.3 +18.0 85.3  | 34 44.8 +19.2 86.0  | 34 48.6 +20.4 86.7  | 17   | 34 35.1 +16.8 84.7  | 34 40.3 +18.0 85.3  |
| 18               | 34 51.9 +16.1 83.5  | 34 58.3 +17.3 84.2  | 35 04.0 +18.6 84.9  | 35 09.0 +19.8 85.6  | 18   | 34 51.9 +16.1 83.5  | 34 58.3 +17.3 84.2  |
| 19               | 35 08.0 +15.4 82.3  | 35 15.6 +16.7 83.0  | 35 22.6 +17.9 83.7  | 35 28.8 +19.1 84.4  | 19   | 35 08.0 +15.4 82.3  | 35 15.6 +16.7 83.0  |
| 20               | 35 23.4 +14.7 81.1  | 35 32.3 +16.0 81.8  | 35 40.5 +17.2 82.5  | 35 47.9 +18.4 83.3  | 20   | 35 23.4 +14.7 81.1  | 35 32.3 +16.0 81.8  |
| 21               | 35 38.1 +14.1 79.9  | 35 48.3 +15.2 80.6  | 35 57.7 +16.4 81.4  | 36 06.3 +17.7 82.1  | 21   | 35 38.1 +14.1 79.9  | 35 48.3 +15.2 80.6  |
| 22               | 35 52.2 +13.3 78.7  | 36 03.5 +14.6 79.5  | 36 14.1 +15.8 80.2  | 36 24.0 +17.0 80.9  | 22   | 35 52.2 +13.3 78.7  | 36 03.5 +14.6 79.5  |
| 23               | 36 05.5 +12.6 77.5  | 36 18.1 +13.8 78.2  | 36 29.9 +15.1 79.0  | 36 41.0 +16.3 79.7  | 23   | 36 05.5 +12.6 77.5  | 36 18.1 +13.8 78.2  |
| 24               | 36 18.1 +11.8 76.3  | 36 31.9 +13.1 77.0  | 36 45.0 +14.3 77.8  | 36 57.3 +15.6 78.5  | 24   | 36 18.1 +11.8 76.3  | 36 31.9 +13.1 77.0  |

|             | Base Value | Base Z | Next incremental Z | Difference in Z | Increment | Correction<br>(Diff Z x Increment) / 60 |
|-------------|------------|--------|--------------------|-----------------|-----------|-----------------------------------------|
| Latitude    | 25°        | 78.7°  | 79.4°              | 0.7°            | 27.0'     |                                         |
| Declination | 23°        | 78.7°  | 77.5°              | -1.2°           | 23.1'     |                                         |
| LHA         | 300°       | 78.7°  | 79.0°              | 0.3°            | 59.1'     |                                         |

|             | Base Value | Base Z | Next incremental Z | Difference in Z | Increment | Correction<br>(Diff Z x Increment) / 60 |
|-------------|------------|--------|--------------------|-----------------|-----------|-----------------------------------------|
| Latitude    | 25°        | 78.7°  | 79.4°              | 0.7°            | 27.0'     | +0.32°                                  |
| Declination | 23°        | 78.7°  | 77.5°              | -1.2°           | 23.1'     | -0.46°                                  |
| LHA         | 300°       | 78.7°  | 79.0°              | 0.3°            | 59.1'     | +0.30°                                  |

Total correction = 0.32° - 0.46° + 0.30° = +0.2°

## Azimuth Problems

Step 7: Apply the correction to the base values to determine true azimuth.

Base azimuth:  $078.7^\circ$

Correction:  $+0.2^\circ$

Corrected azimuth:  $078.7^\circ + 0.2^\circ = \underline{078.9^\circ}$

*Note - Check azimuth rules: if LHA greater than  $180^\circ$ , then  $zn = z$ .*

Step 8: Answer the required questions.

T:  $078.9^\circ$  (Determine in Step 7)

V:  $3.0^\circ$  E (Given)

M:  $075.9^\circ$  (Calculated)

**D:  $3.6^\circ$  W**

C:  $079.5^\circ$  (Given)

Note this problem can be solved without the triple interpolation using the formula:

$$\tan Z = \left( \frac{\cos d \sin LHA}{(\cos L)(\sin d) - (\sin L)(\cos d)(\cos LHA)} \right), \text{ where:}$$

LHA is local hour angle  
L is latitude  
d is declination

## Azimuth Problems

AZI D2. On 12 September, your 0736 zone time DR position is latitude  $28^{\circ} 34' S$ , longitude  $174^{\circ} 49' E$ . At that time you observe the Sun bearing  $084^{\circ}$  per standard magnetic compass (psc). The chronometer reads 07h 38m 11s, and the chronometer error is 01m 46s fast. The variation is  $11^{\circ} W$ . What is the deviation of the standard magnetic compass?

Answer:  $3.4^{\circ} E$

Step 1: Determine the correct chronometer time of the sight.

Chronometer: 07h 38m 11s

Chronometer error: 01m 46s fast

Correct chronometer time: 07h 38m 11s – 1m 46s = 07h 36m 25s

Step 2: Determine the GMT of the sight.

Ship time: 0736

Chronometer time: 07h 36m 25s

DR Longitude:  $174^{\circ} 49' E$  – corresponds to (-12 ZD)

GMT of sight: 19:36:25, 11 September

Step 3: Determine the declination of the Sun.

Declination (hours):  $N 4^{\circ} 22.6'$

d number: -1.0'

Declination (increment): -0.6'

Declination (total):  $N 4^{\circ} 22.0'$

Step 4: Determine the GHA of the Sun.

GHA (hours):  $105^{\circ} 52.6'$

GHA (increment):  $9^{\circ} 06.3'$

GHA (total):  $114^{\circ} 58.9'$

Step 5: Determine the LHA of the Sun.

GHA (Sun):  $114^{\circ} 58.9'$

DR Longitude:  $174^{\circ} 49.0' E$  (subtract west, add east)

LHA (Sun):  $114^{\circ} 58.9' + 174^{\circ} 49.0' E = \underline{289^{\circ} 47.9'}$

|    |    |      |      |    |     |      |
|----|----|------|------|----|-----|------|
| 11 | 00 | 180  | 48.4 | N  | 4   | 40.7 |
| 01 |    | 195  | 48.6 |    |     | 39.8 |
| 02 |    | 210  | 48.8 |    |     | 38.8 |
| 03 |    | 225  | 49.0 | .. |     | 37.9 |
| 04 |    | 240  | 49.3 |    |     | 36.9 |
| 05 |    | 255  | 49.5 |    |     | 36.0 |
| 06 |    | 270  | 49.7 | N  | 4   | 35.0 |
| 07 |    | 285  | 49.9 |    |     | 34.1 |
| 08 |    | 300  | 50.1 |    |     | 33.1 |
| F  | 09 | 315  | 50.4 | .. |     | 32.2 |
| R  | 10 | 330  | 50.6 |    |     | 31.2 |
| I  | 11 | 345  | 50.8 |    |     | 30.3 |
| D  | 12 | 0    | 51.0 | N  | 4   | 29.3 |
| A  | 13 | 15   | 51.2 |    |     | 28.3 |
| Y  | 14 | 30   | 51.5 |    |     | 27.4 |
|    | 15 | 45   | 51.7 | .. |     | 26.4 |
|    | 16 | 60   | 51.9 |    |     | 25.5 |
|    | 17 | 75   | 52.1 |    |     | 24.5 |
|    | 18 | 90   | 52.3 | N  | 4   | 23.6 |
|    | 19 | 105  | 52.6 |    |     | 22.6 |
|    | 20 | 120  | 52.8 |    |     | 21.7 |
|    | 21 | 135  | 53.0 | .. |     | 20.7 |
|    | 22 | 150  | 53.2 |    |     | 19.8 |
|    | 23 | 165  | 53.4 |    |     | 18.8 |
|    |    | S.D. | 15.9 | d  | 1.0 |      |

| 36 | SUN    | PLANETS | ARIES  | MOON | or Corr |
|----|--------|---------|--------|------|---------|
| 00 | 9 00.0 | 9 01.5  | 8 35.4 | 6.0  | 0.0     |
| 01 | 9 00.3 | 9 01.7  | 8 35.6 | 0.1  | 0.1     |
| 02 | 9 00.5 | 9 02.0  | 8 35.9 | 0.2  | 0.1     |
| 03 | 9 00.8 | 9 02.2  | 8 36.1 | 0.3  | 0.2     |
| 04 | 9 01.0 | 9 02.5  | 8 36.4 | 0.4  | 0.2     |
| 05 | 9 01.3 | 9 02.7  | 8 36.6 | 0.5  | 0.3     |
| 06 | 9 01.5 | 9 03.0  | 8 36.8 | 0.6  | 0.4     |
| 07 | 9 01.8 | 9 03.2  | 8 37.1 | 0.7  | 0.4     |
| 08 | 9 02.0 | 9 03.5  | 8 37.3 | 0.8  | 0.5     |
| 09 | 9 02.3 | 9 03.7  | 8 37.5 | 0.9  | 0.5     |
| 10 | 9 02.5 | 9 04.0  | 8 37.8 | 1.0  | 0.6     |
| 11 | 9 02.8 | 9 04.2  | 8 38.0 | 1.1  | 0.7     |
| 12 | 9 03.0 | 9 04.5  | 8 38.3 | 1.2  | 0.7     |
| 13 | 9 03.3 | 9 04.7  | 8 38.5 | 1.3  | 0.8     |
| 14 | 9 03.5 | 9 05.0  | 8 38.7 | 1.4  | 0.9     |
| 15 | 9 03.8 | 9 05.2  | 8 39.0 | 1.5  | 0.9     |
| 16 | 9 04.0 | 9 05.5  | 8 39.2 | 1.6  | 1.0     |
| 17 | 9 04.3 | 9 05.7  | 8 39.5 | 1.7  | 1.0     |
| 18 | 9 04.5 | 9 06.0  | 8 39.7 | 1.8  | 1.1     |
| 19 | 9 04.8 | 9 06.2  | 8 39.9 | 1.9  | 1.2     |
| 20 | 9 05.0 | 9 06.5  | 8 40.2 | 2.0  | 1.2     |
| 21 | 9 05.3 | 9 06.7  | 8 40.4 | 2.1  | 1.3     |
| 22 | 9 05.5 | 9 07.0  | 8 40.6 | 2.2  | 1.3     |
| 23 | 9 05.8 | 9 07.2  | 8 40.9 | 2.3  | 1.4     |
| 24 | 9 06.0 | 9 07.5  | 8 41.1 | 2.4  | 1.5     |
| 25 | 9 06.3 | 9 07.7  | 8 41.4 | 2.5  | 1.5     |
| 26 | 9 06.5 | 9 08.0  | 8 41.6 | 2.6  | 1.6     |
| 27 | 9 06.8 | 9 08.2  | 8 41.8 | 2.7  | 1.6     |
| 28 | 9 07.0 | 9 08.5  | 8 42.1 | 2.8  | 1.7     |
| 29 | 9 07.3 | 9 08.7  | 8 42.3 | 2.9  | 1.8     |

# Azimuth Problems

Step 6: Enter HO229 with whole values of latitude, declination (contrary in this case), and LHA. By increasing the value of each argument by 1 whole increment, triple interpolate for the exact values of each for the desired time/location.

|                 | Base Value | Base Z | Next incremental Z | Difference in Z | Increment | Correction<br>(Diff Z x Increment) / 60 |
|-----------------|------------|--------|--------------------|-----------------|-----------|-----------------------------------------|
| Latitude – S    | 28°        |        |                    |                 | 34.0'     |                                         |
| Declination - N | 4°         |        |                    |                 | 22.0'     |                                         |
| LHA             | 289°       |        |                    |                 | 47.9'     |                                         |

|             | Base Value | Base Z | Next incremental Z | Difference in Z | Increment | Correction<br>(Diff Z x Increment) / 60 |
|-------------|------------|--------|--------------------|-----------------|-----------|-----------------------------------------|
| Latitude    | 28°        | 102.8° |                    |                 | 34.0'     |                                         |
| Declination | 4°         | 102.8° |                    |                 | 22.0'     |                                         |
| LHA         | 289°       | 102.8° |                    |                 | 47.9'     |                                         |

| TITUDE CONTRARY NAME TO DECLINATION L.H.A. 71°, 289° |       |       |         |       |       |         |       |       |         |       |       |
|------------------------------------------------------|-------|-------|---------|-------|-------|---------|-------|-------|---------|-------|-------|
| 25°                                                  |       |       | 26°     |       |       | 27°     |       |       | 28°     |       |       |
| Hc                                                   | d     | Z     | Hc      | d     | Z     | Hc      | d     | Z     | Hc      | d     | Z     |
| 17 09.7                                              | -26.7 | 98.3  | 17 00.9 | -27.6 | 98.6  | 16 51.8 | -28.6 | 98.9  | 16 42.4 | -29.6 | 99.2  |
| 16 43.0                                              | -26.9 | 99.2  | 16 33.3 | -27.9 | 99.5  | 16 23.2 | -28.8 | 99.8  | 16 12.8 | -29.7 | 100.1 |
| 16 16.1                                              | -27.2 | 100.1 | 16 05.4 | -28.1 | 100.4 | 15 54.4 | -29.1 | 100.7 | 15 43.1 | -30.0 | 101.0 |
| 15 48.9                                              | -27.4 | 101.1 | 15 37.3 | -28.4 | 101.4 | 15 25.3 | -29.3 | 101.6 | 15 13.1 | -30.2 | 101.9 |
| 15 21.5                                              | -27.6 | 102.0 | 15 08.9 | -28.5 | 102.3 | 14 56.0 | -29.4 | 102.5 | 14 42.9 | -30.4 | 102.8 |
| 14 53.9                                              | -27.8 | 102.9 | 14 40.4 | -28.8 | 103.2 | 14 26.6 | -29.7 | 103.4 | 14 12.5 | -30.6 | 103.7 |
| 14 26.1                                              | -28.1 | 103.8 | 14 11.6 | -29.0 | 104.1 | 13 56.9 | -29.9 | 104.3 | 13 41.9 | -30.8 | 104.6 |
| 13 58.0                                              | -28.2 | 104.7 | 13 42.6 | -29.2 | 105.0 | 13 27.0 | -30.1 | 105.2 | 13 11.1 | -30.9 | 105.4 |
| 13 29.8                                              | -28.5 | 105.7 | 13 13.4 | -29.3 | 105.9 | 12 56.9 | -30.2 | 106.1 | 12 40.2 | -31.2 | 106.3 |
| 13 01.3                                              | -28.6 | 106.6 | 12 44.1 | -29.5 | 106.8 | 12 26.7 | -30.5 | 107.0 | 12 09.0 | -31.3 | 107.2 |
|                                                      |       |       |         |       |       |         |       |       | 11 51.2 | -32.2 | 107.4 |

| TITUDE CONTRARY NAME TO DECLINATION L.H.A. 70°, 290° |       |       |         |       |       |         |       |       |         |       |       |
|------------------------------------------------------|-------|-------|---------|-------|-------|---------|-------|-------|---------|-------|-------|
| 25°                                                  |       |       | 26°     |       |       | 27°     |       |       | 28°     |       |       |
| Hc                                                   | d     | Z     | Hc      | d     | Z     | Hc      | d     | Z     | Hc      | d     | Z     |
| 18 03.5                                              | -26.8 | 98.7  | 17 54.2 | -27.8 | 99.1  | 17 44.6 | -28.8 | 99.4  | 17 34.6 | -29.7 | 99.7  |
| 17 36.7                                              | -27.1 | 99.7  | 17 26.4 | -28.0 | 100.0 | 17 15.8 | -28.9 | 100.3 | 17 04.9 | -29.9 | 100.6 |
| 17 09.6                                              | -27.3 | 100.6 | 16 58.4 | -28.3 | 100.9 | 16 46.9 | -29.3 | 101.2 | 16 35.0 | -30.1 | 101.5 |
| 16 42.3                                              | -27.6 | 101.6 | 16 30.1 | -28.5 | 101.8 | 16 17.6 | -29.4 | 102.1 | 16 04.9 | -30.4 | 102.4 |
| 16 14.7                                              | -27.8 | 102.5 | 16 01.6 | -28.8 | 102.8 | 15 48.2 | -29.7 | 103.0 | 15 34.5 | -30.6 | 103.3 |
| 15 46.9                                              | -28.1 | 103.4 | 15 32.8 | -29.0 | 103.7 | 15 18.5 | -29.9 | 103.9 | 15 03.9 | -30.8 | 104.2 |
| 15 18.8                                              | -28.3 | 104.3 | 15 03.8 | -29.1 | 104.6 | 14 48.6 | -30.1 | 104.8 | 14 33.1 | -31.0 | 105.1 |
| 14 50.5                                              | -28.4 | 105.2 | 14 34.7 | -29.4 | 105.5 | 14 18.5 | -30.3 | 105.7 | 14 02.1 | -31.2 | 106.0 |
| 14 22.1                                              | -28.7 | 106.1 | 14 05.3 | -29.6 | 106.4 | 13 48.2 | -30.5 | 106.6 | 13 30.9 | -31.3 | 106.9 |
| 13 53.4                                              | -28.9 | 107.0 | 13 35.7 | -29.8 | 107.3 | 13 17.7 | -30.7 | 107.5 | 12 59.6 | -31.6 | 107.7 |

|             | Base Value | Base Z | Next incremental Z | Difference in Z | Increment | Correction<br>(Diff Z x Increment) / 60 |
|-------------|------------|--------|--------------------|-----------------|-----------|-----------------------------------------|
| Latitude    | 28°        | 102.8° | 103.0°             | 0.2°            | 34.0'     |                                         |
| Declination | 4°         | 102.8° | 103.7°             | 0.9°            | 22.0'     |                                         |
| LHA         | 289°       | 102.8° | 103.3°             | 0.5°            | 47.9'     |                                         |

|             | Base Value | Base Z | Next incremental Z | Difference in Z | Increment | Correction<br>(Diff Z x Increment) / 60 |
|-------------|------------|--------|--------------------|-----------------|-----------|-----------------------------------------|
| Latitude    | 28°        | 102.8° | 103.0°             | 0.2°            | 34.0'     | +0.11°                                  |
| Declination | 4°         | 102.8° | 103.7°             | 0.9°            | 22.0'     | +0.33°                                  |
| LHA         | 289°       | 102.8° | 103.3°             | 0.5°            | 47.9'     | +0.40°                                  |

$$\text{Total correction} = 0.11^\circ + 0.33^\circ + 0.40^\circ = +0.8^\circ$$

Step 7: Apply the correction to the base values to determine true azimuth.

## Azimuth Problems

Base azimuth:  $102.8^\circ$

Correction:  $+0.8^\circ$

Corrected azimuth:  $102.8^\circ + 0.8^\circ = 103.6^\circ$

Azimuth rules correction:  $180^\circ - 103.6^\circ = \underline{76.4^\circ}$

*Note - Check azimuth rules: if LHA greater than  $180^\circ$ , then  $zn = 180^\circ - z$ .*

Step 8: Answer the required questions.

T:  $076.4^\circ$  (Determine in Step 7)

V:  $11.0^\circ$  W (Given)

M:  $087.4^\circ$  (Calculated)

**D:  $3.4^\circ$  E**

C:  $084.0^\circ$  (Given)

Note this problem can be solved without the triple interpolation using the formula:

$$\tan Z = \left( \frac{\cos d \sin LHA}{((\cos L)(\sin d) - (\sin L)(\cos d)(\cos LHA))} \right), \text{ where:}$$

LHA is local hour angle  
L is latitude  
d is declination

## Azimuth Problems

### Azimuth of Stars/Planets Problems

AZI D3. At 2326 ZT on 22 June your vessel's position is latitude  $28^{\circ} 30' N$ , longitude  $150^{\circ} 04' W$ . An azimuth of the planet Jupiter is observed, and the standard compass bearing is  $250.4^{\circ}$ . The chronometer reads 09h 24m 36s and is 01m 12s slow. The variation of this area is  $13.5^{\circ} E$ . What is the deviation of the standard compass?

Answer:  $2.3^{\circ} E$

Step 1: Determine the correct chronometer time of the sight.

Chronometer: 09h 24m 36s

Chronometer error: 01m 12s slow

Correct chronometer time: 09h 24m 36s + 1m 12s = 09h 25m 48s

Step 2: Determine the GMT of the sight.

Ship time: 2326

Chronometer time: 09h 25m 48s

DR Longitude:  $150^{\circ} 04' W$  – corresponds to (+10 ZD)

GMT of sight: 09:25:48, 23 June

Step 3: Determine the declination of Jupiter.

Declination (hours):  $N 0^{\circ} 37.7'$  (d number 0.1')

Declination (increment): 0

Declination (total):  $N 0^{\circ} 37.7'$

Step 4: Determine the GHA of Jupiter.

GHA (hours):  $224^{\circ} 33.4'$

GHA (increment):  $6^{\circ} 27.0'$  (v number 2.3)

GHA (v correction):  $+1.0'$

GHA (total):  $231^{\circ} 01.4'$

Step 5: Determine the LHA of Jupiter.

GHA (Jupiter):  $231^{\circ} 01.4'$

DR Longitude:  $150^{\circ} 04' W$  (subtract west, add east)

LHA (Jupiter):  $231^{\circ} 01.4' - 150^{\circ} 04.0' W = \underline{80^{\circ} 57.4'}$

| G.M.T.                          | ARIES    |                     | VENUS -3.3        |                   | MARS +1.7         |        | JUPITER -1.6 |  |
|---------------------------------|----------|---------------------|-------------------|-------------------|-------------------|--------|--------------|--|
|                                 | G.H.A.   | G.H.A.              | Dec.              | G.H.A.            | Dec.              | G.H.A. | Dec.         |  |
| T<br>U<br>E<br>S<br>D<br>A<br>Y | 23 00    | 271 04.4            | 157 25.8 N23 04.4 | 200 00.3 N22 30.5 | 89 12.7 N 0 38.4  |        |              |  |
|                                 | 01       | 286 06.9            | 172 25.0 03.9     | 215 00.9 30.8     | 104 15.0 38.4     |        |              |  |
|                                 | 02       | 301 09.4            | 187 24.2 03.5     | 230 01.5 31.0     | 119 17.3 38.3     |        |              |  |
|                                 | 03       | 316 11.8            | 202 23.3 03.1     | 245 02.1 31.3     | 134 19.6 38.2     |        |              |  |
|                                 | 04       | 331 14.3            | 217 22.5 02.6     | 260 02.6 31.5     | 149 21.9 38.1     |        |              |  |
|                                 | 05       | 346 16.7            | 232 21.7 02.2     | 275 03.2 31.8     | 164 24.2 38.0     |        |              |  |
|                                 | 06       | 1 19.2              | 247 20.9 N23 01.8 | 290 03.8 N22 32.0 | 179 26.5 N 0 37.9 |        |              |  |
|                                 | 07       | 16 21.7             | 262 20.1 01.3     | 305 04.4 32.3     | 194 28.8 37.9     |        |              |  |
|                                 | 08       | 31 24.1             | 277 19.3 00.9     | 320 05.0 32.5     | 209 31.1 37.8     |        |              |  |
|                                 | 09       | 46 26.6             | 292 18.5 00.4     | 335 05.6 32.8     | 224 33.4 37.7     |        |              |  |
|                                 | 10       | 61 29.1             | 307 17.7 23 00.0  | 350 06.2 33.0     | 239 35.7 37.6     |        |              |  |
|                                 | 11       | 76 31.5             | 322 16.8 22 59.6  | 5 06.8 33.3       | 254 37.9 37.5     |        |              |  |
|                                 | 12       | 91 34.0             | 337 16.0 N22 59.1 | 20 07.4 N22 33.5  | 269 40.2 N 0 37.4 |        |              |  |
|                                 | 13       | 106 36.5            | 352 15.2 58.7     | 35 08.0 33.8      | 284 42.5 37.4     |        |              |  |
|                                 | 14       | 121 38.9            | 7 14.4 58.2       | 50 08.6 34.0      | 299 44.8 37.3     |        |              |  |
|                                 | 15       | 136 41.4            | 22 13.6 57.8      | 65 09.2 34.3      | 314 47.1 37.2     |        |              |  |
|                                 | 16       | 151 43.9            | 37 12.8 57.3      | 80 09.8 34.5      | 329 49.4 37.1     |        |              |  |
|                                 | 17       | 166 46.3            | 52 12.0 56.9      | 95 10.3 34.8      | 344 51.7 37.0     |        |              |  |
|                                 | 18       | 181 48.8            | 67 11.2 N22 56.4  | 110 10.9 N22 35.0 | 359 54.0 N 0 36.9 |        |              |  |
|                                 | 19       | 196 51.2            | 82 10.4 56.0      | 125 11.5 35.3     | 14 56.3 36.8      |        |              |  |
|                                 | 20       | 211 53.7            | 97 09.6 55.5      | 140 12.1 35.5     | 29 58.6 36.8      |        |              |  |
|                                 | 21       | 226 56.2            | 112 08.8 55.1     | 155 12.7 35.7     | 45 00.9 36.7      |        |              |  |
|                                 | 22       | 241 58.6            | 127 08.0 54.6     | 170 13.3 36.0     | 60 03.2 36.6      |        |              |  |
| 23                              | 257 01.1 | 142 07.2 54.1       | 185 13.9 36.2     | 75 05.5 36.5      |                   |        |              |  |
| h m s                           |          |                     |                   |                   |                   |        |              |  |
| Veri Poss.                      | 5 58.7   | t <sup>1</sup> -0.8 | d 0.4             | v 0.6             | d 0.3             | v 2.3  | d 0.1        |  |

| m  | SUN     | ARIES  | MOON   | v or Corr |
|----|---------|--------|--------|-----------|
| 25 | PLANETS |        |        | d         |
| 00 | 6 15-0  | 6 16-0 | 5 57-9 | 0-0 0-0   |
| 01 | 6 15-3  | 6 16-3 | 5 58-2 | 0-1 0-0   |
| 02 | 6 15-5  | 6 16-5 | 5 58-4 | 0-2 0-1   |
| 03 | 6 15-8  | 6 16-8 | 5 58-6 | 0-3 0-1   |
| 04 | 6 16-0  | 6 17-0 | 5 58-9 | 0-4 0-2   |
| 45 | 6 26-3  | 6 27-3 | 6 08-7 | 4-5 1-9   |
| 46 | 6 26-5  | 6 27-6 | 6 08-9 | 4-6 2-0   |
| 47 | 6 26-8  | 6 27-8 | 6 09-1 | 4-7 2-0   |
| 48 | 6 27-0  | 6 28-1 | 6 09-4 | 4-8 2-0   |
| 49 | 6 27-3  | 6 28-3 | 6 09-6 | 4-9 2-1   |

# Azimuth Problems

Step 6: Enter HO229 with whole values of latitude, declination (same in this case), and LHA. By increasing the value of each argument by 1 whole increment, triple interpolate for the exact values of each for the desired time/location.

|                 | Base Value | Base Z | Next incremental Z | Difference in Z | Increment | Correction<br>(Diff Z x Increment) / 60 |
|-----------------|------------|--------|--------------------|-----------------|-----------|-----------------------------------------|
| Latitude – N    | 28°        |        |                    |                 | 30.0'     |                                         |
| Declination - N | 0°         |        |                    |                 | 37.7'     |                                         |
| LHA             | 80°        |        |                    |                 | 57.4'     |                                         |

| 80°, 280° L.H.A. |         |        |        | LATITUDE SAME NAME AS DECLINATION |        |        |         |        |        |         |        |        |         | N. Lat. { L.H.A. greater than 180° ..... Zn=Z<br>L.H.A. less than 180° ..... Zn=360°-Z |        |         |        |        |         |        |        |         |        |        |      |      |       |      |    |      |       |      |   |
|------------------|---------|--------|--------|-----------------------------------|--------|--------|---------|--------|--------|---------|--------|--------|---------|----------------------------------------------------------------------------------------|--------|---------|--------|--------|---------|--------|--------|---------|--------|--------|------|------|-------|------|----|------|-------|------|---|
| Dec.             | 23°     |        |        | 24°                               |        |        | 25°     |        |        | 26°     |        |        | 27°     |                                                                                        |        | 28°     |        |        | 29°     |        |        | 30°     |        |        | Dec. |      |       |      |    |      |       |      |   |
|                  | Hc<br>° | d<br>' | Z<br>" | Hc<br>°                           | d<br>' | Z<br>" | Hc<br>° | d<br>' | Z<br>" | Hc<br>° | d<br>' | Z<br>" | Hc<br>° | d<br>'                                                                                 | Z<br>" | Hc<br>° | d<br>' | Z<br>" | Hc<br>° | d<br>' | Z<br>" | Hc<br>° | d<br>' | Z<br>" |      |      |       |      |    |      |       |      |   |
| 0                | 9       | 11.9   | +23.6  | 93.9                              | 9      | 07.7   | +24.6   | 94.1   | 9      | 03.3    | +25.6  | 94.3   | 8       | 58.7                                                                                   | +26.6  | 94.4    | 8      | 54.0   | +27.5   | 94.6   | 8      | 49.2    | +28.4  | 94.7   | 8    | 44.1 | +29.4 | 94.9 | 8  | 39.0 | +30.2 | 95.0 | 0 |
| 1                | 9       | 35.5   | +23.6  | 93.0                              | 9      | 32.3   | +24.5   | 93.2   | 9      | 28.9    | +25.5  | 93.3   | 9       | 25.3                                                                                   | +26.4  | 93.5    | 9      | 21.5   | +27.4   | 93.7   | 9      | 17.6    | +28.3  | 93.8   | 9    | 13.5 | +29.2 | 94.0 | 9  | 09.2 | +30.2 | 94.2 | 1 |
| 2                | 9       | 59.1   | +23.3  | 92.1                              | 9      | 56.8   | +24.4   | 92.3   | 9      | 54.4    | +25.3  | 92.4   | 9       | 51.7                                                                                   | +26.3  | 92.6    | 9      | 48.9   | +27.2   | 92.8   | 9      | 45.9    | +28.2  | 92.9   | 9    | 42.7 | +29.1 | 93.1 | 9  | 39.4 | +30.0 | 93.3 | 2 |
| 3                | 10      | 22.4   | +23.3  | 91.1                              | 10     | 21.2   | +24.1   | 91.3   | 10     | 19.7    | +25.1  | 91.5   | 10      | 18.0                                                                                   | +26.1  | 91.7    | 10     | 16.1   | +27.1   | 91.9   | 10     | 14.1    | +28.0  | 92.0   | 10   | 11.8 | +29.0 | 92.2 | 10 | 09.4 | +29.9 | 92.4 | 3 |
| 4                | 10      | 45.7   | +23.0  | 90.2                              | 10     | 45.3   | +24.1   | 90.4   | 10     | 44.8    | +25.0  | 90.6   | 10      | 44.1                                                                                   | +26.0  | 90.8    | 10     | 43.2   | +26.9   | 91.0   | 10     | 42.1    | +27.9  | 91.2   | 10   | 40.8 | +28.8 | 91.3 | 10 | 39.3 | +29.7 | 91.5 | 4 |
| 5                | 11      | 08.7   | +22.9  | 89.3                              | 11     | 09.4   | +23.8   | 89.5   | 11     | 09.8    | +24.8  | 89.7   | 11      | 10.1                                                                                   | +25.8  | 89.9    | 11     | 10.1   | +26.8   | 90.1   | 11     | 10.0    | +27.7  | 90.2   | 11   | 09.6 | +28.7 | 90.4 | 11 | 09.0 | +29.6 | 90.6 | 5 |
| 6                | 11      | 31.6   | +22.6  | 88.3                              | 11     | 33.2   | +23.7   | 88.5   | 11     | 34.6    | +24.7  | 88.7   | 11      | 35.9                                                                                   | +25.6  | 88.9    | 11     | 36.9   | +26.6   | 89.1   | 11     | 37.7    | +27.5  | 89.3   | 11   | 38.3 | +28.4 | 89.5 | 11 | 38.6 | +29.4 | 89.8 | 6 |
| 7                | 11      | 54.2   | +22.5  | 87.4                              | 11     | 56.9   | +23.5   | 87.6   | 11     | 59.3    | +24.4  | 87.8   | 12      | 01.5                                                                                   | +25.4  | 88.0    | 12     | 03.5   | +26.4   | 88.2   | 12     | 05.2    | +27.4  | 88.4   | 12   | 06.7 | +28.3 | 88.7 | 12 | 08.0 | +29.3 | 88.9 | 7 |
| 8                | 12      | 16.7   | +22.3  | 86.4                              | 12     | 20.4   | +23.2   | 86.6   | 12     | 23.7    | +24.3  | 86.9   | 12      | 26.9                                                                                   | +25.3  | 87.1    | 12     | 29.9   | +26.2   | 87.3   | 12     | 32.6    | +27.1  | 87.5   | 12   | 35.0 | +28.2 | 87.7 | 12 | 37.3 | +29.0 | 88.0 | 8 |
| 9                | 12      | 39.0   | +22.1  | 85.5                              | 12     | 43.6   | +23.1   | 85.7   | 12     | 48.0    | +24.1  | 85.9   | 12      | 52.2                                                                                   | +25.0  | 86.2    | 12     | 56.1   | +26.0   | 86.4   | 12     | 59.7    | +27.0  | 86.6   | 13   | 03.2 | +27.9 | 86.8 | 13 | 06.3 | +28.9 | 87.1 | 9 |

| 81°, 279° L.H.A. |    |      |       | LATITUDE SAME NAME AS DECLINATION |    |      |       |      |    |      |       |      |     | N. Lat. { L.H.A. greater than 180° .....Zn=Z<br>L.H.A. less than 180° .....Zn=360°-Z |       |      |    |      |       |      |    |      |       |      |      |      |       |      |    |      |       |      |   |
|------------------|----|------|-------|-----------------------------------|----|------|-------|------|----|------|-------|------|-----|--------------------------------------------------------------------------------------|-------|------|----|------|-------|------|----|------|-------|------|------|------|-------|------|----|------|-------|------|---|
| 23°              |    |      |       | 24°                               |    |      | 25°   |      |    | 26°  |       |      | 27° |                                                                                      |       | 28°  |    |      | 29°   |      |    | 30°  |       |      |      |      |       |      |    |      |       |      |   |
| Dec.             | Hc | d    | Z     | Hc                                | d  | Z    | Hc    | d    | Z  | Hc   | d     | Z    | Hc  | d                                                                                    | Z     | Hc   | d  | Z    | Hc    | d    | Z  | Hc   | d     | Z    | Dec. |      |       |      |    |      |       |      |   |
| 0                | 8  | 16.8 | +23.6 | 93.5                              | 8  | 13.0 | +24.6 | 93.7 | 8  | 09.0 | +25.6 | 93.8 | 8   | 05.0                                                                                 | +26.5 | 94.0 | 8  | 00.7 | +27.5 | 94.1 | 7  | 56.4 | +28.3 | 94.3 | 7    | 51.8 | +29.3 | 94.4 | 7  | 47.2 | +30.2 | 94.5 | 0 |
| 1                | 8  | 40.4 | +23.5 | 92.6                              | 8  | 37.6 | +24.4 | 92.8 | 8  | 34.6 | +25.4 | 92.9 | 8   | 31.5                                                                                 | +26.3 | 93.1 | 8  | 28.2 | +27.3 | 93.2 | 8  | 24.7 | +28.3 | 93.4 | 8    | 21.1 | +29.2 | 93.5 | 8  | 17.4 | +30.1 | 93.7 | 1 |
| 2                | 9  | 03.9 | +23.3 | 91.7                              | 9  | 02.0 | +24.4 | 91.8 | 9  | 00.0 | +25.3 | 92.0 | 8   | 57.8                                                                                 | +26.3 | 92.2 | 8  | 55.5 | +27.2 | 92.3 | 8  | 53.0 | +28.1 | 92.5 | 8    | 50.3 | +29.1 | 92.6 | 8  | 47.5 | +30.0 | 92.8 | 2 |
| 3                | 9  | 27.2 | +23.2 | 90.7                              | 9  | 26.4 | +24.1 | 90.9 | 9  | 25.3 | +25.2 | 91.1 | 9   | 24.1                                                                                 | +26.1 | 91.2 | 9  | 22.7 | +27.1 | 91.4 | 9  | 21.1 | +28.0 | 91.6 | 9    | 19.4 | +28.9 | 91.7 | 9  | 17.5 | +29.9 | 91.9 | 3 |
| 4                | 9  | 50.4 | +23.1 | 89.8                              | 9  | 50.5 | +24.1 | 90.0 | 9  | 50.5 | +24.9 | 90.2 | 9   | 50.2                                                                                 | +26.0 | 90.3 | 9  | 49.8 | +26.9 | 90.5 | 9  | 49.1 | +27.9 | 90.7 | 9    | 48.3 | +28.8 | 90.9 | 9  | 47.4 | +29.7 | 91.0 | 4 |
| 5                | 10 | 13.5 | +22.9 | 88.9                              | 10 | 14.6 | +23.8 | 89.1 | 10 | 15.4 | +24.9 | 89.2 | 10  | 16.2                                                                                 | +25.8 | 89.4 | 10 | 16.7 | +26.7 | 89.6 | 10 | 17.0 | +27.7 | 89.8 | 10   | 17.1 | +28.7 | 90.0 | 10 | 17.1 | +29.6 | 90.1 | 5 |
| 6                | 10 | 36.4 | +22.7 | 87.9                              | 10 | 38.4 | +23.7 | 88.1 | 10 | 40.3 | +24.7 | 88.3 | 10  | 42.0                                                                                 | +25.6 | 88.5 | 10 | 43.4 | +26.6 | 88.7 | 10 | 44.7 | +27.6 | 88.9 | 10   | 45.8 | +28.5 | 89.1 | 10 | 46.7 | +29.4 | 89.3 | 6 |
| 7                | 10 | 59.1 | +22.5 | 87.0                              | 11 | 02.1 | +23.5 | 87.2 | 11 | 05.0 | +24.5 | 87.4 | 11  | 07.6                                                                                 | +25.5 | 87.6 | 11 | 10.0 | +26.5 | 87.8 | 11 | 12.3 | +27.3 | 88.0 | 11   | 14.3 | +28.3 | 88.2 | 11 | 16.1 | +29.3 | 88.4 | 7 |
| 8                | 11 | 21.6 | +22.4 | 86.0                              | 11 | 25.6 | +23.4 | 86.2 | 11 | 29.5 | +24.3 | 86.5 | 11  | 33.1                                                                                 | +25.3 | 86.7 | 11 | 36.5 | +26.2 | 86.9 | 11 | 39.6 | +27.3 | 87.1 | 11   | 42.6 | +28.2 | 87.3 | 11 | 45.4 | +29.1 | 87.5 | 8 |
| 9                | 11 | 44.0 | +22.1 | 85.1                              | 11 | 49.0 | +23.2 | 85.3 | 11 | 53.8 | +24.1 | 85.5 | 11  | 58.4                                                                                 | +25.1 | 85.7 | 12 | 02.7 | +26.1 | 85.9 | 12 | 06.9 | +27.0 | 86.2 | 12   | 10.8 | +28.0 | 86.4 | 12 | 14.5 | +28.9 | 86.6 | 9 |

|             | Base Value | Base Z | Next incremental Z | Difference in Z | Increment | Correction<br>(Diff Z x Increment) / 60 |
|-------------|------------|--------|--------------------|-----------------|-----------|-----------------------------------------|
| Latitude    | 28°        | 94.7°  |                    |                 | 30.0'     |                                         |
| Declination | 0°         | 94.7°  |                    |                 | 37.7'     |                                         |
| LHA         | 80°        | 94.7°  |                    |                 | 57.4'     |                                         |

|             | Base Value | Base Z | Next incremental Z | Difference in Z | Increment | Correction<br>(Diff Z x Increment) / 60 |
|-------------|------------|--------|--------------------|-----------------|-----------|-----------------------------------------|
| Latitude    | 28°        | 94.7°  | 94.9°              | 0.2°            | 30.0'     |                                         |
| Declination | 0°         | 94.7°  | 93.8°              | -0.9°           | 37.7'     |                                         |
| LHA         | 80°        | 94.7°  | 94.3°              | -0.4°           | 57.4'     |                                         |

|             | Base Value | Base Z | Next incremental Z | Difference in Z | Increment | Correction<br>(Diff Z x Increment) / 60 |
|-------------|------------|--------|--------------------|-----------------|-----------|-----------------------------------------|
| Latitude    | 28°        | 94.7°  | 94.9°              | 0.2°            | 30.0'     | +0.10°                                  |
| Declination | 0°         | 94.7°  | 93.8°              | -0.9°           | 37.7'     | -0.57°                                  |
| LHA         | 80°        | 94.7°  | 94.3°              | -0.4°           | 57.4'     | -0.38°                                  |

$$\text{Total correction} = 0.10^\circ - 0.57^\circ - 0.38^\circ = \underline{-0.9^\circ}$$

## Azimuth Problems

- Step 7: Apply the correction to the base values to determine true azimuth.  
 Base azimuth:  $094.7^\circ$   
 Correction:  $-0.9^\circ$   
 Corrected azimuth:  $094.7^\circ - 0.9^\circ = 093.8^\circ$   
 Azimuth rules correction:  $360^\circ - 93.8^\circ = \underline{266.2^\circ}$   
*Note - Check azimuth rules: if LHA less than  $180^\circ$ , then  $zn = 360^\circ - z$ .*
- Step 8: Answer the required questions.  
 T:  $266.2^\circ$  (Determine in Step 7)  
 V:  $13.5^\circ$  E (Given)  
 M:  $252.7^\circ$  (Calculated)  
**D:  $2.3^\circ$  E**  
 C:  $250.4^\circ$  (Given)

Note this problem can be solved without the triple interpolation using the formula:

$$\tan Z = \left( \frac{\cos d \sin LHA}{(\cos L)(\sin d) - (\sin L)(\cos d)(\cos LHA)} \right), \text{ where:}$$

LHA is local hour angle  
 L is latitude  
 d is declination



# Azimuth Problems

AZI D4. On 4 October your 1907 zone time DR position is latitude  $25^{\circ} 15.0' S$ , longitude  $105^{\circ} 44.0' E$ . At that time, you observe Deneb bearing  $011.5^{\circ}$  psc. The chronometer reads 00h 07m 42s and the chronometer error is 00m 36s fast. The variation is  $7.5^{\circ} W$ . What is the deviation of the standard compass?

Answer:  $3.2^{\circ} E$

Step 1: Determine the correct chronometer time of the sight.

Chronometer: 00h 07m 42s

Chronometer error: 00m 36s fast

Correct chronometer time: 00h 07m 42s – 36s = 00h 07m 06s

Step 2: Determine the GMT of the sight.

Ship time: 1907

Chronometer time: 00h 07m 06s

DR Longitude:  $105^{\circ} 44' E$  – corresponds to (-7 ZD)

GMT of sight: 12:07:06, 4 October

Step 3: Determine the declination of Deneb.

Declination (total): N  $45^{\circ} 13.2'$

Step 4: Determine the GHA of Deneb.

GHA (Aries - hours):  $193^{\circ} 05.3'$

GHA (Aries - increment):  $1^{\circ} 46.8'$

GHA (Aries - total):  $194^{\circ} 52.1'$

SHA (Deneb):  $49^{\circ} 47.8'$

GHA (Deneb):  $244^{\circ} 39.9'$

Step 5: Determine the LHA of Deneb.

GHA (Deneb):  $244^{\circ} 39.9'$

DR Longitude:  $105^{\circ} 44.0' E$  (subtract west, add east)

LHA (Deneb):  $244^{\circ} 39.9' + 105^{\circ} 44.0' E = \underline{350^{\circ} 23.9'}$

| G.M.T. | ARIES    |              |         | VENUS -3.7   |      |  | MARS +1.7    |      |  | JUPITER -1.2 |      |  | SATURN +1.0  |      |  | STARS      |              |      |
|--------|----------|--------------|---------|--------------|------|--|--------------|------|--|--------------|------|--|--------------|------|--|------------|--------------|------|
|        | G.H.A.   | Dec.         |         | G.H.A.       | Dec. |  | G.H.A.       | Dec. |  | G.H.A.       | Dec. |  | G.H.A.       | Dec. |  | Name       | S.H.A.       | Dec. |
| 4 00   | 12 35.7  | 141 09.3 S20 | 45.7    | 229 55.9 N16 | 05.3 |  | 175 04.4 S 6 | 15.6 |  | 180 10.5 S 2 | 55.6 |  | 195 12.6     | 55.7 |  | Acomar     | 315 36.3 S40 | 22.6 |
| 01     | 27 38.2  | 156 08.9     | 46.5    | 244 56.8     | 04.8 |  | 190 06.4     | 15.8 |  | 195 12.6     | 55.7 |  | 210 14.8     | 55.8 |  | Achernar   | 335 44.1 S57 | 19.7 |
| 02     | 42 40.6  | 171 08.5     | 47.4    | 259 57.8     | 04.4 |  | 205 08.4     | 16.0 |  | 210 14.8     | 55.8 |  | 225 17.0     | 56.0 |  | Acrux      | 173 37.2 S62 | 59.7 |
| 03     | 57 43.1  | 186 08.0     | 48.3    | 274 58.7     | 03.9 |  | 220 10.3     | 16.2 |  | 225 17.0     | 56.0 |  | 240 19.2     | 56.1 |  | Adhara     | 255 31.6 S28 | 56.6 |
| 04     | 72 45.6  | 201 07.6     | 49.1    | 289 59.7     | 03.5 |  | 235 12.3     | 16.4 |  | 240 19.2     | 56.1 |  | 255 21.4     | 56.2 |  | Aldebaran  | 291 17.0 N16 | 28.4 |
| 05     | 87 48.0  | 216 07.1     | 50.0    | 305 00.7     | 03.0 |  | 250 14.2     | 16.6 |  | 255 21.4     | 56.2 |  | 270 23.5 S 2 | 56.3 |  | Alioth     | 166 42.4 N56 | 03.7 |
| 06     | 102 50.5 | 231 06.7 S20 | 50.8    | 320 01.6 N16 | 02.6 |  | 265 16.2 S 6 | 16.8 |  | 270 23.5 S 2 | 56.3 |  | 285 25.7     | 56.4 |  | Alkaid     | 153 18.4 N49 | 24.5 |
| 07     | 117 53.0 | 246 06.2     | 51.7    | 335 02.6     | 02.1 |  | 280 18.2     | 17.0 |  | 285 25.7     | 56.4 |  | 300 27.9     | 56.6 |  | Al Na'ir   | 28 13.7 S47  | 03.1 |
| 08     | 132 55.4 | 261 05.8     | 52.5    | 350 03.6     | 01.6 |  | 295 20.1     | 17.2 |  | 300 27.9     | 56.6 |  | 315 30.1     | 56.7 |  | Alnilam    | 276 10.8 S 1 | 12.7 |
| S 09   | 147 57.9 | 276 05.3     | 53.4    | 5 04.5       | 01.2 |  | 310 22.1     | 17.4 |  | 315 30.1     | 56.7 |  | 330 32.3     | 56.8 |  | Alphard    | 218 20.1 S 8 | 34.5 |
| U 10   | 163 00.3 | 291 04.9     | 54.2    | 20 05.5      | 00.7 |  | 325 24.1     | 17.6 |  | 330 32.3     | 56.8 |  | 345 34.4     | 56.9 |  | Alphecca   | 126 31.8 N26 | 46.9 |
| N 11   | 178 02.8 | 306 04.4     | 55.1    | 35 06.5      | 00.3 |  | 340 26.0     | 17.8 |  | 345 34.4     | 56.9 |  | 0 36.6 S 2   | 57.0 |  | Alpheratz  | 358 08.2 N28 | 59.4 |
| D 12   | 193 05.3 | 321 04.0 S20 | 55.9    | 50 07.4 N15  | 59.8 |  | 355 28.0 S 6 | 18.0 |  | 0 36.6 S 2   | 57.0 |  | 15 38.8      | 57.1 |  | Altair     | 62 31.8 N 8  | 49.3 |
| A 13   | 208 07.7 | 336 03.5     | 56.7    | 65 08.4      | 59.4 |  | 10 29.9      | 18.2 |  | 15 38.8      | 57.1 |  | 25 31.9      | 57.3 |  | Ankaa      | 353 39.1 S42 | 24.3 |
| Y 14   | 223 10.2 | 351 03.1     | 57.6    | 80 09.3      | 58.9 |  | 25 31.9      | 18.5 |  | 25 31.9      | 57.3 |  | 40 33.9      | 57.4 |  | Antares    | 112 56.2 S26 | 23.4 |
| 15     | 238 12.7 | 6 02.6       | 58.4    | 95 10.3      | 58.5 |  | 40 33.9      | 18.7 |  | 40 33.9      | 57.4 |  | 55 35.8      | 57.5 |  | Arcturus   | 146 18.1 N19 | 16.9 |
| 16     | 253 15.1 | 21 02.2      | 59.3    | 110 11.3     | 58.0 |  | 55 35.8      | 18.9 |  | 55 35.8      | 57.5 |  | 70 37.8      | 57.6 |  | Atria      | 108 20.1 S68 | 59.9 |
| 17     | 268 17.6 | 36 01.7      | 21 00.1 | 125 12.2     | 57.6 |  | 70 37.8      | 19.1 |  | 70 37.8      | 57.6 |  | 85 39.7 S 6  | 19.3 |  | Avior      | 234 28.2 S59 | 26.7 |
| 18     | 283 20.1 | 51 01.3 S21  | 01.0    | 140 13.2 N15 | 57.1 |  | 85 39.7 S 6  | 19.3 |  | 85 39.7 S 6  | 19.3 |  | 100 41.7     | 19.5 |  | Bellatrix  | 278 57.9 N 6 | 20.1 |
| 19     | 298 22.5 | 66 00.8      | 01.8    | 155 14.2     | 56.6 |  | 100 41.7     | 19.5 |  | 105 51.9     | 57.9 |  | 115 43.7     | 19.7 |  | Betelgeuse | 271 27.4 N 7 | 24.3 |
| 20     | 313 25.0 | 81 00.4      | 02.6    | 170 15.1     | 56.2 |  | 115 43.7     | 19.7 |  | 120 54.1     | 58.0 |  | 130 45.6     | 19.9 |  | Canopus    | 264 06.8 S52 | 40.8 |
| 21     | 328 27.5 | 95 59.9      | 03.5    | 185 16.1     | 55.7 |  | 130 45.6     | 19.9 |  | 135 56.3     | 58.1 |  | 145 47.6     | 20.1 |  | Copella    | 281 10.1 N45 | 58.7 |
| 22     | 343 29.9 | 110 59.5     | 04.3    | 200 17.1     | 55.3 |  | 145 47.6     | 20.1 |  | 150 58.4     | 58.2 |  | 160 49.6     | 20.3 |  | Deneb      | 49 47.8 N45  | 13.2 |
| 23     | 358 32.4 | 125 59.0     | 05.1    | 215 18.0     | 54.8 |  | 160 49.6     | 20.3 |  | 166 00.6     | 58.3 |  | 175 51.5 S 6 | 20.5 |  | Denebola   | 182 58.6 N14 | 40.7 |
| 5 00   | 13 34.8  | 140 58.6 S21 | 06.0    | 230 19.0 N15 | 54.4 |  | 175 51.5 S 6 | 20.5 |  | 181 02.8 S 2 | 58.5 |  | 196 05.0     | 58.6 |  | Diphda     | 349 19.8 S18 | 05.2 |
| 01     | 28 37.3  | 155 58.1     | 06.8    | 245 20.0     | 53.9 |  | 190 53.5     | 20.7 |  | 196 05.0     | 58.6 |  | 211 07.2     | 58.7 |  |            |              |      |
| 02     | 43 39.8  | 170 57.7     | 07.7    | 260 20.9     | 53.4 |  | 205 55.4     | 20.9 |  | 211 07.2     | 58.7 |  | 226 09.3     | 58.8 |  |            |              |      |
| 03     | 58 42.2  | 185 57.2     | 08.5    | 275 21.9     | 53.0 |  | 220 57.4     | 21.1 |  | 226 09.3     | 58.8 |  | 241 11.5     | 58.9 |  |            |              |      |
| 04     | 73 44.7  | 200 56.8     | 09.3    | 290 22.9     | 52.5 |  | 235 59.4     | 21.3 |  | 241 11.5     | 58.9 |  |              |      |  |            |              |      |

| m  | SUN     | ARIES  |
|----|---------|--------|
| 7  | PLANETS |        |
| 00 | 1 45-0  | 1 45-3 |
| 01 | 1 45-3  | 1 45-5 |
| 02 | 1 45-5  | 1 45-8 |
| 03 | 1 45-8  | 1 46-0 |
| 04 | 1 46-0  | 1 46-3 |
| 05 | 1 46-3  | 1 46-5 |
| 06 | 1 46-5  | 1 46-8 |
| 07 | 1 46-8  | 1 47-0 |
| 08 | 1 47-0  | 1 47-3 |
| 09 | 1 47-3  | 1 47-5 |

# Azimuth Problems

Step 6: Enter HO229 with whole values of latitude, declination (contrary in this case), and LHA. By increasing the value of each argument by 1 whole increment, triple interpolate for the exact values of each for the desired time/location.

| LATITUDE CONTRARY NAME TO DECLINATION |                     |                     |                     |                     |                     |                     | L.H.A. 9°, 351° |
|---------------------------------------|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|-----------------|
| 24°                                   | 25°                 | 26°                 | 27°                 | 28°                 | 29°                 | 30°                 | Dec.            |
| Hc d Z                                | Hc d Z              | Hc d Z              | Hc d Z              | Hc d Z              | Hc d Z              | Hc d Z              |                 |
| 21 30.1 -59.3 173.1                   | 20 30.5 -59.3 173.1 | 19 30.9 -59.3 173.1 | 18 31.4 -59.4 173.2 | 17 31.8 -59.4 173.2 | 16 32.2 -59.4 173.3 | 15 32.6 -59.4 173.3 | 44              |
| 20 30.8 -59.3 173.2                   | 19 31.2 -59.3 173.3 | 18 31.6 -59.3 173.3 | 17 32.0 -59.4 173.3 | 16 32.4 -59.4 173.4 | 15 32.8 -59.4 173.4 | 14 33.2 -59.4 173.4 | 45              |
| 19 31.5 -59.4 173.4                   | 18 31.9 -59.4 173.4 | 17 32.3 -59.4 173.5 | 16 32.6 -59.3 173.5 | 15 33.0 -59.4 173.5 | 14 33.4 -59.4 173.6 | 13 33.8 -59.4 173.6 | 46              |
| 18 32.1 -59.3 173.5                   | 17 32.5 -59.3 173.6 | 16 32.9 -59.4 173.6 | 15 33.3 -59.4 173.6 | 14 33.6 -59.3 173.7 | 13 34.0 -59.4 173.7 | 12 34.4 -59.5 173.7 | 47              |
| 17 32.8 -59.3 173.7                   | 16 33.2 -59.4 173.7 | 15 33.5 -59.3 173.8 | 14 33.9 -59.4 173.8 | 13 34.3 -59.4 173.8 | 12 34.6 -59.4 173.8 | 11 34.9 -59.4 173.9 | 48              |
| 16 33.5 -59.3 173.9                   | 15 33.8 -59.3 173.9 | 14 34.2 -59.4 173.9 | 13 34.5 -59.4 173.9 | 12 34.9 -59.4 174.0 | 11 35.2 -59.4 174.0 | 10 35.5 -59.4 174.0 | 49              |
| 15 34.2 -59.4 174.0                   | 14 34.5 -59.4 174.0 | 13 34.8 -59.3 174.1 | 12 35.1 -59.3 174.1 | 11 35.5 -59.4 174.1 | 10 35.8 -59.4 174.1 | 9 36.1 -59.4 174.1  | 50              |

| LATITUDE CONTRARY NAME TO DECLINATION |                     |                     |                     |                     |                     |                     | L.H.A. 10°, 350° |
|---------------------------------------|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|------------------|
| 24°                                   | 25°                 | 26°                 | 27°                 | 28°                 | 29°                 | 30°                 | Dec.             |
| Hc d Z                                | Hc d Z              | Hc d Z              | Hc d Z              | Hc d Z              | Hc d Z              | Hc d Z              |                  |
| 21 23.1 -59.2 172.3                   | 20 23.6 -59.2 172.3 | 19 24.1 -59.1 172.4 | 18 24.7 -59.2 172.4 | 17 25.2 -59.2 172.5 | 16 25.7 -59.3 172.5 | 15 26.2 -59.3 172.6 | 44               |
| 20 23.9 -59.1 172.5                   | 19 24.4 -59.1 172.5 | 18 25.0 -59.2 172.6 | 17 25.5 -59.3 172.6 | 16 26.0 -59.3 172.6 | 15 26.4 -59.2 172.7 | 14 26.9 -59.2 172.7 | 45               |
| 19 24.8 -59.2 172.7                   | 18 25.3 -59.2 172.7 | 17 25.8 -59.2 172.7 | 16 26.2 -59.2 172.8 | 15 26.7 -59.2 172.8 | 14 27.2 -59.3 172.8 | 13 27.7 -59.3 172.9 | 46               |
| 18 25.6 -59.1 172.8                   | 17 26.1 -59.2 172.9 | 16 26.6 -59.2 172.9 | 15 27.0 -59.2 172.9 | 14 27.5 -59.3 173.0 | 13 27.9 -59.2 173.0 | 12 28.4 -59.3 173.0 | 47               |
| 17 26.5 -59.2 173.0                   | 16 26.9 -59.2 173.0 | 15 27.4 -59.2 173.1 | 14 27.8 -59.2 173.1 | 13 28.2 -59.2 173.1 | 12 28.7 -59.3 173.2 | 11 29.1 -59.3 173.2 | 48               |
| 16 27.3 -59.2 173.2                   | 15 27.7 -59.2 173.2 | 14 28.2 -59.3 173.2 | 13 28.6 -59.3 173.3 | 12 29.0 -59.3 173.3 | 11 29.4 -59.3 173.3 | 10 29.8 -59.3 173.3 | 49               |
| 15 28.1 -59.1 173.3                   | 14 28.5 -59.2 173.4 | 13 28.9 -59.2 173.4 | 12 29.3 -59.2 173.4 | 11 29.7 -59.2 173.5 | 10 30.1 -59.3 173.5 | 9 30.5 -59.3 173.5  | 50               |

|                 | Base Value | Base Z | Next incremental Z | Difference in Z | Increment | Correction<br>(Diff Z x Increment) / 60 |
|-----------------|------------|--------|--------------------|-----------------|-----------|-----------------------------------------|
| Latitude - S    | 25°        |        |                    |                 | 15.0'     |                                         |
| Declination - N | 45°        |        |                    |                 | 13.2'     |                                         |
| LHA             | 350°       |        |                    |                 | 23.9'     |                                         |

|             | Base Value | Base Z | Next incremental Z | Difference in Z | Increment | Correction<br>(Diff Z x Increment) / 60 |
|-------------|------------|--------|--------------------|-----------------|-----------|-----------------------------------------|
| Latitude    | 25°        | 172.5° |                    |                 | 15.0'     |                                         |
| Declination | 45°        | 172.5° |                    |                 | 13.2'     |                                         |
| LHA         | 350°       | 172.5° |                    |                 | 23.9'     |                                         |

|             | Base Value | Base Z | Next incremental Z | Difference in Z | Increment | Correction<br>(Diff Z x Increment) / 60 |
|-------------|------------|--------|--------------------|-----------------|-----------|-----------------------------------------|
| Latitude    | 25°        | 172.5° | 172.6°             | 0.1°            | 15.0'     |                                         |
| Declination | 45°        | 172.5° | 172.7°             | 0.2°            | 13.2'     |                                         |
| LHA         | 350°       | 172.5° | 173.3°             | 0.8°            | 23.9'     |                                         |

|             | Base Value | Base Z | Next incremental Z | Difference in Z | Increment | Correction<br>(Diff Z x Increment) / 60 |
|-------------|------------|--------|--------------------|-----------------|-----------|-----------------------------------------|
| Latitude    | 25°        | 172.5° | 172.6°             | 0.1°            | 15.0'     | +0.00°                                  |
| Declination | 45°        | 172.5° | 172.7°             | 0.2°            | 13.2'     | +0.00°                                  |
| LHA         | 350°       | 172.5° | 173.3°             | 0.8°            | 23.9'     | +0.32°                                  |

$$\text{Total correction} = 0.0^\circ + 0.0^\circ + 0.32^\circ = \underline{+0.3^\circ}$$

## Azimuth Problems

- Step 7: Apply the correction to the base values to determine true azimuth.  
 Base azimuth:  $172.5^\circ$   
 Correction:  $+0.3^\circ$   
 Corrected azimuth:  $172.5^\circ + 0.3^\circ = 172.8^\circ$   
 Azimuth rules correction:  $180^\circ - 172.8^\circ = \underline{007.2^\circ}$   
*Note - Check azimuth rules: if LHA greater than  $180^\circ$ , then  $zn = 180^\circ - z$ .*
- Step 8: Answer the required questions.  
 T:  $007.2^\circ$  (Determine in Step 7)  
 V:  $7.5^\circ$  W (Given)  
 M:  $14.7^\circ$  (Calculated)  
**D:  $3.2^\circ$  E**  
 C:  $011.5^\circ$  (Given)

Note this problem can be solved without the triple interpolation using the formula:

$$\tan Z = \left( \frac{\cos d \sin LHA}{((\cos L)(\sin d) - (\sin L)(\cos d)(\cos LHA))} \right), \text{ where:}$$

LHA is local hour angle  
 L is latitude  
 d is declination

## Azimuth Problems

### Azimuth of Polaris Problems

- Refer to the Latitude by Polaris section for more detail on theory regarding Local Hour Angle (LHA) and Polaris problems in general.

AZI D5. On 5 February your 2320 ZT position is latitude  $52^{\circ} 28' N$ , longitude  $23^{\circ} 48' W$ . You observe Polaris bearing  $000.2^{\circ}$  pgc. At the time of observation, the helmsman noted that she was heading  $224^{\circ}$  pgc and  $244^{\circ}$  psc. The variation is  $20^{\circ} W$ . What is the deviation for that heading?

Answer:  $1.5^{\circ} W$ .

| 34     |    |          |
|--------|----|----------|
|        |    | ARIES    |
| G.M.T. |    | G.H.A.   |
| d      | h  | m        |
| 6      | 00 | 136 02.4 |
| 01     |    | 151 04.9 |
| 02     |    | 166 07.4 |
| 03     |    | 181 09.8 |
| 04     |    | 196 12.3 |
| 05     |    | 211 14.8 |

- Step 1: Determine the GMT of the sight.  
 DR Longitude:  $23^{\circ} 48' W$  - corresponds to ZD (+2).  
 Local time of observation: 2320 ZT  
 GMT time of observation = 2320 ZT + 2 hours = 0120 GMT (6 Feb).

- Step 2: Determine the GHA of Aries for the time of sight.  
 GHA (Aries), whole hours:  $151^{\circ} 04.9'$   
 GHA (Aries), increment:  $5^{\circ} 00.8'$   
 GHA (Aries), total:  $151^{\circ} 04.9' + 5^{\circ} 00.8' = 156^{\circ} 05.7'$

| 20 <sup>m</sup> |             |        |
|-----------------|-------------|--------|
| 20              | SUN PLANETS | ARIES  |
| s               | m           | s      |
| 00              | 5 00.0      | 5 00.8 |
| 01              | 5 00.3      | 5 01.1 |
| 02              | 5 00.5      | 5 01.3 |
| 03              | 5 00.8      | 5 01.6 |
| 04              | 5 01.0      | 5 01.8 |

- Step 3: Determine the LHA of Aries.  
 GHA (Aries):  $156^{\circ} 05.7'$   
 DR Longitude:  $23^{\circ} 48' W$   
 LHA (Aries) =  $156^{\circ} 05.7' - 23^{\circ} 48' W = 132^{\circ} 17.7'$

- Step 4: Enter the Polaris Tables with LHA (Aries), DR Latitude, and Month to determine the azimuth to Polaris  
Azimuth (interpolated) =  $358.7^{\circ}$

- Step 5: Determine the gyro compass error.  
 G (Gyro):  $000.2^{\circ}$  pgc  
 E (Error): TBD  
 T (True):  $358.7^{\circ}$  per azimuth tables  
 Gyro error =  $1.5^{\circ} W$

| L.H.A. ARIES | $120^{\circ}-129^{\circ}$ | $130^{\circ}-139^{\circ}$ |
|--------------|---------------------------|---------------------------|
| Lat.         |                           |                           |
| 0            | 359.2                     | 359.2                     |
| 20           | 359.1                     | 359.1                     |
| 40           | 358.9                     | 359.0                     |
| 50           | 358.7                     | 358.8                     |
| 55           | 358.6                     | 358.6                     |

- Step 6: Determine the deviation.  
 G:  $224^{\circ}$  pgc (Given)  
 E:  $1.5^{\circ} W$  (Determine in step 5)  
 T:  $222.5^{\circ}$  (Calculated)  
 V:  $20^{\circ} W$  (Given)  
 M:  $242.5^{\circ}$  (Calculated)  
**D:  $1.5^{\circ} W$  (Calculated)**  
 C:  $244^{\circ}$  per steering compass (Given)

## Azimuth Problems

### Azimuth of the Sun

AZI B1. On 17 April your 1610 zone time DR position is latitude  $22^{\circ} 07.0' \text{ N}$ , longitude  $158^{\circ} 16.0' \text{ W}$ . At that time, you observe the Sun bearing  $271^{\circ} \text{ psc}$ . The chronometer reads 03h 08m 52s and the chronometer error is 01m 16s slow. The variation is  $4^{\circ} \text{ E}$ . What is the deviation of the standard magnetic compass?

- a)  $1.1^{\circ} \text{ W}$
- b)  $1.7^{\circ} \text{ E}$
- c)  **$2.3^{\circ} \text{ W}$  - correct**
- d)  $2.9^{\circ} \text{ E}$

AZI B2. On 21 April, your 1542 zone time DR position is latitude  $28^{\circ} 54.0' \text{ S}$ . Longitude  $19^{\circ} 07.0' \text{ W}$ . At that time, you observe the Sun bearing  $299^{\circ} \text{ psc}$ . The chronometer reads 04h 44m 11s and the chronometer error is 01m 54s fast. The variation is  $3^{\circ} \text{ E}$ . What is the deviation of the standard compass?

- a)  **$0.3^{\circ} \text{ W}$  - correct**
- b)  $0.4^{\circ} \text{ E}$
- c)  $2.7^{\circ} \text{ W}$
- d)  $2.7^{\circ} \text{ E}$

AZI B3. On 1 September your 1115 zone time DR position is latitude  $25^{\circ} 20' \text{ N}$ , longitude  $28^{\circ} 24' \text{ W}$ . At that time, you observe the Sun bearing  $160.5^{\circ} \text{ psc}$ . The chronometer reads 01h 14m 58s and the chronometer error is 01m 17s fast. The variation is  $13.5^{\circ} \text{ W}$ . What is the deviation of the standard compass?

- a)  **$2.1^{\circ} \text{ E}$  - correct**
- b)  $4.1^{\circ} \text{ E}$
- c)  $11.0^{\circ} \text{ W}$
- d)  $11.0^{\circ} \text{ E}$

AZI B4. On 24 May, your vessel's 1000 ZT position is latitude  $25^{\circ} 36.0' \text{ N}$ , longitude  $118^{\circ} 39.5' \text{ W}$ , when you observe an azimuth of the Sun. Determine the gyro error using the azimuth information:

Chronometer time: 06h 21m 48s

Chronometer error: Fast 01m 36s

Gyro bearing:  $099.4^{\circ}$

Variation:  $11.1^{\circ} \text{ E}$

- a)  $0.3^{\circ} \text{ W}$
- b)  **$1.3^{\circ} \text{ W}$  - correct**
- c)  $1.8^{\circ} \text{ E}$
- d)  $2.4^{\circ} \text{ E}$

### Azimuth of Stars/Planets Problems

AZI B5. On 5 June your 0420 zone time DR position is latitude  $26^{\circ} 47.0'$  N, longitude  $133^{\circ} 19.5'$  W. At that time, you observe Vega bearing  $298.1^{\circ}$  psc. The chronometer reads 01h 21m 17s, and the chronometer error is 02m 25s fast. The variation is  $3.5^{\circ}$  E. What is the deviation of the standard compass?

- a)  $1.8^{\circ}$  E
- b)  $5.2^{\circ}$  E
- c)  **$1.8^{\circ}$  W - correct**
- d)  $5.2^{\circ}$  W

AZI B6. On 6 October your 0416 zone time DR position is latitude  $25^{\circ} 16.0'$  N, longitude  $130^{\circ} 25.0'$  E. At that time, you observe Mars bearing  $083^{\circ}$  psc. The chronometer reads 07h 16m 22s and the chronometer error is 10s fast. The variation is  $1.5^{\circ}$  E. What is the deviation of the standard compass?

- a)  $0.4^{\circ}$  E
- b)  **$1.2^{\circ}$  W - correct**
- c)  $3.5^{\circ}$  E
- d)  $19.0^{\circ}$  E

AZI B7. On 28 July your 1937 zone time DR position is latitude  $26^{\circ} 13.0'$  N, longitude  $78^{\circ} 27.0'$  E. At that time, you observe Deneb bearing  $048.7^{\circ}$  psc. The chronometer reads 02h 37m 42s and the chronometer error is 00m 15s fast. The variation is  $4^{\circ}$  W. What is the gyro error?

- a)  $2.4^{\circ}$  W
- b)  **$2.8^{\circ}$  E - correct**
- c)  $3.6^{\circ}$  W
- d)  $3.6^{\circ}$  E

AZI B8. On 2 March your 2216 zone time DR position is latitude  $21^{\circ} 20.0'$  S, longitude  $17^{\circ} 10.0'$  W. At that time, you observe Saturn bearing  $078^{\circ}$  psc. The chronometer reads 11h 14m 04s and the chronometer error is 02m 20s slow. The variation is  $4.5^{\circ}$  W. What is the deviation of the standard compass?

- a)  $1.5^{\circ}$  W
- b)  $1.6^{\circ}$  E
- c)  $2.9^{\circ}$  W
- d)  **$3.6^{\circ}$  E - correct**

### Azimuth of Polaris Problems

AZI B9. On 11 January your 0450 ZT position is latitude  $38^{\circ} 42'$  N, longitude  $14^{\circ} 16'$  W. You observe Polaris bearing  $358.5^{\circ}$  pgc. At the time of observation, the helmsman noted he was heading  $160^{\circ}$  pgc and  $173^{\circ}$  psc. The variation is  $9^{\circ}$  W. What is the deviation for that heading?

- a)  $1^{\circ}$  E
- b)  $1^{\circ}$  W
- c)  **$3^{\circ}$  W - correct**
- d)  $13^{\circ}$  W

AZI B10. On 19 November, your 0146 ZT position is latitude  $33^{\circ} 48'$  N, longitude  $25^{\circ} 22'$  E. You observe Polaris bearing  $359.8^{\circ}$  pgc. At the time of observation, the helmsman noted that he was heading  $224^{\circ}$  pgc and  $222.5^{\circ}$  psc. The variation is  $2^{\circ}$  E. What is the deviation for that heading?

- a)  $2.0^{\circ}$  E
- b)  $0.5^{\circ}$  E
- c)  **$1.0^{\circ}$  W - correct**
- d)  $1.5^{\circ}$  W

AZI B11. On 23 July, your 2100 ZT position is latitude  $36^{\circ} 43.0'$  N, longitude  $16^{\circ} 09.8'$  W, when you observe an azimuth of Polaris to determine compass error. Polaris bears  $359.0^{\circ}$  per gyrocompass. At the time of the observation, the helmsman noted that he was heading  $319^{\circ}$  per gyrocompass and  $331^{\circ}$  per standard compass. Variation is  $12.0^{\circ}$  W. Which of the following statements is TRUE?

- a) The gyro error is  $0.7^{\circ}$  E
- b) The gyro error is  $1.7^{\circ}$  W
- c) **The deviation is  $1.7^{\circ}$  E - correct**
- d) The compass error is  $13.7^{\circ}$  W

AZI B12. On 3 October your 0330 zone time (ZD +5) DR position is latitude  $47^{\circ} 41'$  N, longitude  $86^{\circ} 49'$  W. At that time, you observe Polaris bearing  $357.5^{\circ}$  pgc. The chronometer time of observation is 08h 32m 04s and the chronometer is 0m 27s slow. The variation is  $5.5^{\circ}$  W. What is the gyro error?

- a)  $7.5^{\circ}$  E
- b)  $5.0^{\circ}$  E
- c)  $3.5^{\circ}$  E
- d)  **$2.0^{\circ}$  E - correct**





## **Mercator Sailing Problems**



## Mercator Sailings Problems

- Terms:
  - DLo – the difference in two longitudes.
  - L is latitude.
  - DLat or  $l$  is the difference between two latitudes.
  - Cn or C is the course/course angle. Course angle is the course measured from  $0^\circ$  at the reference direction clockwise or counterclockwise through  $90^\circ$  or  $180^\circ$ . It is labeled with the reference direction as a prefix and the direction of measurement from the reference direction as a suffix. For example, a true course of  $330^\circ$  T would be noted as N  $30^\circ$  W.
  - D is distance in nautical miles.
  - m is the Meridional parts. The actual length of an arc from the equator to a given latitude, given along a longitude/meridian line. The Meridional Parts Table in Bowditch provides this value.
    - m1 – the meridional parts of the point of departure.
    - m2 – the meridional parts of the destination.
- The main Mercator sailing formula needed are:
  - $l = D \cos C$ , which can be restated as  $D = l \left( \frac{1}{\cos C} \right)$
  - $DLo = m \tan C$
  - $\tan C = \frac{DLo}{m}$

## Mercator Sailings Problems

### Mercator Latitude and Longitude Problems

MER D1. You depart latitude  $40^{\circ} 42.0' \text{ N}$ , longitude  $074^{\circ} 01.0' \text{ W}$  and steam 3365.6 miles on course  $118^{\circ} \text{ T}$ . What is the longitude of your arrival by Mercator Sailing?

Answer:  $17^{\circ} 40.62' \text{ W}$ .

Step 1: Convert standard latitude and longitudes to decimal form:

Departure Location

$$40^{\circ} 42.0' \text{ N} = 40.70^{\circ} \text{ N}$$

$$74^{\circ} 01.0' \text{ W} = 74.02^{\circ} \text{ W}$$

Step 2: Determine the Course Angle:

$$\text{Course} = 118^{\circ} \text{ T}$$

$$\text{Course Angle} = \text{S } 62^{\circ} \text{ E}$$

Step 3: Determine the Difference of Latitude ( $l$ ) given the known course and distance. Then convert the mileage to arc.

$$l = D \cos C$$

$$l = (3365.6) \cos(62^{\circ})$$

$$l = (3365.6) (0.4695)$$

$$l = 1580.05'$$

$$l = 1580.05' \div 60 = 26.3342^{\circ}$$

Step 4: Given that the initial course was to the southeast, subtract the Difference of Latitude ( $l$ ) from the initial latitude to determine the arrival latitude.

$$\text{Departure Latitude: } 40.70^{\circ} \text{ N}$$

$$\text{Difference of Latitude: } -26.3342^{\circ}$$

$$\text{Arrival Latitude} = 40.70^{\circ} - 26.3342^{\circ} = 14.366^{\circ} = 14^{\circ} 22.0' \text{ N}$$

Step 5: Use the Meridional Parts Table in Bowditch to obtain the meridional parts ( $m1$  and  $m2$ ) for the given latitudes.

$$\text{Latitude 1: } 40^{\circ} 42.0'$$

$$\text{Meridional Parts 1: } m1 = 2662.8$$

$$\text{Latitude 2: } 14^{\circ} 22.0'$$

$$\text{Meridional Parts 2: } m2 = 865.4$$

Step 6: Determine the difference in meridional parts ( $m$ ).

$$m1 - m2 = m$$

$$2662.8 - 865.4 = m = 1797.4$$

## Mercator Sailings Problems

Step 7: Determine the Difference in Longitude (*DLo*). Convert the mileage to arc.

$$DLo = m \tan C$$

$$DLo = (1797.4) \tan 62^\circ$$

$$DLo = (1797.4) (1.8807)$$

$$DLo = 3380.42'$$

$$DLo = 3380.42' \div 60 = 56.34^\circ$$

Step 8: Determine the arrival longitude using the Difference of Longitude (*DLo*).

$$\text{Departure Longitude: } 74.017^\circ = 74^\circ 01.0' \text{ W}$$

$$\text{Difference of Longitude: } 56.34^\circ = 56^\circ 20.4'$$

$$\text{Arrival Longitude} = 74.017^\circ - 56.34^\circ = 17.677^\circ = \mathbf{17^\circ 40.62' \text{ N}}$$

## Mercator Sailings Problems

### Mercator Course and Distance Problems

MER D2. A vessel at latitude  $45^{\circ} 36.0' \text{ N}$ , longitude  $011^{\circ} 36.0' \text{ W}$  heads for a destination at latitude  $24^{\circ} 16.0' \text{ N}$ , longitude  $073^{\circ} 52.0' \text{ W}$ . Determine the true course and distance by Mercator sailing.

Answer:  $247.2^{\circ} \text{ T}$ , 3299.2 nm.

Step 1: Convert standard latitude and longitudes to decimal form:

Departure Location

$$45^{\circ} 36.0' \text{ N} = 45.600^{\circ} \text{ N}$$

$$11^{\circ} 36.0' \text{ W} = 11.600^{\circ} \text{ W}$$

Arrival Location

$$24^{\circ} 16.0' \text{ N} = 24.267^{\circ} \text{ N}$$

$$73^{\circ} 52.0' \text{ W} = 73.867^{\circ} \text{ W}$$

Step 2: Determine the Difference of Latitude ( $l$ ). Convert to minutes of arc.

$$l = 45.600^{\circ} \text{ N} - 24.267^{\circ} \text{ N} = 21.333^{\circ}$$

$$l = 21.333^{\circ} \times 60 = 1279.98'$$

Step 3: Determine the Difference in Longitude ( $DLo$ ). Convert to minutes of arc.

$$DLo = 11.600^{\circ} \text{ W} - 73.867^{\circ} \text{ W} = 62.267^{\circ}$$

$$DLo = 62.267^{\circ} \times 60 = 3736.02'$$

Step 4: Use the Meridional Parts Table in Bowditch to obtain the meridional parts ( $m1$  and  $m2$ ) for the given latitudes.

Latitude 1:  $45^{\circ} 36.0'$

Meridional Parts 1:  $m1 = 3064.7$

Latitude 2:  $24^{\circ} 16.0'$

Meridional Parts 2:  $m2 = 1492.1$

Step 5: Determine the difference in meridional parts ( $m$ ).

$$m1 - m2 = m$$

$$3064.7 - 1492.1 = m = 1572.6$$

## Mercator Sailings Problems

Step 6: Determine the Course Angle ( $C$ ).

$$\begin{aligned}
 DLo &= m \tan C \\
 \tan C &= \frac{DLo}{m} \\
 \tan C &= \frac{3736.02'}{1572.6} \\
 \tan C &= 2.3756 \\
 C &= \tan^{-1} 2.3756 \\
 C &= 67.172
 \end{aligned}$$

Step 7: Determine the actual course steered given the solved course angle. Note that the vessel headed in a SW direction given the initial and final positions. Therefore, the course angle  $67.172^\circ$  is expressed as S  $67.172^\circ$  W. You can round final answers to nearest tenth.

$$\begin{aligned}
 C &= \text{S } 67.172^\circ \text{ W} \\
 180^\circ + 67.172^\circ \text{ W} &= \mathbf{247.172^\circ \text{ T} = 247.2^\circ \text{ T}}
 \end{aligned}$$

Step 8: Determine the distance travelled using the Plane Sailing formula.

$$\begin{aligned}
 l &= D \cos C \\
 D &= l \left( \frac{1}{\cos C} \right) \\
 D &= (1279.98) \left( \frac{1}{\cos 247.2} \right) \\
 D &= (1279.98) \left( \frac{1}{(0.3875)} \right) \\
 D &= (1279.98) (2.5806) \\
 \mathbf{D} &= \mathbf{3303.2 \text{ nm}}
 \end{aligned}$$

## Mercator Sailing Problems

### Mercator Latitude and Longitude

MER B1. A vessel steams 1082 miles on course  $047^{\circ}$  T from latitude  $37^{\circ} 18.0'$  N, longitude  $24^{\circ} 40.0'$  W. What is the latitude and longitude of the point of arrival by Mercator sailing?

- a)  $49^{\circ} 30'$  N,  $6^{\circ} 22'$  W
- b)  $49^{\circ} 33'$  N,  $6^{\circ} 25'$  W
- c)  **$49^{\circ} 36'$  N,  $6^{\circ} 28'$  W - correct**
- d)  $49^{\circ} 39'$  N,  $6^{\circ} 31'$  W

MER B2. A vessel steams 1650 miles on course  $077^{\circ}$  T from latitude  $12^{\circ} 47'$  N, longitude  $45^{\circ} 10'$  E. What is the latitude and longitude of the point of arrival by Mercator sailing?

- a)  $18^{\circ} 54'$  N,  $72^{\circ} 58'$  E
- b)  **$18^{\circ} 58'$  N,  $72^{\circ} 52'$  E - correct**
- c)  $19^{\circ} 02'$  N,  $72^{\circ} 44'$  E
- d)  $19^{\circ} 06'$  N,  $72^{\circ} 36'$  E

MER B3. You depart latitude  $49^{\circ} 45.0'$  N, longitude  $6^{\circ} 35.0'$  W and steam 3599 miles on course  $246.5^{\circ}$  T. What is the longitude of your arrival by Mercator sailing?

- a)  $76^{\circ} 36.2'$  W
- b)  **$77^{\circ} 02.8'$  W - correct**
- c)  $78^{\circ} 14.0'$  W
- d)  $78^{\circ} 22.6'$  W



### Mercator Course and/or Distance

MER B4. Your vessel departs latitude  $32^{\circ} 45' \text{ N}$ , longitude  $79^{\circ} 50' \text{ W}$ , and is bound for latitude  $34^{\circ} 21' \text{ S}$ , longitude  $18^{\circ} 29' \text{ E}$ . Determine the distance by Mercator sailing.

- a) 5,021 miles
- b) 6,884 miles - correct**
- c) 6,954 miles
- d) 7,002 miles

MER B5. Your vessel receives a distress call from a vessel reporting her position as latitude  $35^{\circ} 01' \text{ S}$ , longitude  $18^{\circ} 51' \text{ W}$ . Your position is latitude  $30^{\circ} 18' \text{ S}$ , longitude  $21^{\circ} 42' \text{ W}$ . Determine the true course from your vessel to the vessel in distress by Mercator sailing.

- a)  $135^{\circ} \text{ T}$
- b)  $149^{\circ} \text{ T}$
- c)  $153^{\circ} \text{ T}$  - correct**
- d)  $160^{\circ} \text{ T}$

MER B6. A vessel at latitude  $32^{\circ} 14.7' \text{ N}$ , longitude  $66^{\circ} 28.9' \text{ W}$  heads for a destination at latitude  $36^{\circ} 58.7' \text{ N}$ , longitude  $75^{\circ} 42.2' \text{ W}$ . Determine the true course by Mercator sailing.

- a)  $058.2^{\circ} \text{ T}$
- b)  $235.2^{\circ} \text{ T}$
- c)  $301.8^{\circ} \text{ T}$  - correct**
- d)  $348.3^{\circ} \text{ T}$

MER B7. A vessel at latitude  $10^{\circ} 22' \text{ S}$ , longitude  $7^{\circ} 18' \text{ E}$  heads for a destination at latitude  $6^{\circ} 54' \text{ N}$ , longitude  $57^{\circ} 23' \text{ W}$ . Determine the course and distance by Mercator sailing.

- a)  $285^{\circ} \text{ T}$ , 3825.3 miles
- b)  $285^{\circ} \text{ T}$ , 4025.7 miles - correct**
- c)  $296^{\circ} \text{ T}$ , 3825.3 miles
- d)  $296^{\circ} \text{ T}$ , 4025.7 miles

MER B8. A vessel at latitude  $18^{\circ} 54' \text{ N}$ , longitude  $73^{\circ} 00' \text{ E}$  heads for a destination at latitude  $13^{\circ} 12' \text{ N}$ , longitude  $54^{\circ} 00' \text{ E}$ . Determine the true course and distance by Mercator sailing.

- a)  $247^{\circ} \text{ T}$ , 1161 miles
- b)  $250^{\circ} \text{ T}$ , 1172 miles
- c)  $253^{\circ} \text{ T}$ , 1154 miles - correct**
- d)  $256^{\circ} \text{ T}$ , 1136 miles

MER B9. A vessel at latitude  $21^{\circ} 18.5' \text{ N}$ , longitude  $157^{\circ} 52.2' \text{ W}$  heads for a destination at latitude  $8^{\circ} 53.0' \text{ N}$ , longitude  $79^{\circ} 31.0' \text{ W}$ . Determine the true course and distance by Mercator sailing.

- a)  $081^{\circ} \text{ T}$ , 4617.5 miles
- b)  $081^{\circ} \text{ T}$ , 4915.8 miles
- c)  $099^{\circ} \text{ T}$ , 4617.5 miles - correct**
- d)  $099^{\circ} \text{ T}$ , 4915.8 miles

MER B10. A vessel at latitude  $29^{\circ} 38.0' \text{ N}$ , longitude  $93^{\circ} 49.0' \text{ W}$  heads for a destination at latitude  $24^{\circ} 38.0' \text{ N}$ , longitude  $82^{\circ} 55.2' \text{ W}$ . Determine the true course and distance by Mercator sailing.

- a)  $115^{\circ} \text{ T}$ , 637 miles
- b)  $117^{\circ} \text{ T}$ , 658 miles - correct**
- c)  $122^{\circ} \text{ T}$ , 648 miles
- d)  $126^{\circ} \text{ T}$ , 665 miles

## **Middle Latitude Sailing Problems**



## Mid Latitude Sailings Problems

- Terms:
  - DLo is the difference in two longitudes.
  - $\lambda 1$  is the starting longitude.
  - $\lambda 2$  is the ending longitude.
  - $p$  is departure. The distance between two meridians at any given parallel of latitude.
  - $L1$  is the starting latitude.
  - $L2$  is the ending latitude.
  - DLat or  $l$  is the difference between two latitudes.
  - $Lm$  is the middle latitude, the average of the starting and ending latitudes.
  - $Cn$  or  $C$  is the course/course angle. Course angle is the course measured from  $0^\circ$  at the reference direction clockwise or counterclockwise through  $90^\circ$  or  $180^\circ$ . It is labeled with the reference direction as a prefix and the direction of measurement from the reference direction as a suffix. For example, a true course of  $330^\circ$  T would be noted as N  $30^\circ$  W.
  - $D$  is distance in nautical miles.
- The main formula needed are:
  - $l = D \cos C$
  - $p = D \sin C$
  - $DLo = \frac{p}{\cos Lm}$
  - $\tan C = \frac{p}{l}$
- Mid Latitude Sailing involves the use of the mid (or middle) latitude for converting departure ( $p$ ) to difference in longitude (DLo) when the course is not due east or west, and it is assumed such course is steered at the mid latitude.
- Bowditch article 1006 provides background knowledge on this task and is available during Coast Guard exams.

## Mid Latitude Sailings Problems

### Mid Latitude Sailings Course and Distance

MLS D1. A vessel in latitude  $20^{\circ} 00' \text{ N}$ , longitude  $107^{\circ} 30' \text{ W}$  is to proceed to latitude  $24^{\circ} 40' \text{ N}$ , longitude  $112^{\circ} 30' \text{ W}$ . What is the course and distance by mid-latitude sailing?

Answer: Course  $315.27^{\circ} \text{ T}$ , 394.4 nm.

Step 1: Convert standard latitude and longitudes to decimal form:

Departure Location

$$20^{\circ} 00' \text{ N} = 20.0^{\circ} \text{ N}$$

$$107^{\circ} 30' \text{ W} = 107.5^{\circ} \text{ W}$$

Arrival Location

$$24^{\circ} 40' \text{ N} = 24.67^{\circ} \text{ N}$$

$$112^{\circ} 30' \text{ W} = 112.5^{\circ} \text{ W}$$

Step 2: Determine the mid-latitude ( $L_m$ ).

$$L_m = (20.0^{\circ} \text{ N} + 24.67^{\circ} \text{ N}) \div 2 = 22.33^{\circ} \text{ N}$$

Step 3: Determine the Difference of Latitude ( $l$ ) and convert to arc minutes to determine  $l$ .

$$DLat = 24.67^{\circ} - 20.0^{\circ} = 4.67^{\circ}$$

$$l = 4.67^{\circ} \times 60 = 280.2'$$

Step 4: Determine the Difference of Longitude ( $DLo$ ) and convert to arc minutes.

$$112.5^{\circ} \text{ W} - 107.5^{\circ} \text{ W} = 5.0^{\circ} = 300'$$

Step 5: Determine the Departure ( $p$ ).

$$p = DLo \cos L_m$$

$$p = 300' \cos(22.33)$$

$$p = (300) (0.9250)$$

$$p = 277.49'$$

Step 6: Determine the Course Angle ( $C$ ).

$$\tan C = \frac{p}{l}$$

$$\tan C = \frac{277.49}{280.2}$$

$$\tan C = 0.9903$$

$$C = \tan^{-1} 0.9903$$

$$C = 44.722^{\circ}$$

## Mid Latitude Sailings Problems

Step 7: Determine the distance.

$$D = l \sec C$$

$$D = (280.2) \sec(44.722)$$

$$D = (280.2) \left( \frac{1}{\cos 44.722} \right)$$

$$D = (280.2) \left( \frac{1}{0.7105} \right)$$

$$\mathbf{D = 394.4 \text{ nm}}$$

Step 8: Determine the actual course given the solved Course Angle ( $C$ ). Also note that the vessel clearly headed in a northwesterly direction based on the origin and destination points. Therefore, the course is given by:

$$\text{Course} = 360^\circ - C$$

$$\text{Course} = 360^\circ - 44.722^\circ$$

$$\mathbf{\text{Course} = 315.278^\circ}$$

## Mid Latitude Sailings Problems

### Mid Latitude Sailings Arrival Position

MLS D2. A vessel steams 640 miles on course 047° T from latitude 34° 45' N, longitude 140° 00' E. What are the latitude and longitude of arrival by mid-latitude sailing?

Answer: 42° 01.5' N, 149° 57.2' E

Step 1: Convert standard latitude and longitudes to decimal form:

Departure Location

$$34^{\circ} 45' \text{ N} = 34.750^{\circ} \text{ N}$$

$$140^{\circ} 00' \text{ E} = 140.000^{\circ} \text{ E}$$

Step 2: Determine the Difference in Latitude ( $l$ ) and convert to decimal notation.

$$l = D \cos C$$

$$l = (640) \cos(047^{\circ})$$

$$l = (640) (0.6820)$$

$$l = 436.5'$$

$$436.5' \div 60 = 7.275^{\circ} \text{ (to the north based on initial course).}$$

Step 3: Determine the arrival latitude using the Difference in Latitude ( $l$ ). Convert to standard notation for partial problem answer.

$$\text{Latitude 1} = 34.750^{\circ} \text{ N}$$

$$\text{Difference in Latitude} = 7.275^{\circ} \text{ to the north.}$$

$$\text{Latitude 2} = 34.750^{\circ} + 7.275^{\circ} = 42.025^{\circ} \text{ N} = \mathbf{42^{\circ} 01.5' \text{ N}}$$

Step 4: Determine the mid latitude using the Difference in Latitude ( $l$ ) and arrival latitude.

$$\text{Latitude 1} = 34.750^{\circ} \text{ N}$$

$$\text{Latitude 2} = 42.025^{\circ} \text{ N}$$

$$\text{Mid Lat} = \frac{34.750^{\circ} + 42.025^{\circ}}{2} = 38.388^{\circ}$$

Step 5: Determine the Departure ( $p$ ).

$$p = D \sin C$$

$$p = (640) \sin 47^{\circ}$$

$$p = (640) (0.7313)$$

$$p = 468.1'$$



## Mid Latitude Sailings Problems

Step 6: Determine the Difference in Longitude (*DLo*) given the departure and mid-latitude.

$$DLo = p \left( \frac{1}{\cos Lm} \right)$$

$$DLo = p \left( \frac{1}{\cos Lm} \right)$$

$$DLo = (468.1') \left( \frac{1}{\cos 38.388^\circ} \right)$$

$$DLo = (468.1') \left( \frac{1}{(0.7838)} \right)$$

$$DLo = (468.1') (1.2758)$$

$$DLo = 597.2'$$

Step 7: Convert the Difference in Longitude (*DLo*) to decimal notation and determine the arrival longitude. Convert to standard notation for partial problem answer.

$$DLo = 597.2' \div 60 = 9.953^\circ \text{ (to the east based on initial course).}$$

$$\text{Longitude 1} = 140.000^\circ \text{ E}$$

$$\text{Difference in Longitude} = 9.953^\circ \text{ to the east.}$$

$$\text{Longitude 2} = 140.000^\circ + 9.953^\circ = 149.953^\circ \text{ E}$$

$$149.953^\circ \text{ E} = \mathbf{149^\circ 57.2' \text{ E}}$$

## Mid Latitude Sailings Problems

### Mid Latitude Sailings Course and Distance

MLS B1. A vessel at latitude  $14^{\circ} 10' \text{N}$ , longitude  $61^{\circ} 00' \text{W}$  is to proceed to latitude  $10^{\circ} 00' \text{N}$ , longitude  $53^{\circ} 23' \text{W}$ . What is the course and distance by mid-latitude sailing?

- a)  $117.3^{\circ} \text{ T}$  for 503 miles
- b)  $117.9^{\circ} \text{ T}$  for 504 miles
- c)  $118.6^{\circ} \text{ T}$  for 508 miles
- d)  $119.2^{\circ} \text{ T}$  for 512 miles - correct

MLS B2. A vessel at latitude  $20^{\circ} 00' \text{N}$ , longitude  $107^{\circ} 30' \text{W}$  is to proceed to latitude  $24^{\circ} 40' \text{N}$ , longitude  $112^{\circ} 30' \text{W}$ . What is the course and distance by mid-latitude sailing?

- a)  $314.0^{\circ} \text{ T}$  for 389 miles
- b)  $315.3^{\circ} \text{ T}$  for 394 miles - correct
- c)  $317.2^{\circ} \text{ T}$  for 397 miles
- d)  $318.3^{\circ} \text{ T}$  for 399 miles

MLS B3. A vessel at latitude  $20^{\circ} 10' \text{N}$ , longitude  $122^{\circ} 00' \text{E}$  is to proceed to latitude  $26^{\circ} 18' \text{N}$ , longitude  $128^{\circ} 20' \text{E}$ . What are the course and distance by mid-latitude sailing?

- a)  $041.2^{\circ} \text{ T}$  for 501 miles
- b)  $041.9^{\circ} \text{ T}$  for 503.6 miles
- c)  $043.5^{\circ} \text{ T}$  for 507.3 miles - correct
- d)  $044.7^{\circ} \text{ T}$  for 509.7 miles

### Mid Latitude Sailings Arrival

MLS B4. A vessel steams 576 miles on course  $260^{\circ}$  T from latitude  $40^{\circ} 36' \text{N}$ , longitude  $50^{\circ} 24' \text{W}$ . What are the latitude and longitude of the point of arrival by mid-latitude sailing?

- a)  $39^{\circ} 12' \text{N}$ ,  $62^{\circ} 28' \text{W}$
- b)  $39^{\circ} 06' \text{N}$ ,  $62^{\circ} 34' \text{W}$
- c)  $39^{\circ} 02' \text{N}$ ,  $62^{\circ} 37' \text{W}$
- d)  $38^{\circ} 56' \text{N}$ ,  $62^{\circ} 42' \text{W}$  - correct

MLS B5. A vessel steams 580 miles on course  $083^{\circ}$  T from latitude  $13^{\circ} 12' \text{N}$ ,  $71^{\circ} 12' \text{W}$ . What are the latitude and longitude of the point of arrival by mid-latitude sailing?

- a)  $14^{\circ} 17' \text{N}$ ,  $61^{\circ} 23' \text{W}$
- b)  $14^{\circ} 20' \text{N}$ ,  $61^{\circ} 21' \text{W}$
- c)  $14^{\circ} 23' \text{N}$ ,  $61^{\circ} 19' \text{W}$  - correct
- d)  $14^{\circ} 25' \text{N}$ ,  $61^{\circ} 17' \text{W}$

MLS B6. A vessel steams 640 miles on course  $047^{\circ}$  T from latitude  $34^{\circ} 45' \text{N}$ , longitude  $140^{\circ} 00' \text{E}$ . What are the latitude and longitude of the point of arrival by mid-latitude sailing?

- a)  $41^{\circ} 57' \text{N}$ ,  $150^{\circ} 02' \text{E}$
- b)  $42^{\circ} 01' \text{N}$ ,  $149^{\circ} 57' \text{E}$  - correct
- c)  $42^{\circ} 06' \text{N}$ ,  $149^{\circ} 53' \text{E}$
- d)  $42^{\circ} 09' \text{N}$ ,  $149^{\circ} 50' \text{E}$



## **Parallel Sailing Problems**



## Parallel Sailings Problems

- Terms:
  - DLo – the difference in two longitudes.
  - p is departure. The distance between two meridians at any given parallel of latitude.
  - L is latitude. For parallel sailing problems, the latitude does not change since the course is either 090° T or 270° T.
- The main parallel sailing formula needed is:
  - $DLo = \frac{p}{\cos l}$  which can be re-arranged as  $p = DLo \cos L$
- The main parallel sailing formula is identical to the mid-latitude formula, given that when determining Difference in Longitude (DLo), it is assumed a vessel is proceeding along a parallel, e.g. parallel sailing.

## Parallel Sailings Problems

PAR D1. You depart latitude  $52^{\circ} 01' \text{N}$  longitude  $176^{\circ} 09' \text{E}$  to latitude  $52^{\circ} 01' \text{N}$ ,  $178^{\circ} 46' \text{W}$ .  
what are the course and distance by parallel sailing?

Answer:  $090^{\circ} \text{T}$ , 188 miles.

Step 1: Convert standard latitude and longitudes to decimal form:

Departure Location

$$52^{\circ} 01' \text{N} = 52.017^{\circ} \text{N}$$

$$176^{\circ} 09' \text{E} = 176.150^{\circ} \text{E}$$

Arrival Longitude

$$178^{\circ} 46' \text{W} = 178.766^{\circ} \text{W}$$

Step 2: Determine the Course and Difference of Longitude (DLo).

$$\text{Long 1} = 176.150^{\circ} \text{E}$$

$$\text{Long 2} = 178.766^{\circ} \text{W}$$

$$\text{Eastern Hemisphere Distance } (180^{\circ} - 176.150^{\circ}) = 3.85^{\circ} \text{ to the east}$$

$$\text{Western Hemisphere Distance } (180^{\circ} - 178.766^{\circ}) = 1.234^{\circ} \text{ to the east}$$

$$\text{Total DLo} = 3.85^{\circ} + 1.234^{\circ} = 5.084^{\circ} \text{ to the east (e.g. course } 090^{\circ} \text{T)}$$

$$\text{DLo converted to minutes} = 5.084^{\circ} \times 60 = 305'$$

Step 3: Determine the Departure (same as distance for parallel sailing problems) using the parallel sailing formula.

$$\text{DLo} = p \sec l = p \left( \frac{1}{\cos L} \right)$$

$$p = (\text{DLo})(\cos L) \quad - \text{Rearranged terms}$$

$$p = (305')(\cos 52.017^{\circ})$$

$$p = (305')(0.6154)$$

$$p = 187.7 \text{ miles}$$



## Parallel Sailings Problems

PAR D2. You depart latitude  $25^{\circ} 54' \text{ N}$ , longitude  $009^{\circ} 38' \text{ E}$  and steam 592 miles on course  $270^{\circ} \text{ T}$ . What is the longitude of arrival?

Answer  $001^{\circ} 20.1' \text{ W}$ . Since the course is  $270^{\circ}$ , this is strictly a parallel sailing problem.

Step 4: Convert standard latitude and longitudes to decimal form:

Departure Location

$$25^{\circ} 54' \text{ N} = 25.900^{\circ} \text{ N}$$

$$009^{\circ} 38' \text{ E} = 9.633^{\circ} \text{ E}$$

Step 5: Determine the Departure (p).

$$p = D \sin C$$

$$p = (592) \sin(270^{\circ})$$

$$p = (592) (-1.0)$$

$$p = -592'$$

Step 6: Determine the Difference of Longitude (DLo) using the parallel sailing formula.

$$DLo = p \sec l = p \left( \frac{1}{\cos l} \right)$$

$$DLo = (-592') \left( \frac{1}{\cos 25.900^{\circ}} \right)$$

$$DLo = (-592') \left( \frac{1}{0.8996} \right)$$

$$DLo = (-592')(1.1116)$$

$$DLo = -658.1'$$

Step 7: Convert the Difference of Longitude (DLo) into decimal notation.

$$-658.1' \div 60 = -10.968^{\circ} = 10.968^{\circ} \text{ to the west.}$$

Step 8: Sum the longitudes to determine the final longitude.

$$\text{Departure longitude} = 9.633^{\circ} \text{ E}$$

$$\text{Difference in longitude} = 10.968^{\circ} \text{ to the west.}$$

$$\text{Arrival longitude} = 9.633^{\circ} \text{ E} - 10.968^{\circ} \text{ to the west} = -1.335^{\circ}$$

$$-1.335^{\circ} = 1.335^{\circ} \text{ W}$$

Step 9: Convert the arrival longitude to standard notation.

$$1.335^{\circ} \text{ W} = \mathbf{001^{\circ} 20.1' \text{ W}}$$

## Parallel Sailings Problems

PAR D3. You depart latitude  $38^{\circ} 12' \text{ S}$ , longitude  $012^{\circ} 06' \text{ W}$  and steam 1543 miles on course  $270^{\circ} \text{ T}$ . What is the longitude of arrival?

Answer:  $044^{\circ} 49.3' \text{ W}$ . Since the course is  $270^{\circ}$ , this is strictly a parallel sailing problem.

Step 1: Convert standard latitude and longitudes to decimal form:

Departure Location

$$38^{\circ} 12' \text{ S} = 38.200^{\circ} \text{ S}$$

$$012^{\circ} 06' \text{ W} = 12.100^{\circ} \text{ W}$$

Step 2: Determine the Departure (p).

$$p = D \sin C$$

$$p = (1543) \sin(270^{\circ})$$

$$p = (1543) (-1.0)$$

$$p = -1543'$$

Step 3: Determine the Difference of Longitude (DLo) using the parallel sailing formula.

$$DLo = p \sec l = p \left( \frac{1}{\cos l} \right)$$

$$DLo = (-1543') \left( \frac{1}{\cos 38.200^{\circ}} \right)$$

$$DLo = (-1543') \left( \frac{1}{0.7859} \right)$$

$$DLo = (-1543')(1.2724)$$

$$DLo = -1963.3'$$

Step 4: Convert the Difference of Longitude (DLo) into decimal notation.

$$-1963.3' \div 60 = -32.722^{\circ} = 32.722^{\circ} \text{ to the west.}$$

Step 5: Sum the longitudes to determine the final longitude.

$$\text{Departure longitude} = 12.100^{\circ} \text{ W}$$

$$\text{Difference in longitude} = 32.722^{\circ} \text{ to the west.}$$

$$\text{Arrival longitude} = 12.100^{\circ} \text{ W} + 32.722^{\circ} \text{ to the west} = 44.822^{\circ} \text{ W}$$

Step 6: Convert the arrival longitude to standard notation.

$$44.822^{\circ} \text{ W} = \mathbf{044^{\circ} 49.3' \text{ W}}$$

## Parallel Sailings Problems

### Parallel Distance

PAR B1. Determine the distance from latitude  $59^{\circ} 12' N$ , longitude  $14^{\circ} 00' W$  to latitude  $59^{\circ} 12' N$ , longitude  $03^{\circ} 20' W$  by parallel sailing.

- a) 324.2 miles
- b) 325.4 miles
- c) **327.7 miles- correct**
- d) 328.9 miles

PAR B2. Determine the distance from latitude  $34^{\circ} 18' S$ , longitude  $172^{\circ} 40' E$  to latitude  $34^{\circ} 18' S$ , longitude  $152^{\circ} 38' E$  by parallel sailing.

- a) **993.0 miles- correct**
- b) 995.2 miles
- c) 996.4 miles
- d) 998.6 miles

PAR B3. Determine the distance from  $19^{\circ} 54' N$ ,  $166^{\circ} 36' E$  to  $19^{\circ} 54' N$ ,  $157^{\circ} 54' W$  by parallel sailing.

- a) 2204.6 miles
- b) 2006.9 miles
- c) **2002.8 miles - correct**
- d) 1990.6 miles

### Parallel Course and Distance

PAR B4. Your vessel receives a distress call from a vessel reporting her position as latitude  $35^{\circ} 01.0' S$ , longitude  $18^{\circ} 51.0' W$ . Your position is latitude  $35^{\circ} 01.0' S$ , longitude  $21^{\circ} 42.0' W$ . Determine the true course and distance from your vessel to the vessel in distress by parallel sailing.

- a)  **$090^{\circ} T$ , 140.0 miles- correct**
- b)  $090^{\circ} T$ , 189.2 miles
- c)  $270^{\circ} T$ , 140.0 miles
- d)  $270^{\circ} T$ , 189.2 miles

### Parallel Longitude of Arrival

PAR B5. You depart latitude  $15^{\circ} 48' \text{ N}$ , longitude  $174^{\circ} 06' \text{ E}$  and steam 905 miles on course  $090^{\circ} \text{ T}$ . What is the longitude of arrival?

- a)  $165^{\circ} 41' \text{ W}$
- b)  $170^{\circ} 13' \text{ W}$  - correct**
- c)  $172^{\circ} 47' \text{ W}$
- d)  $179^{\circ} 06' \text{ E}$

PAR B6. You depart latitude  $38^{\circ} 12' \text{ S}$ , longitude  $12^{\circ} 06' \text{ W}$  and steam 1543 miles on course  $270^{\circ} \text{ T}$ . What is the longitude of arrival?

- a)  $44^{\circ} 49' \text{ W}$  - correct**
- b)  $45^{\circ} 12' \text{ W}$
- c)  $45^{\circ} 37' \text{ W}$
- d)  $45^{\circ} 42' \text{ W}$

PAR B7. You depart latitude  $25^{\circ} 54' \text{ S}$ , longitude  $9^{\circ} 38' \text{ E}$  and steam 592 miles on course  $270^{\circ} \text{ T}$ . What is the longitude of arrival?

- a)  $1^{\circ} 20' \text{ E}$
- b)  $0^{\circ} 40' \text{ E}$
- c)  $0^{\circ} 40' \text{ W}$
- d)  $1^{\circ} 20' \text{ W}$  - correct**

## **Great Circle Sailing Problems**



## Great Circle Sailings Problems

- Terms:
  - DLo is the difference in two longitudes.
  - $\lambda 1$  is the starting longitude.
  - $\lambda 2$  is the ending longitude.
  - L1 is the starting latitude.
  - L2 is the ending latitude.
  - Vertex is the most poleward position along the great circle route.
  - Lv is the latitude of the vertex.
  - $\lambda v$  is the longitude of the vertex.
  - Lx is the latitude of any spot along the great circle route.
  - DLo(v) is the difference in longitude from the vertex to a point on the great circle route.
  - Cn or C is the course/course angle. Course angle is the course measured from 0° at the reference direction clockwise or counterclockwise through 90° or 180°. It is labeled with the reference direction as a prefix and the direction of measurement from the reference direction as a suffix. For example, a true course of 330° T would be noted as N 30° W.
  - D is distance in nautical miles.
- The main formula needed are:
 

|                                                                                           | <u>Bowditch Formula:</u> |
|-------------------------------------------------------------------------------------------|--------------------------|
| ○ $\sin C = \frac{(\sin DLo)(\cos L2)}{\sin D}$                                           | Formula 24               |
| ○ $\cos Lv = (\cos L1)(\sin C)$                                                           | Formula 25               |
| ○ $\sin DLo(v) = \frac{\cos C}{\sin Lv}$                                                  | Formula 27               |
| ○ $\tan Lx = ((\cos DLo(v))(\tan Lv))$                                                    | Formula 31               |
| ○ $\csc Lx = (\csc Lv)(\sec DVx)$                                                         | Formula 32               |
| ○ $\cos D = ((\sin L1)(\sin L2) + (\cos L1)(\cos L2)(\cos DLo))$                          | Formula 36               |
| ○ $\tan C = \left( \frac{\sin DLo}{((\cos L1)(\tan L2)) - ((\sin L1)(\cos DLo))} \right)$ | Formula 37               |

## Great Circle Sailings Problems

- Bowditch article 1016 provides background knowledge on this task and is available during Coast Guard exams. Additionally, all of Bowditch chapter X is useful for this topic.
- See the article in Bowditch or in this text regarding basic trigonometric functions and particularly how to take the inverse Sin, Cos, and Tan when solving equations.
- Great Circle Sailings questions can come in three main varieties:
  - Seeking the course and/or distance.
  - Seeking the latitude and/or longitude of the vertex.
  - Seeking a position along the great circle route.

### Initial Course and/or Distance

GRC D1. Determine the distance and initial course along a great circle route from 33° 53.3'S, 18° 23.1'E to a position 40° 27.0'N, 73° 49.4'W.

Answer: 6762.7 nm, 304.5° T

Step 1: Convert standard latitude and longitudes to decimal form:

Departure Location

$$33^{\circ} 53.3' \text{ S} = 33.888^{\circ} \text{ S}$$

$$18^{\circ} 23.1' \text{ E} = 18.385^{\circ} \text{ E}$$

Arrival Location

$$40^{\circ} 27.0' \text{ N} = 40.450^{\circ} \text{ N}$$

$$73^{\circ} 49.4' \text{ W} = 73.823^{\circ} \text{ W}$$

Step 2: Determine the Difference in Longitude.

$$\lambda_1 = 18.385^{\circ} \text{ E}$$

$$\lambda_2 = 73.823^{\circ} \text{ W}$$

$$DLo = 18.385^{\circ} + 73.823^{\circ} = 92.208^{\circ} \text{ to the west.}$$

Step 3: Determine the Distance.

$$\cos D = ((\sin L_1)(\sin L_2) + (\cos L_1)(\cos L_2)(\cos DLo))$$

$$\cos D = ((\sin 33.888^{\circ})(\sin -40.450^{\circ}) + (\cos 33.888^{\circ})(\cos -40.450^{\circ})(\cos 92.208^{\circ}))$$

$$\cos D = ((0.5576)(-0.6488) + (0.8301)(0.7610)(-0.0385))$$

$$\cos D = ((-0.3618) + (-0.0243))$$

$$\cos D = -0.3861$$

$$D = 112.7^{\circ} = \mathbf{6762.7nm}$$



## Great Circle Sailings Problems

Step 4: Determine the Course Angle.

$$\sin C = \frac{((\sin DLo)(\cos L2))}{\sin D}$$

$$\sin C = \frac{((\sin 92.208^\circ)(\cos 40.450^\circ))}{\sin 112.7^\circ}$$

$$\sin C = \frac{(0.9993)(0.7610)}{(.9225)}$$

$$\sin C = \frac{(0.7605)}{(.9225)}$$

$$\sin C = 0.8244$$

$$C = 55.5^\circ$$

Because of the departure from the southern hemisphere, the elevated pole is the south pole and the correct course angle notation is S 55.5° W.

However due to the change in hemispheres, the prefix must be reversed, so the correct course angle is N 55.5° W, or **304.5° T**.

## Great Circle Sailings Problems

### Latitude and Longitude of the Vertex Problems

GRC D2. The great circle distance from latitude  $25^{\circ} 50.0' \text{ N}$ , longitude  $077^{\circ} 00.0' \text{ W}$  to latitude  $35^{\circ} 56.0' \text{ N}$ , longitude  $006^{\circ} 15.0' \text{ W}$  is 3616 nautical miles. The initial course is  $061.7^{\circ} \text{ T}$ . Determine the latitude and longitude of the vertex.

Answer:  $37^{\circ} 35' \text{ N}$ ,  $025^{\circ} 59' \text{ W}$

Step 1: Convert standard latitude and longitudes to decimal form:

Departure Location

$$25^{\circ} 50.0' \text{ N} = 25.833^{\circ} \text{ N}$$

$$77^{\circ} 00.0' \text{ W} = 77.000^{\circ} \text{ W}$$

Arrival Location

$$35^{\circ} 56.0' \text{ N} = 35.933^{\circ} \text{ N}$$

$$06^{\circ} 15.0' \text{ W} = 06.250^{\circ} \text{ W}$$

Step 2: Determine the Latitude of the Vertex.

$$Lv = \cos^{-1}((\cos L1)(\sin C))$$

$$Lv = \cos^{-1}((\cos 25.833^{\circ})(\sin 61.7^{\circ}))$$

$$Lv = \cos^{-1}(0.9000)(0.8805)$$

$$Lv = \cos^{-1}(0.7924)$$

$$Lv = 37.587^{\circ}$$

Step 3: Convert the decimal longitude to standard notation.

$$37.587^{\circ} \text{ N} = \mathbf{37^{\circ} 35' \text{ N}}$$

Step 4: Determine the Difference in Longitude of the Vertex ( $DLo(v)$ )

$$DLo(v) = \sin^{-1}\left(\frac{\cos C}{\sin Lv}\right)$$

$$DLo(v) = \sin^{-1}\left(\frac{\cos 61.7^{\circ}}{\sin(37.587^{\circ})}\right)$$

$$DLo(v) = \sin^{-1}\left(\frac{(0.4741)}{(0.6099)}\right)$$

$$DLo(v) = \sin^{-1}(0.7773)$$

$$DLo(v) = 51.02^{\circ}$$

Step 5: Determine the Longitude of the Vertex given the initial longitude and the direction of travel (easterly in this case based on given positions).

$$\text{Longitude 1} = 77.000^{\circ} \text{ W}$$

$$\text{Difference of Long}(vx) = 51.02^{\circ}$$

$$\text{Longitude of the Vertex} = 77.00^{\circ} - 51.02^{\circ} = 25.98^{\circ} \text{ W}$$

Step 6: Convert the decimal longitude to standard notation.

$$25.98^{\circ} \text{ W} = \mathbf{25^{\circ} 59' \text{ W}}$$

## Great Circle Sailings Problems

### Positions Along the Great Circle Route

GRC D3. The great circle distance from latitude  $25^{\circ} 50.0' \text{ N}$ , longitude  $077^{\circ} 00.0' \text{ W}$  to latitude  $35^{\circ} 56.0' \text{ N}$ , longitude  $006^{\circ} 15.0' \text{ W}$  is 3616 nautical miles. The initial course is  $061.7^{\circ} \text{ T}$ . The position of the vertex is  $37^{\circ} 35' \text{ N}$ ,  $25^{\circ} 59' \text{ W}$ . Determine the latitude intersecting the great circle track 600 miles west of the vertex, along the great circle track.

Answer:  $37^{\circ} 09' \text{ N}$

Step 1: Convert standard latitude and longitudes to decimal form:

Departure Location

$$25^{\circ} 50.0' \text{ N} = 25.834^{\circ} \text{ N}$$

$$77^{\circ} 00.0' \text{ W} = 77.000^{\circ} \text{ W}$$

Arrival Location

$$35^{\circ} 56.0' \text{ N} = 35.934^{\circ} \text{ N}$$

$$06^{\circ} 15.0' \text{ W} = 06.250^{\circ} \text{ W}$$

Latitude of the Vertex

$$37^{\circ} 35' \text{ N} = 37.583^{\circ} \text{ N}$$

Longitude of the Vertex

$$25^{\circ} 59' \text{ W} = 25.983^{\circ} \text{ W}$$

Step 2: Convert 600 miles to arc.

$$600 \div 60 = 10^{\circ}$$

Step 3: Determine the latitude at a position 600 miles ( $10^{\circ}$  of arc) west of the vertex along the great circle track.

$$\tan Lx = ((\cos DLo(v))(\tan Lv))$$

$$\tan Lx = ((\cos(10^{\circ}))(\tan 37.583^{\circ}))$$

$$\tan Lx = ((0.9848)(0.7696))$$

$$\tan Lx = (0.7579)$$

$$Lx = 37.158^{\circ}$$

Step 4: Convert the decimal latitude to standard notation.

$$Lx = 37.158^{\circ} = \mathbf{37^{\circ} 09' \text{ N}}$$

## Great Circle Sailing Problems

### Great Circle Initial Course and/or Distance

GRC B1. Determine the great circle initial course from  $29^{\circ} 46'S$ ,  $30^{\circ} 26'E$ , to  $31^{\circ} 52'S$ ,  $115^{\circ} 22'E$ .

- a)  $074^{\circ} T$
- b)  $113^{\circ} T$
- c)  **$117^{\circ} T$  - correct**
- d)  $121^{\circ} T$

GRC B2. Determine the great circle initial course from  $07^{\circ} 05'N$ ,  $81^{\circ} 45'W$ , to  $21^{\circ} 15'N$ ,  $157^{\circ} 40'W$ .

- a)  $128^{\circ} T$
- b)  $217^{\circ} T$
- c)  **$290^{\circ} T$  - correct**
- d)  $326^{\circ} T$

GRC B3. Determine the great circle distance and initial course from latitude  $24^{\circ} 52.0' N$ , longitude  $78^{\circ} 27.0' W$  to latitude  $47^{\circ} 19.0' N$ , longitude  $6^{\circ} 42.0' W$ .

- e) **3593 miles,  $048.1^{\circ} T$  - correct**
- f) 3457 miles,  $053.3^{\circ} T$
- g) 3389 miles,  $042.4^{\circ} T$
- h) 3367 miles,  $045.0^{\circ} T$

GRC B4. Determine the great circle distance and initial course from latitude  $26^{\circ} 00' S$ , longitude  $56^{\circ} 00' W$  to latitude  $34^{\circ} 00' S$ , longitude  $18^{\circ} 15.0' E$ .

- a) 3705 miles,  $153^{\circ} T$
- b) 3841 miles,  $068^{\circ} T$
- c) 3849 miles,  $248^{\circ} T$
- d) **3805 miles,  $117^{\circ} T$  - correct**

GRC B5. Determine the great circle distance and initial course from latitude  $38^{\circ} 42' N$ , longitude  $09^{\circ} 10.5' W$  to latitude  $32^{\circ} 05' N$ , longitude  $81^{\circ} 05' W$ .

- a) 3402.0 miles,  $072.5^{\circ} T$
- b) 3412.6 miles,  $085.8^{\circ} T$
- c) 3432.0 miles,  $278.3^{\circ} T$
- d) **3449.4 miles,  $287.2^{\circ} T$  - correct**

### Great Circle Latitude or Longitude of the Vertex

GRC B6. The great circle distance from latitude  $08^{\circ} 50' \text{ N}$ ,  $80^{\circ} 21' \text{ W}$ , to a position  $12^{\circ} 36' \text{ N}$ ,  $128^{\circ} 16' \text{ E}$  is 8664 miles and the initial course is  $306.6^{\circ} \text{ T}$ . Determine the latitude of the vertex.

- a)  $38^{\circ} 46.2' \text{ N}$
- b)  $38^{\circ} 16.4' \text{ N}$
- c)  **$37^{\circ} 30.2' \text{ N}$  - correct**
- d)  $37^{\circ} 05.3' \text{ N}$

GRC B7. The great circle distance from latitude  $35^{\circ} 08' \text{ S}$ , longitude  $19^{\circ} 26' \text{ E}$  to latitude  $33^{\circ} 16' \text{ S}$ , longitude  $115^{\circ} 36' \text{ E}$  is 4559 miles and the initial course is  $121^{\circ} \text{ T}$ . Determine the latitude of the vertex.

- a)  $44^{\circ} 29.1' \text{ S}$
- b)  **$45^{\circ} 30.9' \text{ S}$  - correct**
- c)  $46^{\circ} 18.2' \text{ S}$
- d)  $43^{\circ} 41.8' \text{ S}$

GRC B8. The great circle distance from latitude  $38^{\circ} 17' \text{ N}$ , longitude  $123^{\circ} 16' \text{ W}$  to latitude  $35^{\circ} 01' \text{ N}$ , longitude  $142^{\circ} 21' \text{ W}$  is 4330 miles and the initial course is  $300.9^{\circ} \text{ T}$ . Determine the latitude of the vertex.

- a)  $46^{\circ} 54.8' \text{ N}$
- b)  $47^{\circ} 24.7' \text{ N}$
- c)  $47^{\circ} 35.2' \text{ N}$
- d)  **$47^{\circ} 40.5' \text{ N}$  - correct**

GRC B9. The great circle distance from latitude  $8^{\circ} 50.0' \text{ N}$ , longitude  $80^{\circ} 21.0' \text{ W}$  to latitude  $22^{\circ} 36.0' \text{ N}$ , longitude  $128^{\circ} 16.0' \text{ E}$  is 7801 miles and the initial course is  $318^{\circ} 45' \text{ T}$ . The latitude of the vertex is  $49^{\circ} 20.6' \text{ N}$ . What is the longitude of the vertex?

- a)  $156^{\circ} 43' \text{ W}$
- b)  **$162^{\circ} 41' \text{ W}$  - correct**
- c)  $159^{\circ} 32' \text{ W}$
- d)  $161^{\circ} 18' \text{ W}$

GRC B10. The great circle distance from latitude  $35^{\circ} 08' \text{ S}$ , longitude  $19^{\circ} 26' \text{ E}$  to latitude  $33^{\circ} 16' \text{ S}$ , longitude  $115^{\circ} 36' \text{ E}$  is 4559 miles and the initial course is  $121^{\circ} \text{ T}$ . Determine the longitude of the vertex.

- a)  $26^{\circ} 50.9' \text{ E}$
- b)  **$65^{\circ} 45.9' \text{ E}$  - correct**
- c)  $69^{\circ} 19.1' \text{ E}$
- d)  $72^{\circ} 18.3' \text{ E}$

GRC B11. The great circle distance from latitude  $38^{\circ} 17.0' \text{ N}$ , longitude  $123^{\circ} 16.0' \text{ W}$  to latitude  $35^{\circ} 01.0' \text{ N}$ , longitude  $142^{\circ} 21.0' \text{ E}$  is 4330 miles and the initial course is  $300.9^{\circ} \text{ T}$ . The latitude of the vertex is  $47^{\circ} 40.5' \text{ N}$ . What is the longitude of the vertex?

- a)  $173^{\circ} 04.6' \text{ E}$
- b)  $167^{\circ} 18.0' \text{ E}$
- c)  $173^{\circ} 04.6' \text{ W}$
- d)  **$167^{\circ} 18.5' \text{ W}$  - correct**

### Points Along the Great Circle Route

GRC B12. You are on a great circle track departing latitude  $25^{\circ} 50' \text{ N}$ , longitude  $77^{\circ} 00' \text{ W}$ , and your initial course is  $061.7^{\circ} \text{ T}$ . The position of the vertex is latitude  $37^{\circ} 35.6' \text{ N}$ , longitude  $25^{\circ} 57.8' \text{ W}$ . What is the distance along the great circle track between the point of departure and the vertex?

- a) 2735.1 miles
- b) 2664.9 miles- correct**
- c) 2583.2 miles
- d) 2420.0 miles

GRC B13. You are on a great circle track departing from position latitude  $25^{\circ} 50' \text{ N}$ , longitude  $77^{\circ} 00' \text{ W}$ . The position of the vertex is latitude  $37^{\circ} 35.6' \text{ N}$ , longitude  $25^{\circ} 57.8' \text{ W}$ . The distance along the great circle track from the vertex to a point (x) is 600 miles westward. Determine the position of point (x) on the great circle track.

- a)  $36^{\circ} 47.5' \text{ N}$ ,  $38^{\circ} 21.8' \text{ W}$
- b)  $36^{\circ} 50.4' \text{ N}$ ,  $38^{\circ} 25.6' \text{ W}$
- c)  $36^{\circ} 55.6' \text{ N}$ ,  $38^{\circ} 30.0' \text{ W}$ - correct**
- d)  $37^{\circ} 02.3' \text{ N}$ ,  $38^{\circ} 34.4' \text{ W}$

GRC B14. The great circle distance from latitude  $25^{\circ} 50' \text{ N}$ , longitude  $77^{\circ} 00' \text{ W}$  to latitude  $35^{\circ} 56' \text{ N}$ , longitude  $06^{\circ} 15' \text{ W}$  is 3616nm and the initial course is  $061.7^{\circ} \text{ T}$ . The position of the vertex is latitude  $37^{\circ} 34.9' \text{ N}$ , longitude  $25^{\circ} 59.0' \text{ W}$ . The difference of longitude from the vertex to a point (X) on the great circle route is  $10^{\circ} \text{ W}$ . Determine the latitude which intersects the great circle at point X.

- a)  $37^{\circ} 02.5' \text{ N}$
- b)  $37^{\circ} 09.5' \text{ N}$  - correct**
- c)  $37^{\circ} 15.6' \text{ N}$
- d)  $37^{\circ} 21.2' \text{ N}$





## **Zone Time (Rise/Set/Twilight/LAN) Problems**



## Zone Time of Rise/Set/Twilight/Meridian Passage Problems

- Time problems can either be dedicated problems asking for the time of rise/set/transit or could be a part of larger problems.
- Although the Coast Guard requirements indicated required competence at zone time of twilight problems, there are none currently in the problem database. Only rise/set/transit are found currently.
- Using the Nautical Almanac, values for time of phenomena are given for standard latitudes (various frequencies) and longitudes (every 15°). The most efficient process is to correct times for latitude first, using the nautical almanac, and then to correct for the difference in longitude from the standard meridian being observed.

### Basic Time of Rise/Set Concept Problems

TOP D1. Your ship's position is latitude 25° 00.0' N and longitude 65° 00.0' W. The ship is holding position and is not moving. The date is 4 August and you are observing (+4) zone time. What is the zone time of sunrise at your ship's location?

Answer: 0548.

Step 1: Locate the tabular values in the Nautical Almanac.

Find the latitudes which bracket the desired latitude and note the time of sunrise at those latitudes:

30° N: 0520

20° N: 0536

Note that the interval between the bracketing latitudes is 10°.

Step 2: Identify the latitude difference between the bracketing latitudes and the desired latitude, and the time difference between the tabular latitudes.

30° N: 0520

25° N: this is the unknown value you seek.

20° N: 0536

Differences:

Latitude difference: 20° N to 25° = 5°

Time difference: 20° N to 30° N = 0536 – 0520 = 16 minutes.

| Lat. | Twilight |       | Sunrise |
|------|----------|-------|---------|
|      | Naut.    | Civil |         |
|      | h m      | h m   | h m     |
| N 72 | [ ]      | [ ]   | [ ]     |
| N 70 | ////     | ////  | 01 42   |
| 68   | ////     | ////  | 02 24   |
| 66   | ////     | 00 51 | 02 52   |
| 64   | ////     | 01 50 | 03 14   |
| 62   | ////     | 02 22 | 03 31   |
| 60   | 00 46    | 02 46 | 03 45   |
| N 58 | 01 39    | 03 04 | 03 57   |
| 56   | 02 09    | 03 19 | 04 07   |
| 54   | 02 31    | 03 32 | 04 16   |
| 52   | 02 49    | 03 44 | 04 24   |
| 50   | 03 03    | 03 53 | 04 32   |
| 45   | 03 32    | 04 14 | 04 47   |
| N 40 | 03 53    | 04 30 | 05 00   |
| 35   | 04 09    | 04 43 | 05 11   |
| 30   | 04 23    | 04 54 | 05 20   |
| 20   | 04 45    | 05 13 | 05 36   |
| N 10 | 05 02    | 05 28 | 05 50   |
| 0    | 05 16    | 05 41 | 06 03   |

## Zone Time of Rise/Set/Twilight/Meridian Passage Problems

Step 3: Complete the latitude correction. The two options for this step are to use table 1 in the back of the Nautical Almanac, or for values that are relatively small and at relatively low latitudes, an arithmetic or mental interpolation is sufficient.

- Option 1: “Table 1” correction:

| Tabular Interval |      |      | Difference between the times for consecutive latitudes |                 |                 |                 |                 |                 |                 |                 |                 |                 |                 |                 |                                |                                |  |
|------------------|------|------|--------------------------------------------------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|--------------------------------|--------------------------------|--|
| 10°              | 5°   | 2°   | 5 <sup>m</sup>                                         | 10 <sup>m</sup> | 15 <sup>m</sup> | 20 <sup>m</sup> | 25 <sup>m</sup> | 30 <sup>m</sup> | 35 <sup>m</sup> | 40 <sup>m</sup> | 45 <sup>m</sup> | 50 <sup>m</sup> | 55 <sup>m</sup> | 60 <sup>m</sup> | 1 <sup>h</sup> 05 <sup>m</sup> | 1 <sup>h</sup> 10 <sup>m</sup> |  |
| 0 30             | 0 15 | 0 06 | 0                                                      | 0               | 1               | 1               | 1               | 1               | 1               | 2               | 2               | 2               | 2               | 2               | 0 02                           | 0 02                           |  |
| 1 00             | 0 30 | 0 12 | 0                                                      | 1               | 1               | 2               | 2               | 3               | 3               | 3               | 4               | 4               | 4               | 5               | 05                             | 05                             |  |
| 1 30             | 0 45 | 0 18 | 1                                                      | 1               | 2               | 3               | 3               | 4               | 4               | 5               | 5               | 6               | 7               | 7               | 07                             | 07                             |  |
| 2 00             | 1 00 | 0 24 | 1                                                      | 2               | 3               | 4               | 5               | 5               | 6               | 7               | 7               | 8               | 9               | 10              | 10                             | 10                             |  |
| 2 30             | 1 15 | 0 30 | 1                                                      | 2               | 4               | 5               | 6               | 7               | 8               | 9               | 9               | 10              | 11              | 12              | 12                             | 13                             |  |
| 3 00             | 1 30 | 0 36 | 1                                                      | 3               | 4               | 6               | 7               | 8               | 9               | 10              | 11              | 12              | 13              | 14              | 0 15                           | 0 15                           |  |
| 3 30             | 1 45 | 0 42 | 2                                                      | 3               | 5               | 7               | 8               | 10              | 11              | 12              | 13              | 14              | 16              | 17              | 18                             | 18                             |  |
| 4 00             | 2 00 | 0 48 | 2                                                      | 4               | 6               | 8               | 9               | 11              | 13              | 14              | 15              | 16              | 18              | 19              | 20                             | 21                             |  |
| 4 30             | 2 15 | 0 54 | 2                                                      | 4               | 7               | 9               | 11              | 13              | 15              | 16              | 18              | 19              | 21              | 22              | 23                             | 24                             |  |
| 5 00             | 2 30 | 1 00 | 2                                                      | 5               | 7               | 10              | 12              | 14              | 16              | 18              | 20              | 22              | 23              | 25              | 26                             | 27                             |  |

- Note that the tabular interval is 10°.
- Proceed down the “Tabular Interval” column until you reach the difference between the tabular latitude and your desired latitude (5° in this case).
- The time difference determined in the previous step was 16 minutes. There is no “16 minutes” column in the “difference between the times for consecutive latitudes” section, so note the values for the nearest headings (15m and 20m). In this case, the necessary values are 7 and 10 minutes.
- Mentally interpolate the actual value (8 minutes in this case).

Table 1 corrected time = 0536 – 8 minutes = 0528.

- Option 2: manual calculation:

$$\frac{x}{16 \text{ minutes}} = \frac{5^\circ}{10^\circ}$$

$$\frac{x}{16 \text{ minutes}} = 0.500$$

$$x = (0.5000) (16)$$

$$x = 8 \text{ minutes (earlier than base latitude)}$$

$$\text{Calculated corrected time} = 0536 - 8 \text{ minutes} = \underline{0528}$$

## Zone Time of Rise/Set/Twilight/Meridian Passage Problems

Step 4: Determine the difference in longitude from the standard meridian of the time being observed.

Longitude = 065° W.

If you are observing (+4) zone time, the associated standard meridian is 60° W.

65° W – 60° W = 5° difference (to the west) from standard meridian.

Step 5: Convert the difference in longitude arc to time using the Conversion of Arc to Time table in the Nautical Almanac.

5° of arc to the west = 20 minutes (added, since difference is “to the west”).

| CONVERSION OF ARC TO TIME |    |          |    |           |    |           |    |           |    |           |    |       |    |       |    |
|---------------------------|----|----------|----|-----------|----|-----------|----|-----------|----|-----------|----|-------|----|-------|----|
| 0°–59°                    |    | 60°–119° |    | 120°–179° |    | 180°–239° |    | 240°–299° |    | 300°–359° |    | 0°–00 |    | 0°–25 |    |
| °                         | m  | °        | m  | °         | m  | °         | m  | °         | m  | °         | m  | °     | m  | °     | m  |
| 0                         | 00 | 60       | 00 | 120       | 00 | 180       | 00 | 240       | 00 | 300       | 00 | 0     | 00 | 0     | 00 |
| 1                         | 04 | 61       | 04 | 121       | 04 | 181       | 04 | 241       | 04 | 301       | 04 | 1     | 04 | 0     | 05 |
| 2                         | 08 | 62       | 08 | 122       | 08 | 182       | 08 | 242       | 08 | 302       | 08 | 2     | 08 | 0     | 09 |
| 3                         | 12 | 63       | 12 | 123       | 12 | 183       | 12 | 243       | 12 | 303       | 12 | 3     | 12 | 0     | 13 |
| 4                         | 16 | 64       | 16 | 124       | 16 | 184       | 16 | 244       | 16 | 304       | 16 | 4     | 16 | 0     | 17 |
| 5                         | 20 | 65       | 20 | 125       | 20 | 185       | 20 | 245       | 20 | 305       | 20 | 5     | 20 | 0     | 21 |

Step 6: Apply the longitude correction to the latitude-corrected time to determine time of sunset.

0528 + 0020 = **0548**

## Zone Time of Rise/Set/Twilight/Meridian Passage Problems

### Basic Time of Meridian Transit (Local Apparent Noon) Concept Problems

TOP D2. Your ship's position is latitude  $25^{\circ} 31.5' \text{ N}$  and longitude  $128^{\circ} 06.4' \text{ W}$ . The ship is holding position and not moving. The date is 15 July and you are observing (+9) zone time. What is the zone time of local apparent noon at your ship's location?

Answer: 11:38 zone time.

| Day | SUN             |                 |       |
|-----|-----------------|-----------------|-------|
|     | Eqn. of Time    |                 | Mer.  |
|     | 00 <sup>h</sup> | 12 <sup>h</sup> | Pass. |
| 15  | m s             | m s             | h m   |
| 16  | 05 49           | 05 52           | 12 06 |
| 17  | 05 55           | 05 58           | 12 06 |
| 18  | 06 01           | 06 03           | 12 06 |

Step 1: Locate the tabular values in the Nautical Almanac.  
The time of meridian passage for 15 July is 1206.

Step 2: No latitude correction is required due to the nature of local apparent noon calculations.

Step 3: Determine the difference in longitude from the standard meridian of the time being observed.

Longitude =  $128^{\circ} 06.4' \text{ W}$

The vessel is observing (+9) = standard meridian of  $135^{\circ}$ .

$135^{\circ} \text{ W} - 128^{\circ} 06.4' \text{ W} = 6^{\circ} 53.6'$  difference from standard meridian.

Step 4: Convert the difference in longitude arc to time using the Conversion of Arc to Time in the Nautical Almanac.

$6^{\circ} 53.6'$  of arc to the east = 27 minutes 34 seconds (subtracted).

Step 5: Apply the longitude correction to the latitude-corrected time to determine time of local apparent noon.

$12:06:00 - 00:27:34 = 11:38$

| CONVERSION OF ARC TO TIME |    |          |    |           |    |           |    |           |    |           |    |       |    |       |    |
|---------------------------|----|----------|----|-----------|----|-----------|----|-----------|----|-----------|----|-------|----|-------|----|
| 0°-59°                    |    | 60°-119° |    | 120°-179° |    | 180°-239° |    | 240°-299° |    | 300°-359° |    | 0°-00 |    | 0°-25 |    |
| °                         | '  | °        | '  | °         | '  | °         | '  | °         | '  | °         | '  | °     | '  | °     | '  |
| 0                         | 00 | 60       | 00 | 120       | 00 | 180       | 00 | 240       | 00 | 300       | 00 | 0     | 00 | 0     | 00 |
| 1                         | 04 | 61       | 04 | 121       | 04 | 181       | 04 | 241       | 04 | 301       | 04 | 1     | 04 | 1     | 04 |
| 2                         | 08 | 62       | 08 | 122       | 08 | 182       | 08 | 242       | 08 | 302       | 08 | 2     | 08 | 2     | 08 |
| 3                         | 12 | 63       | 12 | 123       | 12 | 183       | 12 | 243       | 12 | 303       | 12 | 3     | 12 | 3     | 12 |
| 4                         | 16 | 64       | 16 | 124       | 16 | 184       | 16 | 244       | 16 | 304       | 16 | 4     | 16 | 4     | 16 |
| 5                         | 20 | 65       | 20 | 125       | 20 | 185       | 20 | 245       | 20 | 305       | 20 | 5     | 20 | 5     | 20 |
| 6                         | 24 | 66       | 24 | 126       | 24 | 186       | 24 | 246       | 24 | 306       | 24 | 6     | 24 | 6     | 24 |
| 7                         | 28 | 67       | 28 | 127       | 28 | 187       | 28 | 247       | 28 | 307       | 28 | 7     | 28 | 7     | 28 |
| 8                         | 32 | 68       | 32 | 128       | 32 | 188       | 32 | 248       | 32 | 308       | 32 | 8     | 32 | 8     | 32 |
| 9                         | 36 | 69       | 36 | 129       | 36 | 189       | 36 | 249       | 36 | 309       | 36 | 9     | 36 | 9     | 36 |
| 52                        | 28 | 112      | 28 | 172       | 28 | 232       | 28 | 292       | 28 | 352       | 28 | 52    | 28 | 3     | 28 |
| 53                        | 32 | 113      | 32 | 173       | 32 | 233       | 32 | 293       | 32 | 353       | 32 | 53    | 32 | 3     | 32 |
| 54                        | 36 | 114      | 36 | 174       | 36 | 234       | 36 | 294       | 36 | 354       | 36 | 54    | 36 | 3     | 36 |

## Zone Time of Rise/Set/Twilight/Meridian Passage Problems

### Advanced Time of Rise/Set/Passage Problems

TOP D3. On 28 June, your 1820 ZT DR position is latitude  $16^{\circ} 00.0'$  N, longitude  $31^{\circ} 00.0'$  W. You are on course  $310^{\circ}$  at a speed of 18 knots. What will be the zone time of sunset at your vessel?

Answer: 18:39 zone time. The calculation involves two phases. First determine the approximate time of sunset for your current position and determine how far you will travel between the current time and the calculated time. Some schools recommend assuming 0600 ZT for sunrise, 1800 for sunset, and 1200 for meridian passage. Second, complete a sunset calculation for the new DR location.

- Step 1: Locate the tabular values in the Nautical Almanac.  
The nearest bracketing latitudes and their associated sunset times are:

$10^{\circ}$  N = 1824  
 $16^{\circ}$  N = unknown value  
 $20^{\circ}$  N = 1843

|      |       |
|------|-------|
| N 40 | 19 33 |
| 35   | 19 18 |
| 30   | 19 05 |
| 20   | 18 43 |
| N 10 | 18 24 |
| 0    | 18 07 |

- Step 2: Determine the approximate time of sunset for your current DR position using either manual calculation or Table 1 in the Nautical Almanac.

Differences:

$10^{\circ}$  N to  $20^{\circ}$  N =  $10^{\circ}$

$10^{\circ}$  N to  $16^{\circ}$  N =  $6^{\circ}$

$10^{\circ}$  N time to  $20^{\circ}$  N time =  $1843 - 1824 = 19$  minutes

Using direct calculation is reasonable for this interpolation because the latitude is small, and the intervals are short. Table 1 is always available as an option.

$$\frac{x}{19 \text{ minutes}} = \frac{6^{\circ}}{10^{\circ}} = 0.6$$

$$x = (19)(0.6) = 11.4 \text{ minutes (later)}$$

$$\text{Latitude corrected time (calculation method)} = 1824 \text{ (base)} + 11.4 = 1835.4$$

Longitude 1 =  $31^{\circ}$  W.

Observed standard meridian (assumed from problem text) =  $30^{\circ}$  W.

Difference between actual and standard meridian =  $31^{\circ} - 30^{\circ} = 1^{\circ}$  (to the west).

Conversion of  $1^{\circ}$  arc to time = 4 minutes (to the west, or later).

Latitude corrected time = 1835.4

Longitude correction = 4 minutes (later)

Sunset at original DR position ( $16^{\circ}$  N and  $31^{\circ}$  W) =  $1835.4 + 4 = \underline{1839.4}$

## Zone Time of Rise/Set/Twilight/Meridian Passage Problems

Step 3: Perform other preliminary calculations.

$$1820 \text{ DR to } 1839.4 = 19.4 \text{ minutes}$$

$$19.4 \text{ minutes} = 0.323 \text{ hours}$$

$$0.323 \text{ hours at } 18 \text{ knots} = 5.82 \text{ nautical miles covered}$$

Step 4: Determine the ship's DR position at 1839.4, based on steaming  $310^\circ$  T for 5.82 miles by mid-latitude sailing or using a universal plotting sheet.

$$l = D \cos C$$

$$l = (5.82) \cos 310^\circ$$

$$l = (5.82) (0.6428)$$

$$l = 3.741$$

$$\text{Latitude } 1 = 16^\circ 00.0' \text{ N}$$

$$l = 3.741' = 0.0624^\circ \text{ (to the north)}$$

$$\text{Latitude } 2 = 16^\circ \text{ N} + 0.0624^\circ \text{ (to the north)} = 16.0624^\circ \text{ N}$$

$$Lm = \frac{16^\circ + 16.0624^\circ}{2} = 16.0312^\circ$$

$$p = D \sin C$$

$$p = (5.82) \sin 310^\circ$$

$$p = (5.82) (-0.7660)$$

$$p = -4.4584$$

$$DLo = \frac{p}{\cos Lm}$$

$$DLo = \frac{-4.4584}{\cos(16.0312)}$$

$$DLo = \frac{-4.4584}{0.9611}$$

$$DLo = -4.639$$

$$\text{Longitude } 1 = 31^\circ \text{ W}$$

$$DLo = -4.639' = 0.0773^\circ \text{ (to the west)}$$

$$\text{Longitude } 2 = 31^\circ \text{ W} + 0.0773^\circ = 31.0773^\circ \text{ W}$$



## Zone Time of Rise/Set/Twilight/Meridian Passage Problems

Step 5: Determine the latitude corrected time of sunset at the new DR position.

1839.4 DR position:  
 $16.0624^{\circ} \text{ N} = 16^{\circ} 03.7' \text{ N}$   
 $31.0773^{\circ} \text{ W} = 31^{\circ} 04.6' \text{ W}$

|             |              |
|-------------|--------------|
| <b>N 40</b> | <b>19 33</b> |
| <b>35</b>   | <b>19 18</b> |
| <b>30</b>   | <b>19 05</b> |
| <b>20</b>   | <b>18 43</b> |
| <b>N 10</b> | <b>18 24</b> |
| <b>0</b>    | <b>18 07</b> |

Tabular values for nearest bracketing latitudes:

$10^{\circ} \text{ N} = 1824$   
 $16.0624^{\circ} \text{ N} = \text{unknown}$   
 $20^{\circ} \text{ N} = 1843$

Differences:

$10^{\circ} \text{ N} \text{ to } 20^{\circ} \text{ N} = 10^{\circ}$   
 $10^{\circ} \text{ N} \text{ to } 16.0624^{\circ} \text{ N} = 6.0624^{\circ}$   
 $10^{\circ} \text{ N time to } 20^{\circ} \text{ N time} = 1843 - 1824 = 19 \text{ minutes}$

$$\frac{x}{19 \text{ minutes}} = \frac{6.0624^{\circ}}{10^{\circ}}$$

$$\frac{x}{19 \text{ minutes}} = 0.6062$$

$$x = (19)(0.6062)$$

$$x = 11.5 \text{ minutes (later)}$$

$$\text{Latitude corrected time} = 1824 \text{ (base)} + 11.5 \text{ minutes} = \underline{1835.5}$$

Step 6: Determine the longitude corrected time of sunset at the new DR position using the Conversion of Arc to Time in the Nautical Almanac.

$31^{\circ} 04.6' \text{ W} - 30^{\circ} \text{ W} = 1^{\circ} 04.6'$  difference from standard meridian.  
 $1^{\circ} 04.6'$  of arc to the west = 4 minutes 18 seconds (added).

Step 7: Apply the longitude correction to the latitude-corrected time to determine time of local apparent noon.

$$18:35:30 - 00:04:18 = \mathbf{18:39:18}$$

**Note:** this is a long, tedious process for minimal gain in this particular problem, but is illustrative of the process recommended for all problems for maximum accuracy. See the next problem for an example in which the changed DR position is critical.

## Zone Time of Rise/Set/Twilight/Meridian Passage Problems

TOP D4. On 2 April, your 0900 zone time DR position is latitude  $28^{\circ} 04.0' \text{ S}$  and longitude  $94^{\circ} 14.0' \text{ E}$ . Your vessel is on course  $316^{\circ} \text{ T}$  at a speed of 18.5 knots. What is the zone time of local apparent noon (LAN)?

Answer: 11:50 zone time.

Step 1: Locate the tabular values in the Nautical Almanac.  
The time of meridian passage for 2 April is 1204.

| Day | SUN             |                 |       |  |
|-----|-----------------|-----------------|-------|--|
|     | Eqn. of Time    |                 | Mer.  |  |
|     | 00 <sup>h</sup> | 12 <sup>h</sup> | Pass. |  |
| 1   | m s             | m s             | h m   |  |
| 2   | 04 02           | 03 53           | 12 04 |  |
| 3   | 03 44           | 03 35           | 12 04 |  |
| 3   | 03 26           | 03 18           | 12 03 |  |

Step 2: Perform preliminary calculations.

0900 DR to 1204 = 3 hours, 4 minutes

3 hours, 4 minutes = 3.067 hours

3.067 hours at 18.5 knots = 56.740 nautical miles covered

Longitude  $094^{\circ} 14.0' \text{ E}$  = zone descriptor (-6) =  $90^{\circ} \text{ E}$  standard meridian being observed (no other information stated in problem, so assume this zone time).

Step 3: Determine the ship's DR position at 1204, based on steaming  $316^{\circ} \text{ T}$  for 56.740 miles by mid-latitude sailing or using a chart/plotting sheet.

$$l = D \cos C$$

$$l = (56.740) \cos 316^{\circ}$$

$$l = (56.740) (0.7193)$$

$$l = 40.813$$

$$\text{Latitude 1} = 28^{\circ} 04.0' \text{ S} = 28.067^{\circ} \text{ S}$$

$$l = 40.813' = 0.680^{\circ} \text{ (to the north)}$$

$$\text{Latitude 2} = 28.067^{\circ} \text{ S} - 0.680^{\circ} = 27.387^{\circ} = \underline{27^{\circ} 23.22' \text{ S}}$$

$$Lm = \frac{28.067^{\circ} + 27.387^{\circ}}{2} = 27.727^{\circ}$$

$$p = D \sin C$$

$$p = (56.740) \sin 316^{\circ}$$

$$p = (56.740) (-0.6947)$$

$$p = -39.417$$

$$DLo = \frac{p}{\cos Lm}$$

$$DLo = \frac{-39.417}{\cos(27.727^{\circ})}$$

$$DLo = \frac{-39.417}{0.8852}$$

$$DLo = -44.529'$$

$$\text{Longitude 1} = 94^{\circ} 14.0' \text{ E} = 94.233^{\circ} \text{ E}$$

$$DLo = -44.529' = 0.742^{\circ} \text{ (to the west)}$$

$$\text{Longitude 2} = 94.233^{\circ} \text{ E} - 0.742^{\circ} = 93.491^{\circ} = \underline{93^{\circ} 29.46' \text{ E}}$$

## Zone Time of Rise/Set/Twilight/Meridian Passage Problems

Step 4: Determine the time of LAN at the new DR position.

1204 DR position:

27° 23.22' S

93° 29.46' E

$93^{\circ} 29.46' \text{ E} - 90^{\circ} \text{ E} = 3^{\circ} 29.46'$  difference from standard meridian.

Step 5: Convert the difference in longitude arc to time using the Conversion of Arc to Time Table.

$3^{\circ} 29.46'$  of arc to the east = 13 minutes 58 seconds (subtracted).

Step 6: Apply the longitude correction to the latitude-corrected time to determine time of local apparent noon.

$12:04:00 - 00:13:58 = \mathbf{11:50:02}$

### Zone Time of Rise/Set/Transit Problems

#### Basic Time of Phenomena Calculations (For Practice Only, Not on USCG Exams)

TOP B1. It is 3 March and you are keeping zone time (+6). You are stationary in position latitude  $26^{\circ} 26.0' \text{N}$ , longitude  $94^{\circ} 06.0' \text{W}$ . What is the zone time of sunrise at your location?

- a) **0638 - correct**
- b) 0645
- c) 0649

TOP B2. It is 12 June and you are keeping zone time (+9). You are stationary in position latitude  $44^{\circ} 13.0' \text{N}$ , longitude  $138^{\circ} 14.0' \text{W}$ . What is the zone time of sunset at your position?

- a) 1950
- b) **1957 - correct**
- c) 2009

TOP B3. It is 22 February and you are keeping zone time (+9). You are stationary in position latitude  $16^{\circ} 45.0' \text{N}$ , longitude  $130^{\circ} 00.0' \text{W}$ . What is the zone time of local apparent noon at your position?

- a) **1154 - correct**
- b) 1214
- c) 1234

### Zone Time of Sunrise/Sunset Problems

TOP B4. At 0327 zone time on 29 May, your DR position is latitude  $25^{\circ} 00.0'$  N, longitude  $064^{\circ} 15.0'$  W. You are steering  $270^{\circ}$  T at a speed of 13.6 knots. What is the zone time of sunrise?

- a) 0521
- b) 0529 – correct**
- c) 0536
- d) 0548

TOP B5. At 0500 zone time on 21 August, your DR position is latitude  $47^{\circ} 00.0'$  N, longitude  $125^{\circ} 15.0'$  W. You are steering  $000^{\circ}$  T at a speed of 9.8 knots. What is the zone time of sunrise?

- a) 0525 – correct**
- b) 0529
- c) 0531
- d) 0535

TOP B6. On 13 February at 0325 zone time, your DR position is latitude  $23^{\circ} 20.0'$  N, longitude  $155^{\circ} 15.0'$  W. You are steering  $240^{\circ}$  T at a speed of 13.6 knots. What is the zone time of sunrise?

- a) 0652
- b) 0657 – correct**
- c) 0706
- d) 0711

TOP B7. On 17 May, your 0300 zone time DR position is latitude  $27^{\circ} 21.0'$  N, longitude  $146^{\circ} 14.0'$  E. You are on course  $107^{\circ}$  T at a speed of 18 knots. What will be the zone time of sunrise at your vessel?

- a) 0457
- b) 0511
- c) 0519
- d) 0522 - correct**

TOP B8. On 27 September, your 0345 zone time DR position is latitude  $26^{\circ} 18.0'$  S, longitude  $004^{\circ} 18.0'$  W. You are on course  $271^{\circ}$  at a speed of 15 knots. What will be the zone time of sunrise at your vessel?

- a) 0525
- b) 0545
- c) 0555
- d) 0605 – correct**

TOP B9. On 16 February, your 0300 zone time DR position is latitude  $28^{\circ} 32.0'$  S, longitude  $176^{\circ} 49.0'$  E. You are on course  $082^{\circ}$  T at a speed of 21 knots. What will be the zone time of sunrise at your vessel?

- a) 0534
- b) 0552 - correct**
- c) 0631
- d) 0645

TOP B10. At 1544 zone time on 5 October, your DR position is latitude  $25^{\circ} 00.0'$  N, longitude  $60^{\circ} 15.0'$  W. You are steering  $270^{\circ}$  T at a speed of 6.8 knots. What is the zone time of sunset?

- a) 1728
- b) 1737
- c) 1741
- d) 1745 - correct**

TOP B11. At 1800 zone time on 7 December, your DR position is latitude  $22^{\circ} 48.0'$  S, longitude  $91^{\circ} 26.0'$  W. You are steering  $320^{\circ}$  T at a speed of 14 knots. What is the zone time of sunset?

- a) 1830
- b) 1836
- c) 1842 - correct**
- d) 1852

TOP B12. On 10 April, your 1630 zone time DR position is latitude  $21^{\circ} 03.0'$  N, longitude  $63^{\circ} 11.0'$  W. You are on course  $324^{\circ}$  T at a speed of 22 knots. What will be the zone time of sunset at your vessel?

- a) 1805
- b) 1814
- c) 1818
- d) 1833 - correct**

TOP B13. On 18 October, your 1330 zone time DR position is latitude  $27^{\circ} 32.0'$  N, longitude  $154^{\circ} 47.0'$  W. You are on course  $115^{\circ}$  T at a speed of 20 knots. What will be the zone time of sunset at your vessel?

- a) 1715
- b) 1729
- c) 1742 - correct**
- d) 1751

Zone Time of Meridian Transit (Local Apparent Noon)

TOP B14. On 12 February, your 0900 zone time DR position is latitude  $16^{\circ} 43.0'$  N, longitude  $51^{\circ} 42.0'$  W. Your vessel is on course  $093^{\circ}$  T at a speed of 18.5 knots. What is the zone time of local apparent noon?

- a) **1237 - correct**
- b) 1233
- c) 1230
- d) 1226

TOP B15. On 12 July your 0800 zone time DR position is latitude  $24^{\circ} 15.0'$  N, longitude  $132^{\circ} 30.0'$  W. Your vessel is on course  $045^{\circ}$  T at a speed of 15 knots. What is the zone time of local apparent noon?

- a) 1146
- b) 1148
- c) **1152 - correct**
- d) 1159

TOP B16. On 14 October your 0800 zone time DR position is latitude  $28^{\circ} 22.0'$  N, longitude  $161^{\circ} 17.0'$  E. Your vessel is on course  $116^{\circ}$  T at a speed of 17.5 knots. What is the zone time of local apparent noon?

- a) 1142
- b) 1148
- c) 1152
- d) **1156 - correct**

TOP B17. On 16 January, your 0930 zone time DR position is latitude  $26^{\circ} 07.0'$  S, longitude  $51^{\circ} 43.0'$  E. Your vessel is on course  $238^{\circ}$  T at a speed of 17 knots. What is the zone time of local apparent noon?

- a) **1145 - correct**
- b) 1148
- c) 1152
- d) 1156

TOP B18. On 3 October, your 0830 zone time DR position is latitude  $26^{\circ} 15.0'$  S, longitude  $73^{\circ} 16.0'$  E. Your vessel is on course  $280^{\circ}$  T at a speed of 19 knots. What is the zone time of local apparent noon?

- a) 1151
- b) 1154
- c) 1158
- d) **1201 - correct**





## **Gnomonic Chart Navigation Problems**



## Gnomonic Chart Navigation Problems

- These charts are used for planning ocean voyages and are oblique representations of the Earth's surface.
- Great Circles on a Gnomonic chart are straight lines, enabling easy voyage planning and later transfer of waypoints to a Mercator projection chart.
- Problems generally seek to test your plotting skills (use the latitude/longitude scales along the borders of the chart) or your ability to understand the benefits of Great Circles over Rhumb Lines.
- Generally, voyages that cross a large number of meridians (longitude lines) and latitude lines are best served with a Great Circle route. Voyages that transit north/south along a meridian or east/west near the equator are not significantly different than a Rhumb Line.

GNO D1. You are planning a voyage by great circle from latitude  $38^{\circ} 00' \text{ N}$ , longitude  $73^{\circ} 00' \text{ W}$  to latitude  $49^{\circ} 00' \text{ N}$ , longitude  $06^{\circ} 00' \text{ W}$ . Which of the following statements are true? Use Gnomonic tracking chart WOXZC 5274).

Answer: The shoals with a 25-mile radius around Sable Island will be a hazard.



Step 1: Plot the origin and arrival positions on the tracking chart and draw the trackline.

Step 2: Read each answer option carefully to eliminate all but the correct answer.

- a. You will pass to the south of icebergs reported extending to 100 miles south of Cape Race, Newfoundland. (Incorrect – You will pass through the iceberg area)
- b. **The shoals with a 25 mile radius around Sable Island will be a hazard.** (Correct – The track passes within the shoal area)
- c. You will reach the maximum northerly latitude at longitude  $29^{\circ} 45' \text{ W}$ . (Incorrect – The maximum northerly latitude will be significantly further north than the stated position.)
- d. The distance is measured in 60-mile segments using the length of a degree of latitude at the vertex. (Incorrect – Gnomonic charts are not used in this way.)

## Gnomonic Chart Navigation Problems

You are planning a voyage by great circle from Reykjavik (latitude  $63^{\circ} 30' \text{ N}$ , longitude  $24^{\circ} 00' \text{ W}$ ) to the Azores (latitude  $39^{\circ} 30' \text{ N}$ , longitude  $29^{\circ} 00' \text{ W}$ ). Which of the following statements are true? Use Gnomonic tracking chart WOXZC 5274).

Answer: The great circle track is not appreciably shorter than a rhumb line track.



Step 1: Plot the origin and arrival positions on the tracking chart and draw the trackline.

Step 2: Read each answer option carefully to eliminate all but the correct answer.

- a. The distance is measured in sixty-mile segments based on the length of a degree of latitude at the mid-latitude and mid-longitude positions. (Incorrect – Gnomonic charts are not used in this way.)
- b. The northern hemisphere vertex lies south of Reykjavik. (Incorrect – The course is virtually North/South, so the vertexes would be near the poles.)
- c. **The great circle track is not appreciably shorter than a rhumb line track.** (Correct – The course is virtually North/South, yielding no significant savings by great circle.)
- d. When plotted on a Mercator chart, the great circle track will be convex to the British Isles. (Incorrect – The course would be concave to the British Isles.)

## Gnomonic Chart Navigation Problems

### Atlantic Chart - 5274

GNO B1. A great circle track would be most advantageous when compared to the rhumb line track on which route? (Use gnomonic tracking chart WOXZC 5274).

- a) Cayenne ( $4^{\circ} 40' \text{ N}$ ,  $52^{\circ} 15' \text{ W}$ ) to Sao Tome ( $0^{\circ} 00'$ ,  $6^{\circ} 45' \text{ E}$ )
- b) Palm Beach, FL to the English Channel- correct**
- c) Natal, Brazil, to Reykjavik, Iceland
- d) Recife, Brazil, to Monrovia

GNO B2. On which voyage would a great circle track be significantly shorter than a rhumb line track? (Use gnomonic tracking chart WOXZC 5274).

- a) Savannah, GA to Lisbon, Portugal- correct**
- b) Dublin, Ireland (Irish Sea) to La Coruna, Spain (latitude  $43^{\circ} 22' \text{ N}$ , longitude  $8^{\circ} 24' \text{ W}$ )
- c) Reykjavik, Iceland to Lisbon, Portugal
- d) Boston to Sable Island

GNO B3. On a voyage via the southern tip of Nova Scotia (latitude  $43^{\circ} 20' \text{ N}$ , longitude  $65^{\circ} 35' \text{ W}$ ), you wish to sail the shortest route to La Coruna, Spain (latitude  $43^{\circ} 20' \text{ N}$ , longitude  $8^{\circ} 24' \text{ W}$ ). Which of the following will require you to plot a composite sailing? (Use gnomonic tracking chart WOXZC 5274).

- a) Shoals extending 15 miles from Sable Island
- b) Sea ice reported 68 miles ESE of St. John's, Newfoundland
- c) Icebergs reported extending west to west-northwest from latitude  $47^{\circ} \text{ N}$ , longitude  $35^{\circ} \text{ W}$ - correct**
- d) Naval exercises using live ammunition being conducted with a 150-mile radius of latitude  $49^{\circ} \text{ N}$ , longitude  $20^{\circ} \text{ W}$

GNO B4. You are planning a voyage by great circle from the mouth of the Delaware River (latitude  $38^{\circ} 40' \text{ N}$ , longitude  $75^{\circ} \text{ W}$ ) to Lisbon, Portugal. Which statement is true? (Use gnomonic tracking chart WOXZC 5274).

- a) You will reach the northernmost latitude of the voyage in the vicinity of longitude  $42^{\circ} 30' \text{ W}$ - correct**
- b) The Northern Hemisphere vertex lies to the east of Lisbon.
- c) You must plot a composite sailing to remain south of icebergs reported north of  $44^{\circ} \text{ N}$ .
- d) The distance is measured in 60-mile segments using the length of the degree of latitude crossed by the track line.

Pacific Chart - 5270

GNO B5. On which voyage would a great circle track provide a significant savings in distance to steam, when compared to a rhumb line track? (Use gnomonic tracking chart WOXZC 5270).

- a) Valdez, AK to the Marquesas Islands (latitude  $8^{\circ}$  S, longitude  $140^{\circ}$  W)
- b) San Francisco to Kodiak, AK
- c) Christmas Island (latitude  $2^{\circ}$  N, longitude  $157^{\circ} 30'$  W) to Singapore via latitude  $3^{\circ}$  N, longitude  $126^{\circ}$  E
- d) **Guam (latitude  $14^{\circ}$  N, longitude  $145^{\circ}$  E) to Seattle via latitude  $47^{\circ} 30'$  N, longitude  $125^{\circ} 20'$  W- correct**

GNO B6. Using gnomonic tracking chart WOXZC 5270, determine which of the following statements about a voyage from San Francisco to San Bernardino Strait (latitude  $13^{\circ}$  N, longitude  $125^{\circ} 30'$  E) is true.

- a) A composite sailing should be used to avoid the Bonin Islands.
- b) Distance is measured using the length of a degree of longitude at the point of tangency.
- c) **You will cross the Northern Hemisphere vertex at the approximate longitude of  $159^{\circ}$  W- correct**
- d) The entire track line is west of the Northern Hemisphere vertex.

GNO B7. Using gnomonic tracking chart WOXZC 5270, determine which of the following statements about a voyage from Valdez, AK to Hilo, HI is true.

- a) **A great circle track is not significantly shorter than a rhumb line track- correct**
- b) You will cross the Northern Hemisphere vertex where the track line crosses latitude  $45^{\circ}$  N.
- c) Distance is measured using the length of a degree of longitude at the mid-latitude line.
- d) When plotted on a Mercator chart, the track line will be convex to San Francisco.

GNO B8. You are on a voyage via position latitude  $44^{\circ}$  N, longitude  $150^{\circ}$  E to latitude  $46^{\circ} 15'$  N, longitude  $124^{\circ}$  W. Using gnomonic tracking chart WOXZC 5270, determine which statement is true.

- a) **A composite sailing with a limiting latitude of  $51^{\circ}$  N will clear the Aleutian Islands- correct**
- b) The northern hemisphere vertex is east of the arrival position.
- c) The Aleutian Islands are not a navigational hazard on the direct great circle track.
- d) The final course angle lies in the northeast quadrant.

## **Latitude by Polaris Problems**





## Latitude by Polaris Problems

- LHA (Local Hour Angle) of Aries is found using the Nautical Almanac to determine the GHA of Aries for the given time. Then, add (E Hem) or subtract (W Hem) the DR longitude to determine LHA of Aries.
- The formula for determining latitude by Polaris are located in the Nautical Almanac, on the same page as the Polaris corrections and therefore do not need to be memorized.

POL D1. On 14 March at 1845 ZT, you take a sextant observation of Polaris. Your DR position is latitude  $29^{\circ} 10' N$ , longitude  $154^{\circ} 30' W$ . Your sextant reads  $29^{\circ} 53.5'$ . Your chronometer reads 04h 42m 36s, and the chronometer error is 02m 24s slow. Your height of eye is 24 feet and the index error is 1.3' off the arc. Determine the latitude by Polaris.

Answer:  $29^{\circ} 21.3' N$

Step 1: Determine the correct chronometer time of sight.  
 Chronometer time of observation: 04h 42m 36s  
 Chronometer error: 02m 24s slow  
 Correct chronometer time of observation: 04h 42m 36s + 2m 24s = 04:45:00.

Step 2: Determine the correct GMT of the sight  
 DR Longitude:  $154^{\circ} 30' W$  - corresponds to ZD (+10).  
 Local time of observation: 1845 ZT  
 GMT time of observation = 1845 ZT + 10 hours = 0445 GMT (15 Mar).

Step 3: Determine the observed altitude of the body using the correction tables in the Nautical Almanac (reproduced at the end of this Part).  
 Sextant altitude (hs):  $29^{\circ} 53.5'$   
 Index error (1.3' off the arc): IC = + 1.3'  
 Height of eye (24 feet): dip = - 4.8'  
 Apparent altitude (ha) =  $29^{\circ} 53.5' + 1.3' - 4.8' = 29^{\circ} 50.0'$   
 Apparent altitude (stars/planets) correction: -1.7'  
 Observed altitude (ho) =  $29^{\circ} 50' - 1.7' = \underline{29^{\circ} 48.3'}$

|             |          |
|-------------|----------|
| <b>1500</b> | 172 30.6 |
| 01          | 187 33.0 |
| 02          | 202 35.5 |
| 03          | 217 38.0 |
| 04          | 232 40.4 |
| 05          | 247 42.9 |

Step 4: Determine the GHA of Aries for the time of sight.  
 GHA (Aries), whole hours:  $232^{\circ} 40.4'$   
 GHA (Aries), increment:  $11^{\circ} 16.8'$   
 GHA (Aries), total:  $232^{\circ} 40.4' + 11^{\circ} 16.8' = \underline{243^{\circ} 57.2'}$

| <sup>m</sup><br>45 | SUN<br>PLANETS | ARIES   | MOON    |
|--------------------|----------------|---------|---------|
| 00                 | 11 15.0        | 11 16.8 | 10 44.3 |
| 01                 | 11 15.3        | 11 17.1 | 10 44.5 |
| 02                 | 11 15.5        | 11 17.3 | 10 44.7 |
| 03                 | 11 15.8        | 11 17.6 | 10 45.0 |
| 04                 | 11 16.0        | 11 17.9 | 10 45.2 |

Step 5: Determine the LHA of Aries.  
 GHA (Aries):  $243^{\circ} 57.2'$   
 DR Longitude:  $154^{\circ} 30' W$   
 LHA (Aries) =  $243^{\circ} 57.2' - 154^{\circ} 30' W = \underline{89^{\circ} 27.2'}$

## Latitude by Polaris Problems

Step 6: Enter the Polaris Tables with LHA (Aries), DR Latitude, and Month to determine the A0, A1, and A2 correction factors (The complete Polaris Tables are located at the end of this Part).

A0 (LHA correction):  $0^{\circ} 31.7'$

A1 (Latitude correction):  $0.5'$

A2 (Month correction):  $0.8'$

Step 7: Calculate latitude using the Polaris Formula, provided at the bottom of the Polaris Tables.

Latitude = Observed altitude  $- 1^{\circ} + A0 + A1 + A2$

Lat =  $29^{\circ} 48.3' - 1^{\circ} + 31.7' + 0.5' + 0.8' = 29^{\circ} 21.3' \text{ N}$

| L.H.A.<br>ARIES | $80^{\circ}-$<br>$89^{\circ}$ |
|-----------------|-------------------------------|
|                 | $a_0$                         |
| 0               | 0 25.3                        |
| 1               | 25.9                          |
| 2               | 26.6                          |
| 3               | 27.2                          |
| 4               | 27.9                          |
| 5               | 0 28.6                        |
| 6               | 29.3                          |
| 7               | 29.9                          |
| 8               | 30.6                          |
| 9               | 31.4                          |
| 10              | 0 32.1                        |
| Lat.            | $a_1$                         |
| 0               | 0.3                           |
| 10              | .4                            |
| 20              | .4                            |
| 30              | .5                            |
| 40              | 0.5                           |
| 45              | .6                            |
| 50              | .6                            |
| 55              | .7                            |
| 60              | .7                            |
| 62              | 0.7                           |
| 64              | .8                            |
| 66              | .8                            |
| 68              | 0.9                           |
| Month           | $a_2$                         |
| Jan.            | 0.7                           |
| Feb.            | .8                            |
| Mar.            | .8                            |
| Apr.            | 0.8                           |
| May             | .7                            |
| June            | .5                            |
| July            | 0.4                           |
| Aug.            | .3                            |
| Sept.           | .3                            |
| Oct.            | 0.3                           |
| Nov.            | .4                            |
| Dec.            | 0.6                           |

$$\text{Latitude} = \text{Apparent altitude (corrected for refraction)} - 1^{\circ} + a_0 + a_1 + a_2$$

The table is entered with L.H.A. Aries to determine the column to be used; each column refers to a range of  $10^{\circ}$ .  $a_0$  is taken, with mental interpolation, from the upper table with the units of L.H.A. Aries in degrees as argument;  $a_1$ ,  $a_2$  are taken, without interpolation, from the second and third tables with arguments latitude and month respectively.  $a_0$ ,  $a_1$ ,  $a_2$  are always positive. The final table gives the azimuth of *Polaris*.

**ILLUSTRATION**  
On 1981 April 21 at G.M.T.  
23<sup>h</sup> 18<sup>m</sup> 56<sup>s</sup> in longitude  
W. 37° 14' the apparent altitude  
(corrected for refraction), *Ho*, of

From the daily pages:  
G.H.A. Aries (23<sup>h</sup>) 194 55.4  
Increment (18<sup>m</sup> 56<sup>s</sup>) 4 44.8  
Longitude (west) -37 14

*Ho* 49 31.6  
 $a_0$  (argument 162° 26') 1 30.1  
 $a_1$  (lat. 50° approx.) 0.6  
 $a_2$  (April) 0.9

### Latitude by Polaris Problems

POL B1. On 22 August your 1852 zone time DR position is longitude  $155^{\circ} 54'$  E. At that time, you observe Polaris with a sextant altitude (Hs) of  $27^{\circ} 36.9'$ . The chronometer time of observation is 08h 54m 06s and the chronometer error is 02m 20s fast. The index error is  $3.6'$  off the arc and the height of eye is 61.5 feet. What is your latitude by Polaris?

- a)  $27^{\circ} 05.5'$  N
- b)  $27^{\circ} 31.0'$  N
- c)  **$28^{\circ} 05.9'$  N - correct**
- d)  $28^{\circ} 09.5'$  N

POL B2. On 15 July at 0447 ZT, your vessel's DR position is latitude  $22^{\circ} 42'$  N, longitude  $126^{\circ} 36'$  E. At approximately that time, you obtain a sextant altitude (Hs) of Polaris reading  $23^{\circ} 46.2'$  with an index error of  $1.6'$  off the arc. Your chronometer reads 08h 48m 28s and is 1m 16s fast. What is your latitude by Polaris, given a height of eye of 33 feet?

- a)  $22^{\circ} 44.1'$  N
- b)  $22^{\circ} 46.2'$  N
- c)  $22^{\circ} 50.2'$  N
- d)  **$22^{\circ} 54.1'$  N - correct**

POL B3. On 7 March at 1838 ZT in DR position latitude  $34^{\circ} 26.9'$  N, longitude  $58^{\circ} 16.2'$  W, you observe Polaris for latitude. The sextant altitude (Hs) is  $35^{\circ} 08.4'$ . The index error is  $2.5'$  off the arc. The height of eye is 54 feet. What is the latitude at the time of sight?

- a)  $34^{\circ} 29.8'$  N
- b)  **$34^{\circ} 33.4'$  N - correct**
- c)  $34^{\circ} 34.8'$  N
- d)  $34^{\circ} 36.8'$  N

POL B4. On 10 June your 2010 zone time DR position is latitude  $41^{\circ} 10.0'$  N, longitude  $61^{\circ} 15.0'$  W. At that time, you observe Polaris with a sextant altitude (Hs) of  $40^{\circ} 35.8'$ . The chronometer time of observation is 00h 08m 18s, and the chronometer error is 01m 45s slow. The index error is  $2.0'$  on the arc, and the height of eye is 40 feet. What is your latitude by Polaris?

- a)  $41^{\circ} 10.6'$  N
- b)  **$41^{\circ} 15.0'$  N - correct**
- c)  $41^{\circ} 18.3'$  N
- d)  $41^{\circ} 21.2'$  N



## **Latitude by Meridian Passage Problems**



## Latitude by Meridian Passage Problems

- The key to basic meridian passage (local apparent noon) problems is identifying the relationship between the observer and the body.
  - If the observer is in the opposite hemisphere as the body, the formula is  $\text{Latitude} = \text{Zenith Distance} - \text{Declination}$ .
  - If the observer is in the same hemisphere but closer to the equator than the body, the formula is  $\text{Latitude} = \text{Declination} - \text{Zenith Distance}$ .
  - If the observer is in the same hemisphere as the body, but further away from the equator, the formula is  $\text{Latitude} = \text{Zenith Distance} + \text{Declination}$ .
- Zenith Distance is  $90 - \text{the Observed Altitude (Ho)}$ .
- Declination is obtained from the Nautical Almanac.
- Advancing/retarding lines of position is covered in more detail in the Running Fix section.
- Ex-meridian sights are those in which the observer was unable to make an observation at the appropriate time of phenomena. However, sights shortly before or shortly after the appropriate time of phenomena can be corrected yielding a line of latitude. In real practice, it is more accurate to simply do a full sight reduction rather than try to correct a flawed meridian passage sight.

## Latitude by Meridian Passage Problems

### Latitude at LAN Problems

MER D1. On 22 February your 0612 zone time fix gives you a position of latitude  $27^{\circ} 16.2' S$ , longitude  $37^{\circ} 41.6' W$ . Your vessel is on course  $298^{\circ} T$  at 14.2 knots. Local apparent noon (LAN) occurs at 1147 zone time, at which time a meridian altitude of the Sun's lower limb is observed. The observed altitude ( $H_o$ ) for this sight is  $73^{\circ} 33.3'$ . What is the calculated latitude at LAN?

Answer:  $26^{\circ} 31.4' S$ .

- Step 1: Determine the GMT of the sight.  
 DR longitude (0612):  $37^{\circ} 41.6' W$ , which corresponds to (+3 ZD).  
 1147 zone time +3 hours = 1447 GMT.
- Step 2: Determine the declination of the sun for the GMT time of sight.  
 At 1447 GMT:  
 Declination (hours):  $S 10^{\circ} 05.4'$  (decreasing)  
 d number: 0.9  
 Declination (increments):  $- 0.7'$   
 Declination (total):  $S 10^{\circ} 05.4' - 0.7' = \underline{S 10^{\circ} 04.7'}$
- Step 3: Determine the observed altitude of the body.  
 No corrections are required in this problem, since the (ho) is given as  $73^{\circ} 33.3'$
- Step 4: Determine the zenith distance of the sight.  
 $ZD = 90^{\circ} - \text{observed altitude.}$   
 $ZD = 90^{\circ} - 73^{\circ} 33.3' = \underline{16^{\circ} 26.7'}$
- Step 5: Determine the latitude.

|    |    |     |      |     |      |
|----|----|-----|------|-----|------|
| 22 | 00 | 176 | 36.1 | S10 | 18.2 |
| 01 |    | 191 | 36.2 |     | 17.3 |
| 02 |    | 206 | 36.2 |     | 16.4 |
| 03 |    | 221 | 36.3 | ..  | 15.5 |
| 04 |    | 236 | 36.4 |     | 14.6 |
| 05 |    | 251 | 36.5 |     | 13.6 |
| 06 |    | 266 | 36.6 | S10 | 12.7 |
| 07 |    | 281 | 36.6 |     | 11.8 |
| 08 |    | 296 | 36.7 |     | 10.9 |
| S  | 09 | 311 | 36.8 | ..  | 10.0 |
| U  | 10 | 326 | 36.9 |     | 09.1 |
| N  | 11 | 341 | 37.0 |     | 08.2 |
| D  | 12 | 356 | 37.1 | S10 | 07.3 |
| A  | 13 | 11  | 37.1 |     | 06.4 |
| Y  | 14 | 26  | 37.2 |     | 05.4 |
|    | 15 | 41  | 37.3 | ..  | 04.5 |
|    | 16 | 56  | 37.4 |     | 03.6 |
|    | 17 | 71  | 37.5 |     | 02.7 |
|    | 18 | 86  | 37.6 | S10 | 01.8 |
|    | 19 | 101 | 37.6 |     | 00.9 |
|    | 20 | 116 | 37.7 | 10  | 00.0 |
|    | 21 | 131 | 37.8 | 9   | 59.0 |
|    | 22 | 146 | 37.9 |     | 58.1 |
|    | 23 | 161 | 38.0 |     | 57.2 |

Since the observer is in the same hemisphere as the body, but further away from the equator (as evidenced by the DR latitude), the formula is:  
 Latitude = Zenith Distance + Declination  
 Latitude =  $16^{\circ} 26.7' + 10^{\circ} 04.7' = \underline{26^{\circ} 31.4' S}$

| D CORRECTIONS   |             |         |         |                                    |                                    |                                    |                                    |                                    |                                    | 47 <sup>m</sup> |
|-----------------|-------------|---------|---------|------------------------------------|------------------------------------|------------------------------------|------------------------------------|------------------------------------|------------------------------------|-----------------|
| 47 <sup>m</sup> | SUN PLANETS | ARIES   | MOON    | $\frac{v}{d}$ or Corr <sup>n</sup> | $\frac{v}{d}$ or Corr <sup>n</sup> | $\frac{v}{d}$ or Corr <sup>n</sup> | $\frac{v}{d}$ or Corr <sup>n</sup> | $\frac{v}{d}$ or Corr <sup>n</sup> | $\frac{v}{d}$ or Corr <sup>n</sup> |                 |
| 00              | 11 45.0     | 11 46.9 | 11 12.9 | 0-0                                | 0-0                                | 6-0                                | 4-8                                | 12-0                               | 9-5                                |                 |
| 01              | 11 45.3     | 11 47.2 | 11 13.1 | 0-1                                | 0-1                                | 6-1                                | 4-8                                | 12-1                               | 9-6                                |                 |
| 02              | 11 45.5     | 11 47.4 | 11 13.4 | 0-2                                | 0-2                                | 6-2                                | 4-9                                | 12-2                               | 9-7                                |                 |
| 03              | 11 45.8     | 11 47.7 | 11 13.6 | 0-3                                | 0-2                                | 6-3                                | 5-0                                | 12-3                               | 9-7                                |                 |
| 04              | 11 46.0     | 11 47.9 | 11 13.8 | 0-4                                | 0-3                                | 6-4                                | 5-1                                | 12-4                               | 9-8                                |                 |
| 05              | 11 46.3     | 11 48.2 | 11 14.1 | 0-5                                | 0-4                                | 6-5                                | 5-1                                | 12-5                               | 9-9                                |                 |
| 06              | 11 46.5     | 11 48.4 | 11 14.3 | 0-6                                | 0-5                                | 6-6                                | 5-2                                | 12-6                               | 10-0                               |                 |
| 07              | 11 46.8     | 11 48.7 | 11 14.6 | 0-7                                | 0-6                                | 6-7                                | 5-3                                | 12-7                               | 10-1                               |                 |
| 08              | 11 47.0     | 11 48.9 | 11 14.8 | 0-8                                | 0-6                                | 6-8                                | 5-4                                | 12-8                               | 10-1                               |                 |
| 09              | 11 47.3     | 11 49.2 | 11 15.0 | 0-9                                | 0-7                                | 6-9                                | 5-5                                | 12-9                               | 10-2                               |                 |



## Latitude by Meridian Passage Problems

MER D2. On 16 September your 0600 ZT fix gives you a position of latitude  $29^{\circ} 47.2' \text{ N}$ , longitude  $65^{\circ} 28.4' \text{ W}$ . Your vessel is on course  $242^{\circ} \text{ T}$  and your speed is 13.5 knots. Local apparent noon (LAN) occurs at 1227 ZT, at which time a meridian altitude of the Sun's lower limb is observed. The observed altitude ( $H_o$ ) for this sight is  $63^{\circ} 25.3'$ . What is the calculated latitude at LAN?

Answer:  $29^{\circ} 04.6' \text{ N}$ .

Step 1: Determine the GMT of the sight.  
DR longitude (0600):  $65^{\circ} 28.4' \text{ W}$ , which corresponds to (+4 ZD).

1227 zone time +4 hours = 1627 GMT.

Step 2: Determine the declination of the sun for the GMT time of sight.

At 1627 GMT:

Declination (hours):  $\text{N } 2^{\circ} 30.4'$  (decreasing)

d number: 1.0

Declination (increments):  $- 0.5'$

Declination (total):  $\text{N } 2^{\circ} 30.4' - 0.5' =$

$\text{S } 2^{\circ} 29.9'$

Step 3: Determine the observed altitude of the body.

No corrections are required in this problem, since the ( $H_o$ ) is given as  $63^{\circ} 25.3'$

Step 4: Determine the zenith distance of the sight.

$\text{ZD} = 90^{\circ} - \text{observed altitude.}$

$\text{ZD} = 90^{\circ} - 63^{\circ} 25.3' = \underline{26^{\circ} 34.7'}$

Step 5: Determine the latitude.

Since the observer is in the same hemisphere as the body, but further away from the equator (as evidenced by the DR latitude), the formula is:

Latitude = Zenith Distance + Declination

Latitude =  $26^{\circ} 34.7' + 2^{\circ} 29.9' = \underline{26^{\circ} 04.6' \text{ N}}$

| G.M.T. |    | SUN    |      |      |        |
|--------|----|--------|------|------|--------|
|        |    | G.H.A. |      | Dec. |        |
| d      | h  | °      | '    | °    | '      |
| 16     | 00 | 181    | 15.0 | N    | 2 45.9 |
|        | 01 | 196    | 15.2 |      | 44.9   |
|        | 02 | 211    | 15.4 |      | 43.9   |
|        | 03 | 226    | 15.7 |      | 43.0   |
|        | 04 | 241    | 15.9 |      | 42.0   |
|        | 05 | 256    | 16.1 |      | 41.0   |
|        | 06 | 271    | 16.3 | N    | 2 40.1 |
|        | 07 | 286    | 16.6 |      | 39.1   |
|        | 08 | 301    | 16.8 |      | 38.2   |
|        | 09 | 316    | 17.0 |      | 37.2   |
|        | 10 | 331    | 17.2 |      | 36.2   |
|        | 11 | 346    | 17.4 |      | 35.3   |
|        | 12 | 1      | 17.7 | N    | 2 34.3 |
|        | 13 | 16     | 17.9 |      | 33.3   |
|        | 14 | 31     | 18.1 |      | 32.4   |
|        | 15 | 46     | 18.3 |      | 31.4   |
|        | 16 | 61     | 18.6 |      | 30.4   |
|        | 17 | 76     | 18.8 |      | 29.5   |
|        | 18 | 91     | 19.0 | N    | 2 28.5 |
|        | 19 | 106    | 19.2 |      | 27.5   |
|        | 20 | 121    | 19.5 |      | 26.6   |
|        | 21 | 136    | 19.7 |      | 25.6   |
|        | 22 | 151    | 19.9 |      | 24.6   |
|        | 23 | 166    | 20.1 |      | 23.7   |

| D CORRECTIONS   |                |       |       |              |              |              | 27 <sup>m</sup> |
|-----------------|----------------|-------|-------|--------------|--------------|--------------|-----------------|
| 27 <sup>m</sup> | SUN<br>PLANETS | ARIES | MOON  | U<br>or<br>d | U<br>or<br>d | U<br>or<br>d |                 |
| 00              | 6 450          | 6 461 | 6 266 | 0-0 0-0      | 6-0 2-8      | 12-0 5-5     |                 |
| 01              | 6 453          | 6 464 | 6 268 | 0-1 0-0      | 6-1 2-8      | 12-1 5-5     |                 |
| 02              | 6 455          | 6 466 | 6 270 | 0-2 0-1      | 6-2 2-8      | 12-2 5-6     |                 |
| 03              | 6 458          | 6 469 | 6 273 | 0-3 0-1      | 6-3 2-9      | 12-3 5-6     |                 |
| 04              | 6 460          | 6 471 | 6 275 | 0-4 0-2      | 6-4 2-9      | 12-4 5-7     |                 |
| 05              | 6 463          | 6 474 | 6 277 | 0-5 0-2      | 6-5 3-0      | 12-5 5-7     |                 |
| 06              | 6 465          | 6 476 | 6 280 | 0-6 0-3      | 6-6 3-0      | 12-6 5-8     |                 |
| 07              | 6 468          | 6 479 | 6 282 | 0-7 0-3      | 6-7 3-1      | 12-7 5-8     |                 |
| 08              | 6 470          | 6 481 | 6 285 | 0-8 0-4      | 6-8 3-1      | 12-8 5-9     |                 |
| 09              | 6 473          | 6 484 | 6 287 | 0-9 0-4      | 6-9 3-2      | 12-9 5-9     |                 |
| 10              | 6 475          | 6 486 | 6 289 | 1-0 0-5      | 7-0 3-2      | 13-0 6-0     |                 |

## Latitude by Meridian Passage Problems

MER D3. On 7 November your 0830 zone time fix gives you a position of latitude  $27^{\circ} 36.0' \text{ N}$ , longitude  $163^{\circ} 19.0' \text{ W}$ . Your vessel is on course  $289^{\circ} \text{ T}$  and your speed is 19.0 knots. Local apparent noon (LAN) occurs at 1138 zone time, at which time a meridian altitude of the Sun's lower limb is observed. The observed altitude ( $H_o$ ) for this sight is  $45^{\circ} 35.0'$ . What is the calculated latitude at LAN?

Answer:  $27^{\circ} 57.2' \text{ N}$

Step 1: Determine the GMT of the sight.  
 DR longitude (0830):  $163^{\circ} 19.0' \text{ W}$ , which corresponds to (+11 ZD).  
 1138 zone time +11 hours = 2238 GMT.

Step 2: Determine the declination of the sun for the GMT time of sight.  
 At 2238 GMT:  
 Declination (hours):  $S 16^{\circ} 27.4'$  (increasing)  
 d number: 0.7  
 Declination (increments):  $+0.4'$   
 Declination (total):  $S 16^{\circ} 27.4' + 0.4' =$   
 $S 16^{\circ} 27.8'$

|      |     |      |     |      |
|------|-----|------|-----|------|
| 7 00 | 184 | 04.6 | S16 | 11.2 |
| 01   | 199 | 04.6 |     | 12.0 |
| 02   | 214 | 04.6 |     | 12.7 |
| 03   | 229 | 04.6 | ..  | 13.5 |
| 04   | 244 | 04.5 |     | 14.2 |
| 05   | 259 | 04.5 |     | 14.9 |
| 06   | 274 | 04.5 | S16 | 15.7 |
| 07   | 289 | 04.4 |     | 16.4 |
| S 08 | 304 | 04.4 |     | 17.1 |
| A 09 | 319 | 04.3 | ..  | 17.9 |
| T 10 | 334 | 04.3 |     | 18.6 |
| U 11 | 349 | 04.3 |     | 19.4 |
| R 12 | 4   | 04.2 | S16 | 20.1 |
| D 13 | 19  | 04.2 |     | 20.8 |
| A 14 | 34  | 04.2 |     | 21.6 |
| Y 15 | 49  | 04.1 | ..  | 22.3 |
| 16   | 64  | 04.1 |     | 23.0 |
| 17   | 79  | 04.1 |     | 23.8 |
| 18   | 94  | 04.0 | S16 | 24.5 |
| 19   | 109 | 04.0 |     | 25.2 |
| 20   | 124 | 03.9 |     | 26.0 |
| 21   | 139 | 03.9 | ..  | 26.7 |
| 22   | 154 | 03.9 |     | 27.4 |
| 23   | 169 | 03.8 |     | 28.2 |

Step 3: Determine the observed altitude of the body.  
 No corrections are required in this problem, since the ( $h_o$ ) is given as  $45^{\circ} 35.0'$

Step 4: Determine the zenith distance of the sight.  
 $ZD = 90^{\circ} - \text{observed altitude.}$   
 $ZD = 90^{\circ} - 45^{\circ} 35.0' =$   $44^{\circ} 25.0'$

Step 5: Determine the latitude.

Since the observer is in the opposite hemisphere as the body (as evidenced by the DR latitude), the formula is:

Latitude = Zenith Distance - Declination

Latitude =  $44^{\circ} 25.0' - 16^{\circ} 27.8' =$   **$27^{\circ} 57.2' \text{ N}$**

| 38 <sup>m</sup> |             | INCREMENTS AND |        |                                    |                                    |                                    |                                    |
|-----------------|-------------|----------------|--------|------------------------------------|------------------------------------|------------------------------------|------------------------------------|
| 38 <sup>m</sup> | SUN PLANETS | ARIES          | MOON   | $\frac{v}{d}$ or Corr <sup>n</sup> | $\frac{v}{d}$ or Corr <sup>n</sup> | $\frac{v}{d}$ or Corr <sup>n</sup> | $\frac{v}{d}$ or Corr <sup>n</sup> |
| 00              | 9 30.0      | 9 31.6         | 9 04.0 | 0.0 0.0                            | 6.0 3.9                            | 12.0 7.7                           |                                    |
| 01              | 9 30.3      | 9 31.8         | 9 04.3 | 0.1 0.1                            | 6.1 3.9                            | 12.1 7.8                           |                                    |
| 02              | 9 30.5      | 9 32.1         | 9 04.5 | 0.2 0.1                            | 6.2 4.0                            | 12.2 7.8                           |                                    |
| 03              | 9 30.8      | 9 32.3         | 9 04.7 | 0.3 0.2                            | 6.3 4.0                            | 12.3 7.9                           |                                    |
| 04              | 9 31.0      | 9 32.6         | 9 05.0 | 0.4 0.3                            | 6.4 4.1                            | 12.4 8.0                           |                                    |
| 05              | 9 31.3      | 9 32.8         | 9 05.2 | 0.5 0.3                            | 6.5 4.2                            | 12.5 8.0                           |                                    |
| 06              | 9 31.5      | 9 33.1         | 9 05.5 | 0.6 0.4                            | 6.6 4.2                            | 12.6 8.1                           |                                    |
| 07              | 9 31.8      | 9 33.3         | 9 05.7 | 0.7 0.4                            | 6.7 4.3                            | 12.7 8.1                           |                                    |
| 08              | 9 32.0      | 9 33.6         | 9 05.9 | 0.8 0.5                            | 6.8 4.4                            | 12.8 8.2                           |                                    |
| 09              | 9 32.3      | 9 33.8         | 9 06.2 | 0.9 0.6                            | 6.9 4.4                            | 12.9 8.3                           |                                    |

## Latitude by Meridian Passage Problems

### Latitude at 1200 (Advance/Retard LOP)

MER D4. On 13 October your 0515 zone time fix gives you a position of latitude  $26^{\circ} 53.0' N$ , longitude  $90^{\circ} 05.0' W$ . Your vessel is on course  $068^{\circ} T$  and your speed is 7.8 knots. Local apparent noon (LAN) occurs at 1145 zone time, at which time a meridian altitude of the Sun's lower limb is observed. The observed altitude ( $H_o$ ) for this sight is  $54^{\circ} 51.5'$ . What is the latitude at 1200 ZT?

Answer:  $27^{\circ} 13.3' N$ .

Step 1: Determine the GMT of the sight.  
 DR longitude (0515):  $90^{\circ} 05.0' W$ , which corresponds to (+6 ZD).  
 1145 zone time + 6 hours = 1745 GMT.

Step 2: Determine the declination of the sun for the GMT time of sight.  
 At 1745 GMT:  
 Declination (hours):  $S 7^{\circ} 55.2'$  (increasing)  
 d number: 0.9  
 Declination (increments):  $+0.7'$   
 Declination (total):  $S 7^{\circ} 55.2' + 0.7' =$   
 $S 7^{\circ} 55.9'$

|        |    | SUN    |      |      |      |
|--------|----|--------|------|------|------|
| G.M.T. |    | G.H.A. |      | Dec. |      |
| d      | h  | °      | '    | °    | '    |
| 13     | 00 | 183    | 24.5 | S 7  | 39.3 |
| 01     |    | 198    | 24.6 |      | 40.2 |
| 02     |    | 213    | 24.8 |      | 41.2 |
| 03     |    | 228    | 24.9 | ..   | 42.1 |
| 04     |    | 243    | 25.1 |      | 43.1 |
| 05     |    | 258    | 25.2 |      | 44.0 |
| 06     |    | 273    | 25.4 | S 7  | 44.9 |
| 07     |    | 288    | 25.5 |      | 45.9 |
| 08     |    | 303    | 25.7 |      | 46.8 |
| 09     |    | 318    | 25.8 | ..   | 47.7 |
| 10     |    | 333    | 26.0 |      | 48.7 |
| 11     |    | 348    | 26.1 |      | 49.6 |
| 12     |    | 3      | 26.3 | S 7  | 50.5 |
| 13     |    | 18     | 26.4 |      | 51.5 |
| 14     |    | 33     | 26.6 |      | 52.4 |
| 15     |    | 48     | 26.7 | ..   | 53.3 |
| 16     |    | 63     | 26.9 |      | 54.3 |
| 17     |    | 78     | 27.0 |      | 55.2 |

Step 3: Determine the observed altitude of the body.  
 No corrections are required in this problem, since the ( $h_o$ ) is given as  $54^{\circ} 51.5'$

Step 4: Determine the zenith distance of the sight.  
 $ZD = 90^{\circ} - \text{observed altitude.}$   
 $ZD = 90^{\circ} - 54^{\circ} 51.5' =$   $35^{\circ} 08.5'$

Step 5: Determine the latitude.

Since the observer is in the opposite hemisphere as the body (as evidenced by the DR latitude), the formula is:

Latitude = Zenith Distance - Declination

Latitude =  $35^{\circ} 08.5' - 7^{\circ} 55.9' = 27^{\circ} 12.6' N$

| CORRECTIONS     |         |         |         |                        |     |                        |     |                        |     | 45 <sup>m</sup> |
|-----------------|---------|---------|---------|------------------------|-----|------------------------|-----|------------------------|-----|-----------------|
| 45 <sup>m</sup> | SUN     | ARIES   | MOON    | v or Corr <sup>n</sup> |     | v or Corr <sup>n</sup> |     | v or Corr <sup>n</sup> |     |                 |
| s               | °       | '       | °       | '                      | "   | °                      | '   | °                      | '   | "               |
| 00              | 11 15.0 | 11 16.8 | 10 44.3 | 0.0                    | 0.0 | 6.0                    | 4.6 | 12.0                   | 9.1 |                 |
| 01              | 11 15.3 | 11 17.1 | 10 44.5 | 0.1                    | 0.1 | 6.1                    | 4.6 | 12.1                   | 9.2 |                 |
| 02              | 11 15.5 | 11 17.3 | 10 44.7 | 0.2                    | 0.2 | 6.2                    | 4.7 | 12.2                   | 9.3 |                 |
| 03              | 11 15.8 | 11 17.6 | 10 45.0 | 0.3                    | 0.2 | 6.3                    | 4.8 | 12.3                   | 9.3 |                 |
| 04              | 11 16.0 | 11 17.9 | 10 45.2 | 0.4                    | 0.3 | 6.4                    | 4.9 | 12.4                   | 9.4 |                 |
| 05              | 11 16.3 | 11 18.1 | 10 45.4 | 0.5                    | 0.4 | 6.5                    | 4.9 | 12.5                   | 9.5 |                 |
| 06              | 11 16.5 | 11 18.4 | 10 45.7 | 0.6                    | 0.5 | 6.6                    | 5.0 | 12.6                   | 9.6 |                 |
| 07              | 11 16.8 | 11 18.6 | 10 45.9 | 0.7                    | 0.5 | 6.7                    | 5.1 | 12.7                   | 9.6 |                 |
| 08              | 11 17.0 | 11 18.9 | 10 46.2 | 0.8                    | 0.6 | 6.8                    | 5.2 | 12.8                   | 9.7 |                 |
| 09              | 11 17.3 | 11 19.1 | 10 46.4 | 0.9                    | 0.7 | 6.9                    | 5.2 | 12.9                   | 9.8 |                 |

## Latitude by Meridian Passage Problems

Step 6: Advance or retard the latitude line of position to the desired time. Note this task can be accomplished by math (via mid-latitude sailing) or by plotting sheet. This example shows both methods.

a. Method 1: Mid Latitude Sailings.

i. Determine the transit time and distance (D) steamed over that time.

1145 (LAN) to 1200 (desired fix) = 15 minutes = 0.25 hours

7.8 knots for 0.25 hours = 1.95 miles. (Course = 068° T)

ii. Determine the Difference in Latitude ( $l$ ) using the plane sailing formula.

$$l = D \cos C$$

$$l = 1.95 \cos(68^\circ)$$

$$l = (1.95) (0.3746)$$

$$l = 0.73'$$

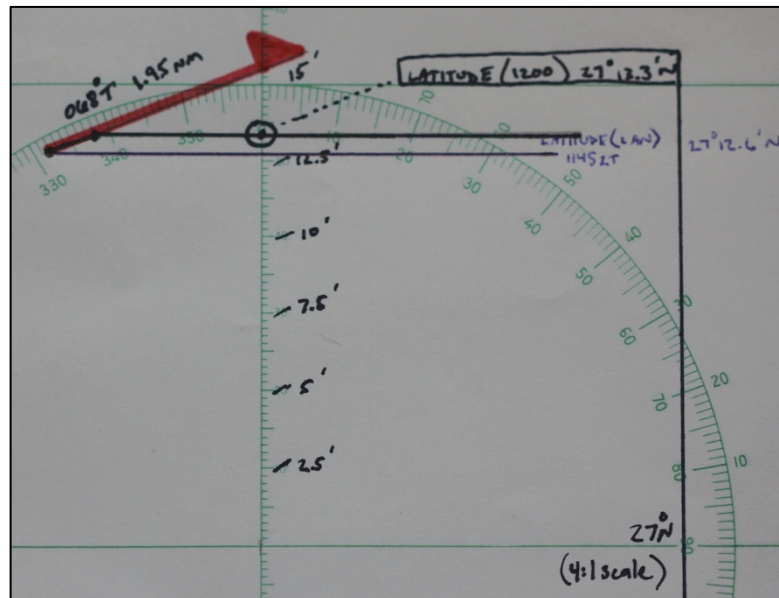
iii. Determine latitude 2 given the initial position and the Difference in Latitude ( $l$ ).

Lat1 (LAN) = 27° 12.6' N

$$l = + 0.73'$$

Lat2 (1200) = 27° 12.6' + 0.73' = **27° 13.3' N**

b. Method 2: Plotting Sheet.



## Latitude by Meridian Passage Problems

### Ex-Meridian Problems

MER D5. On 15 August an ex-meridian altitude of the Sun's lower limb at upper transit was observed at 1130 ZT. Your DR position is latitude  $26^{\circ} 24.0' S$ , longitude  $155^{\circ} 02.0' E$  and your sextant altitude (hs) is  $48^{\circ} 45.9'$ . The index error is  $2.6'$  on the arc and your height of eye is 51.5 feet. The chronometer time of the observation is 01h 27m 38s, and the chronometer error is 02m 14s slow. Find the latitude at meridian passage from the ex-meridian observation.

Answer:  $26^{\circ} 51.7' S$ .

Step 1: Determine the chronometer time of sight based on chronometer error.

Chronometer time: 01h 27m 38s

Chronometer error: 00h 02m 14s slow

Correct sight time: 01h 27m 38s + 00h 02m 14s =  
01h 29m 52s

| SUN             |          |      |      |
|-----------------|----------|------|------|
| G.M.T.          | G.H.A.   | Dec. |      |
| 15 00           | 178 52.3 | N14  | 09.1 |
| 01              | 193 52.4 |      | 08.3 |
| 02              | 208 52.6 |      | 07.5 |
| S.D. 15.8 d 0.8 |          |      |      |

Step 2: Determine the GMT of the sight.

DR longitude:  $155^{\circ} 02.0' E$  (corresponds to -10 ZT)

Clock time of sight: 1130 ZT

$1130 - 10 (ZT) = 0130$ . Therefore, the chronometer time of 01:29:52 (15 August) is correct and used for the sight.

Step 3: Determine the time difference from meridian passage to the time of observation.

Time of sight: 01:29:52 GMT

GHA (hours):  $193^{\circ} 52.4'$

GHA (increment):  $7^{\circ} 28.0'$

GHA (total):  $193^{\circ} 52.4' + 7^{\circ} 28.0' = 201^{\circ} 20.4'$

DR longitude:  $155^{\circ} 02.0' E$

LHA (sun):  $201^{\circ} 20.4' + 155^{\circ} 02.0' E = 356^{\circ} 22.4'$

LHA diff. from meridian passage (LHA =  $360^{\circ}$ ):  $360 - 356^{\circ} 22.4' = 3^{\circ} 37.6'$

LHA difference converted to time:  $3^{\circ} 37.6' = \underline{14m 30s}$

| INCREMENTS AND CORRECTIONS |                |        |        |                         |                   |                 |                |       |      |                         |                   |
|----------------------------|----------------|--------|--------|-------------------------|-------------------|-----------------|----------------|-------|------|-------------------------|-------------------|
| 28 <sup>m</sup>            |                |        |        |                         |                   | 29 <sup>m</sup> |                |       |      |                         |                   |
| <sup>s</sup>               | SUN<br>PLANETS | ARIES  | MOON   | <sup>u</sup><br>or<br>d | Corr <sup>n</sup> | <sup>s</sup>    | SUN<br>PLANETS | ARIES | MOON | <sup>u</sup><br>or<br>d | Corr <sup>n</sup> |
| 00                         | 7 00-0         | 7 01-1 | 6 40-9 | 0-0                     | 0-0               | 0-0             | 2-9            | 12-0  | 5-7  |                         |                   |
| 01                         | 7 00-3         | 7 01-4 | 6 41-1 | 0-1                     | 0-0               | 0-1             | 2-9            | 12-1  | 5-7  |                         |                   |
| 02                         | 7 00-5         | 7 01-7 | 6 41-3 | 0-2                     | 0-1               | 0-2             | 2-9            | 12-2  | 5-8  |                         |                   |
| 03                         | 7 00-8         | 7 01-9 | 6 41-6 | 0-3                     | 0-1               | 0-3             | 3-0            | 12-3  | 5-8  |                         |                   |
| 04                         | 7 01-0         | 7 02-2 | 6 41-8 | 0-4                     | 0-2               | 0-4             | 3-0            | 12-4  | 5-9  |                         |                   |
| 05                         | 7 01-3         | 7 02-4 | 6 42-1 | 0-5                     | 0-2               | 0-5             | 3-1            | 12-5  | 5-9  |                         |                   |
| 06                         | 7 01-5         | 7 02-7 | 6 42-3 | 0-6                     | 0-3               | 0-6             | 3-1            | 12-6  | 6-0  |                         |                   |
| 07                         | 7 01-8         | 7 02-9 | 6 42-5 | 0-7                     | 0-3               | 0-7             | 3-2            | 12-7  | 6-0  |                         |                   |
| 08                         | 7 02-0         | 7 03-2 | 6 42-8 | 0-8                     | 0-4               | 0-8             | 3-2            | 12-8  | 6-1  |                         |                   |
| 09                         | 7 02-3         | 7 03-4 | 6 43-0 | 0-9                     | 0-4               | 0-9             | 3-3            | 12-9  | 6-1  |                         |                   |
| 00                         | 7 15-0         | 7 16-2 | 6 55-2 | 0-0                     | 0-0               | 0-0             | 3-0            | 12-0  | 5-9  |                         |                   |
| 01                         | 7 15-3         | 7 16-4 | 6 55-4 | 0-1                     | 0-0               | 0-1             | 3-0            | 12-1  | 5-9  |                         |                   |
| 02                         | 7 15-5         | 7 16-7 | 6 55-7 | 0-2                     | 0-1               | 0-2             | 3-0            | 12-2  | 6-0  |                         |                   |
| 03                         | 7 15-8         | 7 16-9 | 6 55-9 | 0-3                     | 0-1               | 0-3             | 3-1            | 12-3  | 6-0  |                         |                   |
| 04                         | 7 16-0         | 7 17-2 | 6 56-1 | 0-4                     | 0-2               | 0-4             | 3-1            | 12-4  | 6-1  |                         |                   |
| 05                         | 7 16-3         | 7 17-4 | 6 56-4 | 0-5                     | 0-2               | 0-5             | 3-2            | 12-5  | 6-1  |                         |                   |
| 06                         | 7 16-5         | 7 17-7 | 6 56-6 | 0-6                     | 0-3               | 0-6             | 3-2            | 12-6  | 6-2  |                         |                   |
| 07                         | 7 16-8         | 7 17-9 | 6 56-9 | 0-7                     | 0-3               | 0-7             | 3-3            | 12-7  | 6-2  |                         |                   |
| 08                         | 7 17-0         | 7 18-2 | 6 57-1 | 0-8                     | 0-4               | 0-8             | 3-3            | 12-8  | 6-3  |                         |                   |
| 09                         | 7 17-3         | 7 18-4 | 6 57-3 | 0-9                     | 0-4               | 0-9             | 3-4            | 12-9  | 6-3  |                         |                   |

## Latitude by Meridian Passage Problems

Step 4: Determine the observed altitude for the sight using the correction tables in the Nautical Almanac (also provided at the end of this Part).

Sextant altitude (hs):  $48^{\circ} 45.9'$

Corrections:

Index error:  $2.6'$  on the arc ( $-2.6'$  index correction)

Height of eye:  $51.5'$  ( $-7.0'$  dip correction)

Apparent altitude (ha) =  $48^{\circ} 45.9' - 2.6' - 7.0' = 48^{\circ} 36.3'$

Apparent altitude correction:  $+15.1'$

Observed altitude (ho) =  $48^{\circ} 36.3' + 15.1' = 48^{\circ} 51.4'$

| DIP        |       |            |
|------------|-------|------------|
| Ht. of Eye | Corr. | Ht. of Eye |
| 15.1       | -0.8  | 49.8       |
| 15.5       | -6.9  | 51.3       |
| 16.0       | 7.0   | 52.8       |
| 16.5       | 7.1   | 54.3       |

Step 5: Note the DR latitude:  $26^{\circ} 24.0' S$

Step 6: Determine the declination of the body for the time of sight.

Declination (hours): N  $14^{\circ} 08.3$

Declination (increments):  $d = -0.8$ , therefore increment =  $-0.4'$

Declination (total): N  $14^{\circ} 08.3 - 0.4 = N 14^{\circ} 07.9'$

| OCT.—MAR. SUN |            |            | APR.—SEPT. |            |            |
|---------------|------------|------------|------------|------------|------------|
| App. Alt.     | Lower Limb | Upper Limb | App. Alt.  | Lower Limb | Upper Limb |
| 43 59         | +15.3      | -17.0      | 45 31      | +15.1      | -16.7      |
| 47 10         | +15.4      | -16.9      | 48 55      | +15.2      | -16.6      |
| 50 46         | +15.5      | -16.8      | 52 44      | +15.3      | -16.5      |

Step 7: Enter Altitude Factor Table in Bowditch to determine the altitude factor (a).

Bracketing values:

|                    | $14^{\circ} N$ | $14^{\circ} 07.9'$ | $15^{\circ} N$ |
|--------------------|----------------|--------------------|----------------|
| $26^{\circ} S$     | 2.7            |                    | 2.6            |
| $26^{\circ} 24' S$ |                | a                  |                |
| $27^{\circ} S$     | 2.6            |                    | 2.5            |

Interpolation:

|                  | $14^{\circ} N$ | $14.13^{\circ}$ | $15^{\circ} N$ |
|------------------|----------------|-----------------|----------------|
| $26^{\circ} S$   | 2.7            | 2.69            | 2.6            |
| $26.4^{\circ} S$ | 2.66           | a               | 2.56           |
| $27^{\circ} S$   | 2.6            | 2.59            | 2.5            |

Interpolated value:  $a = 2.63$

| Altitude Factor<br><i>a</i> , the change of altitude in one minute from meridian transit. |                                                                                           |     |     |     |     |     |     |     |     |     |     |     |     |    |  |  |  |  |  |  |  |  |          |
|-------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----|--|--|--|--|--|--|--|--|----------|
| Latitude                                                                                  | Declination contrary name to latitude, upper transit; add correction to observed altitude |     |     |     |     |     |     |     |     |     |     |     |     |    |  |  |  |  |  |  |  |  | Latitude |
|                                                                                           | 12°                                                                                       | 13° | 14° | 15° | 16° | 17° | 18° | 19° | 20° | 21° | 22° | 23° | 24° |    |  |  |  |  |  |  |  |  |          |
| 0                                                                                         | 9.2                                                                                       | 8.5 | 7.9 | 7.3 | 6.8 | 6.4 | 6.0 | 5.7 | 5.4 | 5.1 | 4.9 | 4.6 | 4.4 | 0  |  |  |  |  |  |  |  |  |          |
| 1                                                                                         | 8.5                                                                                       | 7.9 | 7.4 | 6.9 | 6.5 | 6.1 | 5.8 | 5.5 | 5.2 | 4.9 | 4.7 | 4.5 | 4.3 | 1  |  |  |  |  |  |  |  |  |          |
| 2                                                                                         | 7.9                                                                                       | 7.4 | 6.9 | 6.5 | 6.1 | 5.8 | 5.5 | 5.2 | 4.9 | 4.7 | 4.5 | 4.3 | 4.1 | 2  |  |  |  |  |  |  |  |  |          |
| 3                                                                                         | 7.4                                                                                       | 6.9 | 6.5 | 6.1 | 5.8 | 5.5 | 5.2 | 5.0 | 4.7 | 4.5 | 4.3 | 4.1 | 4.0 | 3  |  |  |  |  |  |  |  |  |          |
| 4                                                                                         | 7.0                                                                                       | 6.5 | 6.2 | 5.8 | 5.5 | 5.2 | 5.0 | 4.8 | 4.5 | 4.3 | 4.2 | 4.0 | 3.8 | 4  |  |  |  |  |  |  |  |  |          |
| 5                                                                                         | 6.5                                                                                       | 6.2 | 5.8 | 5.5 | 5.2 | 5.0 | 4.8 | 4.5 | 4.3 | 4.2 | 4.0 | 3.8 | 3.7 | 5  |  |  |  |  |  |  |  |  |          |
| 6                                                                                         | 6.2                                                                                       | 5.8 | 5.5 | 5.3 | 5.0 | 4.8 | 4.6 | 4.4 | 4.2 | 4.0 | 3.9 | 3.7 | 3.6 | 6  |  |  |  |  |  |  |  |  |          |
| 7                                                                                         | 5.9                                                                                       | 5.6 | 5.3 | 5.0 | 4.8 | 4.6 | 4.4 | 4.2 | 4.0 | 3.9 | 3.7 | 3.6 | 3.5 | 7  |  |  |  |  |  |  |  |  |          |
| 8                                                                                         | 5.6                                                                                       | 5.3 | 5.0 | 4.8 | 4.6 | 4.4 | 4.2 | 4.0 | 3.9 | 3.7 | 3.6 | 3.5 | 3.4 | 8  |  |  |  |  |  |  |  |  |          |
| 9                                                                                         | 5.3                                                                                       | 5.0 | 4.8 | 4.6 | 4.4 | 4.2 | 4.1 | 3.9 | 3.8 | 3.6 | 3.5 | 3.4 | 3.3 | 9  |  |  |  |  |  |  |  |  |          |
| 10                                                                                        | 5.0                                                                                       | 4.8 | 4.6 | 4.4 | 4.2 | 4.1 | 3.9 | 3.8 | 3.6 | 3.5 | 3.4 | 3.3 | 3.2 | 10 |  |  |  |  |  |  |  |  |          |
| 11                                                                                        | 4.8                                                                                       | 4.6 | 4.4 | 4.2 | 4.1 | 3.9 | 3.8 | 3.6 | 3.5 | 3.4 | 3.3 | 3.2 | 3.1 | 11 |  |  |  |  |  |  |  |  |          |
| 12                                                                                        | 4.6                                                                                       | 4.4 | 4.3 | 4.1 | 3.9 | 3.8 | 3.7 | 3.5 | 3.4 | 3.3 | 3.2 | 3.1 | 3.0 | 12 |  |  |  |  |  |  |  |  |          |
| 13                                                                                        | 4.4                                                                                       | 4.3 | 4.1 | 3.9 | 3.8 | 3.7 | 3.5 | 3.4 | 3.3 | 3.2 | 3.1 | 3.0 | 2.9 | 13 |  |  |  |  |  |  |  |  |          |
| 14                                                                                        | 4.2                                                                                       | 4.1 | 3.9 | 3.8 | 3.7 | 3.5 | 3.4 | 3.3 | 3.2 | 3.1 | 3.0 | 2.9 | 2.8 | 14 |  |  |  |  |  |  |  |  |          |
| 15                                                                                        | 4.1                                                                                       | 3.9 | 3.8 | 3.7 | 3.5 | 3.4 | 3.3 | 3.2 | 3.1 | 3.0 | 2.9 | 2.8 | 2.8 | 15 |  |  |  |  |  |  |  |  |          |
| 16                                                                                        | 3.9                                                                                       | 3.8 | 3.7 | 3.5 | 3.4 | 3.3 | 3.2 | 3.1 | 3.0 | 2.9 | 2.8 | 2.8 | 2.7 | 16 |  |  |  |  |  |  |  |  |          |
| 17                                                                                        | 3.8                                                                                       | 3.7 | 3.5 | 3.4 | 3.3 | 3.2 | 3.1 | 3.0 | 2.9 | 2.8 | 2.8 | 2.7 | 2.6 | 17 |  |  |  |  |  |  |  |  |          |
| 18                                                                                        | 3.7                                                                                       | 3.5 | 3.4 | 3.3 | 3.2 | 3.1 | 3.0 | 2.9 | 2.9 | 2.8 | 2.7 | 2.6 | 2.5 | 18 |  |  |  |  |  |  |  |  |          |
| 19                                                                                        | 3.5                                                                                       | 3.4 | 3.3 | 3.2 | 3.1 | 3.0 | 2.9 | 2.9 | 2.8 | 2.7 | 2.6 | 2.6 | 2.5 | 19 |  |  |  |  |  |  |  |  |          |
| 20                                                                                        | 3.4                                                                                       | 3.3 | 3.2 | 3.1 | 3.0 | 2.9 | 2.9 | 2.8 | 2.7 | 2.6 | 2.6 | 2.5 | 2.4 | 20 |  |  |  |  |  |  |  |  |          |
| 21                                                                                        | 3.3                                                                                       | 3.2 | 3.1 | 3.0 | 2.9 | 2.8 | 2.8 | 2.7 | 2.6 | 2.5 | 2.5 | 2.4 | 2.4 | 21 |  |  |  |  |  |  |  |  |          |
| 22                                                                                        | 3.2                                                                                       | 3.1 | 3.0 | 2.9 | 2.8 | 2.8 | 2.7 | 2.6 | 2.5 | 2.4 | 2.4 | 2.3 | 2.3 | 22 |  |  |  |  |  |  |  |  |          |
| 23                                                                                        | 3.1                                                                                       | 3.0 | 2.9 | 2.8 | 2.8 | 2.7 | 2.6 | 2.6 | 2.5 | 2.4 | 2.4 | 2.3 | 2.3 | 23 |  |  |  |  |  |  |  |  |          |
| 24                                                                                        | 3.0                                                                                       | 2.9 | 2.8 | 2.8 | 2.7 | 2.6 | 2.6 | 2.5 | 2.5 | 2.4 | 2.4 | 2.3 | 2.3 | 24 |  |  |  |  |  |  |  |  |          |
| 25                                                                                        | 2.9                                                                                       | 2.8 | 2.7 | 2.7 | 2.6 | 2.5 | 2.5 | 2.4 | 2.4 | 2.3 | 2.3 | 2.2 | 2.2 | 25 |  |  |  |  |  |  |  |  |          |
| 26                                                                                        | 2.8                                                                                       | 2.7 | 2.6 | 2.6 | 2.5 | 2.4 | 2.4 | 2.4 | 2.3 | 2.3 | 2.2 | 2.1 | 2.1 | 26 |  |  |  |  |  |  |  |  |          |
| 27                                                                                        | 2.7                                                                                       | 2.6 | 2.5 | 2.5 | 2.4 | 2.3 | 2.3 | 2.3 | 2.2 | 2.2 | 2.1 | 2.1 | 2.0 | 27 |  |  |  |  |  |  |  |  |          |
| 28                                                                                        | 2.6                                                                                       | 2.6 | 2.5 | 2.5 | 2.4 | 2.3 | 2.3 | 2.2 | 2.2 | 2.1 | 2.1 | 2.0 | 2.0 | 28 |  |  |  |  |  |  |  |  |          |
| 29                                                                                        | 2.6                                                                                       | 2.5 | 2.4 | 2.4 | 2.3 | 2.3 | 2.2 | 2.2 | 2.1 | 2.1 | 2.0 | 2.0 | 2.0 | 29 |  |  |  |  |  |  |  |  |          |

## Latitude by Meridian Passage Problems

Step 8: Enter Change in Altitude Table in Bowditch to determine the altitude change correction.

Bracketing values:

|          | t = 14m 20s | t = 14m 30 s | t = 14m 40s |
|----------|-------------|--------------|-------------|
| a = 2.0  | 6.8         |              | 7.2         |
| a = 2.63 |             | Correction   |             |
| a = 3.0  | 10.3        |              | 10.8        |

Interpolation:

|          | t = 14m 20s | t = 14m 30 s | t = 14m 40s |
|----------|-------------|--------------|-------------|
| a = 2.0  | 6.8         | 7.0          | 7.2         |
| a = 2.63 | 9.01        | Correction   | 9.47        |
| a = 3.0  | 10.3        | 10.55        | 10.8        |

Interpolated value = 9.0

Step 9: Apply the Change in Altitude correction to the observed altitude (ho) to determine the corrected altitude.

Observed altitude (ho): 48° 51.4'

Correction: +9.0'

Corrected altitude (ho (corr)): 48° 51.4' + 9.0' = 49° 00.4'

Step 10: Complete the meridian transit (LAN) calculation.

Altitude: 49° 00.4' (to the north)

Zenith Distance (90-Alt) = 40° 59.6'

Declination: 14° 07.9' N

Latitude (ZD – Dec in this case): 40° 59.6' – 14° 07.9' = **26° 51.7' S**

| Change of Altitude in Given Time from Meridian Transit |                   |         |         |         |         |         |         |         |         |         |         |         |         |         |     |                    |
|--------------------------------------------------------|-------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|-----|--------------------|
| a<br>(table<br>24)                                     | t, meridian angle |         |         |         |         |         |         |         |         |         |         |         |         |         |     | a<br>(table<br>24) |
|                                                        | 3° 35'            | 3° 40'  | 3° 45'  | 3° 50'  | 3° 55'  | 4° 00'  | 4° 05'  | 4° 10'  | 4° 15'  | 4° 20'  | 4° 25'  | 4° 30'  | 4° 35'  | 4° 40'  |     |                    |
|                                                        | 14° 20'           | 14° 40' | 15° 00' | 15° 20' | 15° 40' | 16° 00' | 16° 20' | 16° 40' | 17° 00' | 17° 20' | 17° 40' | 18° 00' | 18° 20' | 18° 40' |     |                    |
|                                                        | t                 | t       | t       | t       | t       | t       | t       | t       | t       | t       | t       | t       | t       | t       |     |                    |
| 0.1                                                    | 0.3               | 0.4     | 0.4     | 0.4     | 0.4     | 0.4     | 0.4     | 0.5     | 0.5     | 0.5     | 0.5     | 0.5     | 0.6     | 0.6     | 0.1 |                    |
| 0.2                                                    | 0.7               | 0.7     | 0.8     | 0.8     | 0.8     | 0.8     | 0.9     | 0.9     | 0.9     | 1.0     | 1.0     | 1.0     | 1.1     | 1.1     | 0.2 |                    |
| 0.3                                                    | 1.0               | 1.1     | 1.1     | 1.2     | 1.2     | 1.3     | 1.3     | 1.4     | 1.4     | 1.5     | 1.6     | 1.6     | 1.7     | 1.7     | 0.3 |                    |
| 0.4                                                    | 1.4               | 1.4     | 1.5     | 1.6     | 1.6     | 1.7     | 1.8     | 1.9     | 1.9     | 2.0     | 2.1     | 2.2     | 2.2     | 2.3     | 0.4 |                    |
| 0.5                                                    | 1.7               | 1.8     | 1.9     | 2.0     | 2.0     | 2.1     | 2.2     | 2.3     | 2.4     | 2.5     | 2.6     | 2.7     | 2.8     | 2.9     | 0.5 |                    |
| 0.6                                                    | 2.1               | 2.2     | 2.2     | 2.4     | 2.5     | 2.6     | 2.7     | 2.8     | 2.9     | 3.0     | 3.1     | 3.2     | 3.4     | 3.5     | 0.6 |                    |
| 0.7                                                    | 2.4               | 2.5     | 2.6     | 2.7     | 2.9     | 3.0     | 3.1     | 3.2     | 3.4     | 3.5     | 3.6     | 3.8     | 3.9     | 4.1     | 0.7 |                    |
| 0.8                                                    | 2.7               | 2.9     | 3.0     | 3.1     | 3.3     | 3.4     | 3.6     | 3.7     | 3.9     | 4.0     | 4.2     | 4.3     | 4.5     | 4.6     | 0.8 |                    |
| 0.9                                                    | 3.1               | 3.2     | 3.4     | 3.5     | 3.7     | 3.8     | 4.0     | 4.2     | 4.3     | 4.5     | 4.7     | 4.9     | 5.0     | 5.2     | 0.9 |                    |
| 1.0                                                    | 3.4               | 3.6     | 3.8     | 3.9     | 4.1     | 4.3     | 4.4     | 4.6     | 4.8     | 5.0     | 5.2     | 5.4     | 5.6     | 5.8     | 1.0 |                    |
| 2.0                                                    | 6.8               | 7.2     | 7.5     | 7.8     | 8.2     | 8.5     | 8.9     | 9.3     | 9.6     | 10.0    | 10.4    | 10.8    | 11.2    | 11.6    | 2.0 |                    |
| 3.0                                                    | 10.3              | 10.8    | 11.3    | 11.8    | 12.3    | 12.8    | 13.3    | 13.9    | 14.4    | 15.0    | 15.6    | 16.2    | 16.8    | 17.4    | 3.0 |                    |
| 4.0                                                    | 13.7              | 14.3    | 15.0    | 15.7    | 16.4    | 17.1    | 17.8    | 18.5    | 19.3    | 20.0    | 20.8    | 21.6    | 22.4    | 23.2    | 4.0 |                    |
| 5.0                                                    | 17.1              | 17.9    | 18.8    | 19.6    | 20.5    | 21.3    | 22.2    | 23.1    | 24.1    | 25.0    | 26.0    | 27.0    | 28.0    | 29.0    | 5.0 |                    |
| 6.0                                                    | 20.5              | 21.5    | 22.5    | 23.5    | 24.5    | 25.6    | 26.7    | 27.8    |         |         |         |         |         |         | 6.0 |                    |
| 7.0                                                    | 24.0              | 25.1    | 26.3    | 27.4    |         |         |         |         |         |         |         |         |         |         | 7.0 |                    |
| 8.0                                                    | 27.4              | 28.7    | 30.0    |         |         |         |         |         |         |         |         |         |         |         | 8.0 |                    |

## Latitude by Meridian Passage Problems

MER D5. On 16 June in DR position latitude  $50^{\circ} 57.0'$  S, longitude  $53^{\circ} 03.9'$  W (ZD +4), you take an ex-meridian observation of Acrux at lower transit. The chronometer time of the sight is 10h 08m 18s, and the chronometer error is 02m 12s fast. The sextant altitude (hs) is  $23^{\circ} 49.0'$ . The index error is 1.1' off the arc and your height of eye is 26 feet. What is the latitude at meridian transit?

Answer:  $50^{\circ} 41.1'$  S. In certain cases, depending on the observer's latitude, stars and planets can be circumpolar – they never set. In these cases, meridian transits can be observed twice per day. When the object is at its lowest point in the sky, it is called a lower transit. The calculations are the same as a typical meridian passage, with the exception of the LHA correction, the altitude factor table correction, and the latitude determination, each of which require a lower transit correction.

Step 1: Determine the chronometer time of sight based on chronometer error.  
 Chronometer time: 10h 08m 18s  
 Chronometer error: 00h 02m 12s fast  
 Correct sight time: 10h 08m 18s - 00h 02m 12s = 10h 06m 06s  
 Determine the GMT of the sight.  
 The correct zone descriptor is given in the problem, and the chronometer time of 10h 06m 06s is the correct GMT.

Step 2: Determine the time difference from meridian passage to the time of observation.  
 Time of sight: 10:06:06 GMT  
 GHA (Aries - hours):  $54^{\circ} 35.1'$   
 GHA (Aries - increment):  $1^{\circ} 31.8'$   
 GHA (Aries - total):  $54^{\circ} 35.1' + 1^{\circ} 31.8' = \underline{56^{\circ} 06.9'}$

SHA (Acrux):  $173^{\circ} 36.5'$   
 GHA (Aries):  $56^{\circ} 06.9'$   
 GHA (Acrux):  $173^{\circ} 36.5' + 56^{\circ} 06.9' = 229^{\circ} 43.4'$   
 Lower transit correction:  $-180^{\circ}$   
 GHA (Acrux – lower transit) =  $229^{\circ} 38.4' - 180^{\circ} = \underline{49^{\circ} 38.4'}$

DR longitude:  $53^{\circ} 03.9'$  W  
 LHA (Acrux):  $49^{\circ} 38.4' - 53^{\circ} 03.9'$  W =  $356^{\circ} 39.5'$   
 LHA difference from meridian passage (LHA =  $360^{\circ}$ ):  $360 - 356^{\circ} 39.5' = 3^{\circ} 20.5'$   
 LHA difference converted to time:  $3^{\circ} 20.5' = \underline{13m 22s}$

|        |    | ARIES  |  |
|--------|----|--------|--|
| G.M.T. |    | G.H.A. |  |
| 08     | 24 | 30.2   |  |
| 09     | 39 | 32.6   |  |
| 10     | 54 | 35.1   |  |
| 11     | 69 | 37.6   |  |

| 6 <sup>m</sup> INCREMENTS AND CORRECTIONS |        |             |        |      |                           |                           |                           |                           |                           |
|-------------------------------------------|--------|-------------|--------|------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| h                                         | m      | SUN PLANETS | ARIES  | MOON | or Corr <sup>n</sup><br>d | or Corr <sup>n</sup><br>d | or Corr <sup>n</sup><br>d | or Corr <sup>n</sup><br>d | or Corr <sup>n</sup><br>d |
| 00                                        | 1 30.0 | 1 30.2      | 1 25.9 | 0-0  | 0.0                       | 0-0                       | 0.7                       | 12-0                      | 1-3                       |
| 01                                        | 1 30.3 | 1 30.5      | 1 26.1 | 0-1  | 0.0                       | 0-1                       | 0.7                       | 12-1                      | 1-3                       |
| 02                                        | 1 30.5 | 1 30.7      | 1 26.4 | 0-2  | 0.0                       | 0-2                       | 0.7                       | 12-2                      | 1-3                       |
| 03                                        | 1 30.8 | 1 31.0      | 1 26.6 | 0-3  | 0.0                       | 0-3                       | 0.7                       | 12-3                      | 1-3                       |
| 04                                        | 1 31.0 | 1 31.2      | 1 26.9 | 0-4  | 0.0                       | 0-4                       | 0.7                       | 12-4                      | 1-3                       |
| 05                                        | 1 31.3 | 1 31.5      | 1 27.1 | 0-5  | 0.1                       | 0-5                       | 0.7                       | 12-5                      | 1-4                       |
| 06                                        | 1 31.5 | 1 31.8      | 1 27.3 | 0-6  | 0.1                       | 0-6                       | 0.7                       | 12-6                      | 1-4                       |
| 07                                        | 1 31.8 | 1 32.0      | 1 27.6 | 0-7  | 0.1                       | 0-7                       | 0.7                       | 12-7                      | 1-4                       |
| 08                                        | 1 32.0 | 1 32.3      | 1 27.8 | 0-8  | 0.1                       | 0-8                       | 0.7                       | 12-8                      | 1-4                       |
| 09                                        | 1 32.3 | 1 32.5      | 1 28.0 | 0-9  | 0.1                       | 0-9                       | 0.7                       | 12-9                      | 1-4                       |

| STARS     |          |      |      |
|-----------|----------|------|------|
| Name      | S.H.A.   | Dec. |      |
| Acomar    | 315 37.2 | S40  | 22.7 |
| Achernar  | 335 45.2 | S57  | 19.7 |
| Acrux     | 173 36.5 | S63  | 00.0 |
| Adhara    | 255 32.1 | S28  | 56.9 |
| Aldebaran | 291 17.8 | N16  | 28.2 |



## Latitude by Meridian Passage Problems

Step 3: Determine the observed altitude for the sight using the correction tables in the Nautical Almanac (provided at the end of this Part).

Sextant altitude (hs):  $23^{\circ} 49.0'$

Corrections:

Index error: 1.1' off the arc (+1.1' index correction)

Height of eye: 26' (-5.0' dip correction)

Apparent altitude (ha) =  $23^{\circ} 49.0' + 1.1' - 5.0' = 23^{\circ} 45.1'$

Apparent altitude correction: -2.2'

Observed altitude (ho) =  $23^{\circ} 45.1' - 2.2' = \underline{23^{\circ} 42.9'}$

Step 4: Note the DR latitude:  $50^{\circ} 57.0'$  S

Step 5: Determine the declination of the body for the time of sight.

Declination (total): S  $63^{\circ} 00.0'$

Step 6: Enter the Altitude Factor table in Bowditch to determine the altitude factor (a). Because it is a lower transit problem, be sure to use the correct table (lower portion of the "contrary" table). Refer to the tabular instructions in Bowditch if in doubt.

| Altitude Factor                                                |                                                                                           |     |     |     |     |     |     |     |     |     |     |     |     |          |
|----------------------------------------------------------------|-------------------------------------------------------------------------------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----------|
| a, the change of altitude in one minute from meridian transit. |                                                                                           |     |     |     |     |     |     |     |     |     |     |     |     |          |
| Latitude                                                       | Declination contrary name to latitude, upper transit: add correction to observed altitude |     |     |     |     |     |     |     |     |     |     |     |     | Latitude |
|                                                                | 51°                                                                                       | 52° | 53° | 54° | 55° | 56° | 57° | 58° | 59° | 60° | 61° | 62° | 63° |          |
|                                                                |                                                                                           |     |     |     |     |     |     |     |     |     |     |     |     | 30       |
|                                                                |                                                                                           |     |     |     |     |     |     |     |     |     |     |     |     | 31       |
|                                                                |                                                                                           |     |     |     |     |     |     |     |     |     |     |     |     | 32       |
|                                                                |                                                                                           |     |     |     |     |     |     |     |     |     |     |     |     | 33       |
|                                                                |                                                                                           |     |     |     |     |     |     |     |     |     |     | 0.8 |     | 34       |
|                                                                |                                                                                           |     |     |     |     |     |     |     |     |     |     | 0.7 |     | 35       |
|                                                                |                                                                                           |     |     |     |     |     |     |     |     |     | 0.8 | 0.8 | 0.7 | 36       |
|                                                                |                                                                                           |     |     |     |     |     |     |     |     |     | 0.8 | 0.8 | 0.7 | 37       |
|                                                                |                                                                                           |     |     |     |     |     |     |     |     |     | 0.8 | 0.8 | 0.7 | 38       |
|                                                                |                                                                                           |     |     |     |     |     |     |     |     |     | 0.8 | 0.8 | 0.7 | 39       |
|                                                                |                                                                                           |     |     |     |     |     |     |     |     |     | 0.8 | 0.8 | 0.7 | 40       |
|                                                                |                                                                                           |     |     |     |     |     |     |     |     |     | 0.8 | 0.7 | 0.7 | 41       |
|                                                                |                                                                                           |     |     |     |     |     |     |     |     |     | 0.8 | 0.7 | 0.7 | 42       |
|                                                                |                                                                                           |     |     |     |     |     |     |     |     |     | 0.7 | 0.7 | 0.7 | 43       |
|                                                                |                                                                                           |     |     |     |     |     |     |     |     |     | 0.7 | 0.7 | 0.7 | 44       |
|                                                                |                                                                                           |     |     |     |     |     |     |     |     |     | 0.7 | 0.7 | 0.7 | 45       |
|                                                                |                                                                                           |     |     |     |     |     |     |     |     |     | 0.7 | 0.7 | 0.7 | 46       |
|                                                                |                                                                                           |     |     |     |     |     |     |     |     |     | 0.7 | 0.7 | 0.7 | 47       |
|                                                                |                                                                                           |     |     |     |     |     |     |     |     |     | 0.7 | 0.7 | 0.6 | 48       |
|                                                                |                                                                                           |     |     |     |     |     |     |     |     |     | 0.7 | 0.7 | 0.6 | 49       |
|                                                                |                                                                                           |     |     |     |     |     |     |     |     |     | 0.7 | 0.7 | 0.6 | 50       |
|                                                                |                                                                                           |     |     |     |     |     |     |     |     |     | 0.7 | 0.7 | 0.6 | 51       |
|                                                                |                                                                                           |     |     |     |     |     |     |     |     |     | 0.7 | 0.6 | 0.6 | 52       |

No interpolation is necessary in this case. a = 0.6

## Latitude by Meridian Passage Problems

Step 7: Enter Change in Altitude table in Bowditch to determine the altitude change correction.

| Change of Altitude in Given Time from Meridian Transit |         |         |         |         |         |         |         |         |         |         |         |     |                 |
|--------------------------------------------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|-----|-----------------|
| t, meridian angle                                      |         |         |         |         |         |         |         |         |         |         |         |     | a<br>(table 24) |
| 2° 35'                                                 | 2° 40'  | 2° 45'  | 2° 50'  | 2° 55'  | 3° 00'  | 3° 05'  | 3° 10'  | 3° 15'  | 3° 20'  | 3° 25'  | 3° 30'  |     |                 |
| 10° 20'                                                | 10° 40' | 11° 00' | 11° 20' | 11° 40' | 12° 00' | 12° 20' | 12° 40' | 13° 00' | 13° 20' | 13° 40' | 14° 00' |     |                 |
| 0.2                                                    | 0.2     | 0.2     | 0.2     | 0.2     | 0.2     | 0.3     | 0.3     | 0.3     | 0.3     | 0.3     | 0.3     | 0.1 |                 |
| 0.4                                                    | 0.4     | 0.4     | 0.4     | 0.5     | 0.5     | 0.5     | 0.5     | 0.6     | 0.6     | 0.6     | 0.7     | 0.2 |                 |
| 0.5                                                    | 0.6     | 0.6     | 0.6     | 0.7     | 0.7     | 0.8     | 0.8     | 0.8     | 0.9     | 0.9     | 1.0     | 0.3 |                 |
| 0.7                                                    | 0.8     | 0.8     | 0.9     | 0.9     | 1.0     | 1.0     | 1.1     | 1.1     | 1.2     | 1.2     | 1.3     | 0.4 |                 |
| 0.9                                                    | 0.9     | 1.0     | 1.1     | 1.1     | 1.2     | 1.3     | 1.3     | 1.4     | 1.5     | 1.6     | 1.6     | 0.5 |                 |
| 1.1                                                    | 1.1     | 1.2     | 1.3     | 1.4     | 1.4     | 1.5     | 1.6     | 1.7     | 1.8     | 1.9     | 2.0     | 0.6 |                 |

Bracketing values:

|        | t = 13m 20s | t = 13m 22s       | t = 13m 40s |
|--------|-------------|-------------------|-------------|
| a = .6 | 1.8         | <b>Correction</b> | 1.9         |

Interpolated value = 1.8'

Step 8: Apply the Change in Altitude correction to the observed altitude (ho) to determine the corrected altitude.

Observed altitude (ho): 23° 42.9'

Correction: -1.8' (lower transit corrections are subtracted)

Corrected altitude (ho (corr)): 23° 42.9' - 1.8' = 23° 41.1'

Step 9: Complete the meridian transit calculation.

Altitude: 23° 41.1' (to the north)

Zenith Distance (90-Alt) = 66° 18.9'

Declination: 63° 00.0' S

Latitude (ZD + Dec in this case): 66° 18.9' + 63° 00.0' = 129° 18.9' S

Lower Transit correction: -180°

Latitude = 129° 18.9' - 180° = **50° 41.1' S**

## Latitude by Meridian Passage Problems

### Latitude at LAN

MER B1. On 7 November your 0830 zone time fix gives you a position of latitude  $27^{\circ} 36.0' \text{ N}$ , longitude  $163^{\circ} 19.0' \text{ W}$ . Your vessel is on course  $289^{\circ} \text{ T}$  and your speed is 19.0 knots. Local apparent noon (LAN) occurs at 1138 zone time, at which time a meridian altitude of the Sun's lower limb is observed. The observed altitude ( $H_o$ ) for this sight is  $45^{\circ} 35.0'$ . What is the calculated latitude at LAN?

- a)  $27^{\circ} 52.3' \text{ N}$
- b)  $27^{\circ} 53.4' \text{ N}$
- c)  $27^{\circ} 55.1' \text{ N}$
- d)  **$27^{\circ} 57.2' \text{ N}$  - correct**

MER B2. On 28 July your 0800 zone time fix gives you a position of latitude  $25^{\circ} 16.0' \text{ N}$ , longitude  $71^{\circ} 19.0' \text{ W}$ . Your vessel is on course  $026^{\circ} \text{ T}$  and your speed is 17.5 knots. Local apparent noon (LAN) occurs at 1149 zone time, at which time a meridian altitude of the Sun's lower limb is observed. The observed altitude ( $H_o$ ) for this sight is  $82^{\circ} 28.7'$ . What is the calculated latitude at LAN?

- a)  $26^{\circ} 21.9' \text{ N}$
- b)  $26^{\circ} 23.4' \text{ N}$
- c)  **$26^{\circ} 25.0' \text{ N}$  - correct**
- d)  $26^{\circ} 27.7' \text{ N}$

MER B3. On 22 February your 0612 zone time fix gives you a position of latitude  $27^{\circ} 16.2' \text{ S}$ , longitude  $37^{\circ} 41.6' \text{ W}$ . Your vessel is on course  $298^{\circ} \text{ T}$  at 14.2 knots. Local apparent noon (LAN) occurs at 1147 zone time, at which time a meridian altitude of the Sun's lower limb is observed. The observed altitude ( $H_o$ ) for this sight is  $73^{\circ} 33.3'$ . What is the calculated latitude at LAN?

- a)  **$26^{\circ} 31.4' \text{ S}$  - correct**
- b)  $26^{\circ} 29.5' \text{ S}$
- c)  $26^{\circ} 27.1' \text{ S}$
- d)  $26^{\circ} 24.8' \text{ S}$

MER B4. On 16 September your 0600 ZT fix gives you a position of latitude  $29^{\circ} 47.2' \text{ N}$ , longitude  $65^{\circ} 28.4' \text{ W}$ . Your vessel is on course  $242^{\circ} \text{ T}$  and your speed is 13.5 knots. Local apparent noon (LAN) occurs at 1227 ZT, at which time a meridian altitude of the Sun's lower limb is observed. The observed altitude ( $H_o$ ) for this sight is  $63^{\circ} 25.3'$ . What is the calculated latitude at LAN?

- a)  $29^{\circ} 07.9' \text{ N}$
- b)  $29^{\circ} 06.1' \text{ N}$
- c)  **$29^{\circ} 04.7' \text{ N}$  - correct**
- d)  $29^{\circ} 01.6' \text{ N}$

Latitude at 1200 (Advance/Retard LAN)

MER B5. On 13 October your 0515 zone time fix gives you a position of latitude  $26^{\circ} 53.0'$  N, longitude  $90^{\circ} 05.0'$  W. Your vessel is on course  $068^{\circ}$  T and your speed is 7.8 knots. Local apparent noon (LAN) occurs at 1145 zone time, at which time a meridian altitude of the Sun's lower limb is observed. The observed altitude (Ho) for this sight is  $54^{\circ} 51.5'$ . What is the latitude at 1200 ZT?

- a)  $27^{\circ} 13.3'$  N - correct
- b)  $27^{\circ} 14.6'$  N
- c)  $27^{\circ} 15.7'$  N
- d)  $27^{\circ} 16.8'$  N

MER B6. On 28 July your 0800 zone time (ZT) fix gives you a position of latitude  $25^{\circ} 16.0'$  N, longitude  $71^{\circ} 19.0'$  W. Your vessel is on course  $026^{\circ}$  T at 17.5 knots. Local apparent noon (LAN) occurs at 1150 ZT, at which time a meridian altitude of the Sun's lower limb is observed. The observed altitude (Ho) for this sight is  $82^{\circ} 28.7'$ . What is the latitude at 1200 ZT?

- a)  $26^{\circ} 25.0'$  N
- b)  $26^{\circ} 27.6'$  N - correct
- c)  $26^{\circ} 29.8'$  N
- d)  $26^{\circ} 32.0'$  N

MER B7. On 7 November your 0830 zone time fix gives you a position of latitude  $27^{\circ} 36.0'$  N, longitude  $162^{\circ} 19.0'$  W. Your vessel is on course  $289^{\circ}$  T and your speed is 19.0 knots. Local apparent noon (LAN) occurs at 1138 zone time, at which time a meridian altitude of the Sun's lower limb is observed. The observed altitude (Ho) for this sight is  $45^{\circ} 35.0'$ . What is the latitude at 1200 ZT?

- a)  $27^{\circ} 55.1'$  N
- b)  $27^{\circ} 57.2'$  N
- c)  $27^{\circ} 59.5'$  N - correct
- d)  $28^{\circ} 01.9'$  N

### Latitude from Ex-Meridian Sights

MER B8. On 15 December in DR position latitude  $23^{\circ} 24.0'$  N, longitude  $55^{\circ} 36.0'$  W, you take an ex-meridian observation of the Sun's lower limb. The chronometer time of the sight is 03h 45m 19s, and there is no chronometer error. The sextant altitude (hs) is  $43^{\circ} 02.3'$ . The index error is  $2.6'$  on the arc and your height of eye is 65.0 feet. What is the latitude at meridian transit?

- a)  **$23^{\circ} 33.5'$  N - correct**
- b)  $23^{\circ} 35.8'$  N
- c)  $23^{\circ} 38.1'$  N
- d)  $23^{\circ} 40.6'$  N

MER B9. On 27 March in DR position latitude  $32^{\circ} 31.0'$  N, longitude  $76^{\circ} 25.0'$  W, you take an ex-meridian observation of the Sun's lower limb. The chronometer time of the sight is 05h 23m 32s and the chronometer error is 01m 30s fast. The sextant altitude (hs) is  $59^{\circ} 59.0'$ . The index error is  $1.8'$  off the arc, and your height of eye is 52 feet. What is the latitude at meridian transit?

- a)  $32^{\circ} 21.6'$  N
- b)  **$32^{\circ} 29.5'$  N - correct**
- c)  $32^{\circ} 37.6'$  N
- d)  $32^{\circ} 46.2'$  N

MER B10. On 17 November in DR position latitude  $01^{\circ} 14.4'$  S, longitude  $148^{\circ} 45.5'$  E, you take an ex-meridian observation of the planet Venus at upper transit. The chronometer time of the sight is 05h 31m 42s and the chronometer error is 01m 50s fast. The sextant altitude (hs) is  $64^{\circ} 41.1'$ . The index error is  $1.8'$  off the arc and your height of eye is 50 feet. What is the latitude at meridian transit?

- a)  $01^{\circ} 14.4'$  S
- b)  $01^{\circ} 16.3'$  S
- c)  **$01^{\circ} 18.0'$  S - correct**
- d)  $01^{\circ} 20.2'$  S

MER B11. On 16 June in DR position latitude  $50^{\circ} 57.0'$  S, longitude  $53^{\circ} 03.9'$  W (ZD +4), you take an ex-meridian observation of Acrux at lower transit. The chronometer time of the sight is 10h 08m 18s, and the chronometer error is 02m 12s fast. The sextant altitude (hs) is  $23^{\circ} 49.0'$ . The index error is  $1.1'$  off the arc and your height of eye is 26 feet. What is the latitude at meridian transit?

- a)  **$50^{\circ} 41.2'$  S - correct**
- b)  $51^{\circ} 02.2'$  S
- c)  $51^{\circ} 33.0'$  S
- d)  $51^{\circ} 41.2'$  S

MER B12. On 22 August in DR position latitude  $29^{\circ} 41.8'$  N, longitude  $33^{\circ} 15.5'$  W, you take an ex-meridian observation of the Moon's upper limb at upper transit. The chronometer time of the sight is 08h 00m 02s and the chronometer error is 2m 20s slow. The sextant altitude (hs) is  $74^{\circ} 32.4'$ . The index error is 1.5' off the arc and your height of eye is 48 feet. What is the latitude at meridian transit?

- a)  $29^{\circ} 39.3'$  N
- b)  $29^{\circ} 41.3'$  N
- c)  **$29^{\circ} 47.8'$  N - correct**
- d)  $29^{\circ} 49.7'$  N

## **Star Identification Problems**





## Star Identification Problems

- The Starfinder (2102-D) is an instrument used for identifying stars and planets based on their azimuth (bearing) and altitude (height).
- The key to star identification problems is three-fold:
  - Use the correct hemisphere on the backing plate (North or South)
  - Use the correct plate based on latitude (all USCG Problems use the 25° plate).
  - Find the LHA of Aries (based on the GHA of Aries and your DR longitude).
- The vast majority of problems on USCG exams are of major navigational stars. However, there are some problems in the database seeking minor stars. For these minor star problems, the procedure is the same but requires an extra step at the end of looking up the star's right ascension (RA) and declination (dec) in the back of the Nautical Almanac.

SID D1. On 17 March your 1845 DR position is latitude 25° 10.0' N, longitude 66° 48.0' W. You observe an unidentified star bearing 320° T at an observed altitude (ho) of 50° 02.9'. The chronometer reads 10h 47m 49s and is 1m 54s fast. What star did you observe?

Answer: Mirfak.

Step 1: Determine the correct chronometer time of the sight.

Chronometer: 10h 47m 49s

Chronometer error: 1m 54s fast

Correct chronometer time: 10:47:49 – 00:01:54 = 10:45:55

Step 2: Determine the GMT of the sight.

Chronometer: 10h 45m 55s

1845 ZT DR Longitude: 66° 48.0' W corresponds to (+4 ZD)

GMT of sight: 22:45:55

Step 3: Determine the GHA of Aries for the time of the sight.

GHA Aries (hours): 145° 23.1'

GHA Aries (increment): 11° 30.6'

GHA Aries (Total): 145° 23.1' + 11° 30.6' = 156° 53.7'

Step 4: Determine the LHA of Aries for the time of the sight.

GHA Aries: 156° 53.7'

DR Longitude: 66° 48.0' W (W longitude subtract, E longitude add)

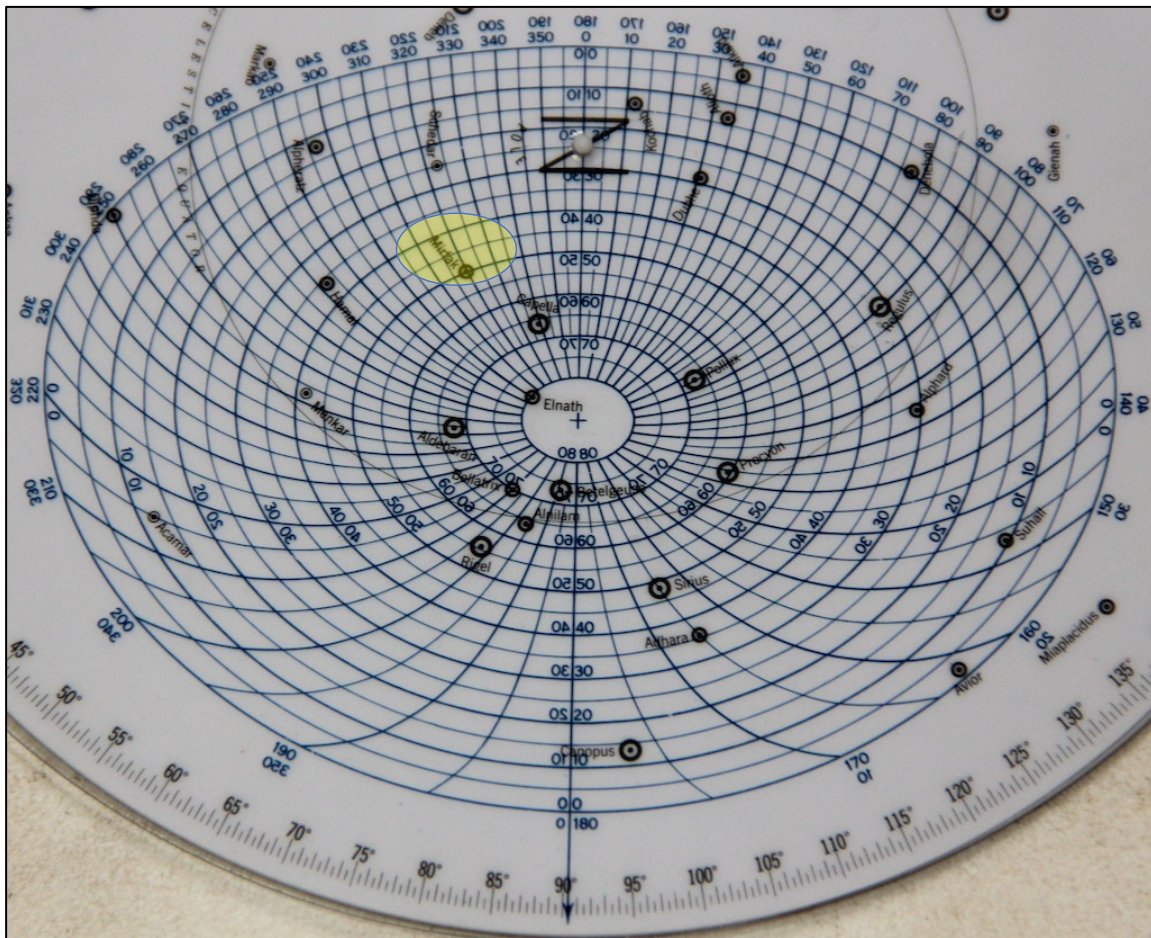
LHA Aries: 156° 53.7' – 66° 48.0' W = 90° 05.7'

|        |    | ARIES  |      |
|--------|----|--------|------|
| G.M.T. |    | G.H.A. |      |
| d      | h  | °      | '    |
| 17     | 00 | 174    | 28.8 |
|        | 01 | 189    | 31.3 |
|        | 02 | 204    | 33.8 |
|        | 03 | 219    | 36.2 |
|        | 04 | 234    | 38.7 |
|        | 05 | 249    | 41.2 |
|        | 06 | 264    | 43.6 |
|        | 07 | 279    | 46.1 |
|        | 08 | 294    | 48.6 |
|        | 09 | 309    | 51.0 |
|        | 10 | 324    | 53.5 |
|        | 11 | 339    | 55.9 |
|        | 12 | 354    | 58.4 |
|        | 13 | 10     | 00.9 |
|        | 14 | 25     | 03.3 |
|        | 15 | 40     | 05.8 |
|        | 16 | 55     | 08.3 |
|        | 17 | 70     | 10.7 |
|        | 18 | 85     | 13.2 |
|        | 19 | 100    | 15.7 |
|        | 20 | 115    | 18.1 |
|        | 21 | 130    | 20.6 |
|        | 22 | 145    | 23.1 |
|        | 23 | 160    | 25.5 |

| m  | SUN PLANETS | ARIES   |
|----|-------------|---------|
| 45 |             |         |
| 55 | 11 28.8     | 11 30.6 |
| 56 | 11 29.0     | 11 30.9 |
| 57 | 11 29.3     | 11 31.1 |
| 58 | 11 29.5     | 11 31.4 |
| 59 | 11 29.8     | 11 31.6 |

## Star Identification Problems

- Step 5: Set up the Starfinder.  
LHA Aries:  $90^{\circ} 05.7'$   
Observer's Latitude (nearest incremental degree):  $25^{\circ}$  N
- Step 6: Search the Starfinder field based on the given altitude and azimuth.  
Observed altitude (ho):  $50^{\circ} 02.9'$   
Observed azimuth:  $320^{\circ}$  T
- Step 7: Identify the observed body.  
**Mirfak** is the closest body to the observed altitude and azimuth.



## Star Identification Problems

SID D2. On 23 September, while taking stars for an evening fix, an unidentified star is observed bearing  $261^\circ$  T at an observed altitude (ho) of  $61^\circ 35'$ . Your 1836 zone time DR position is latitude  $25^\circ 18'$  S, longitude  $162^\circ 36'$  E. The chronometer reads 07h 34m 12s, and the chronometer error is 1m 54s slow. Your vessel is steaming on a course of  $230^\circ$  T at a speed of 18 knots. What star did you observe?

Answer: Antares.

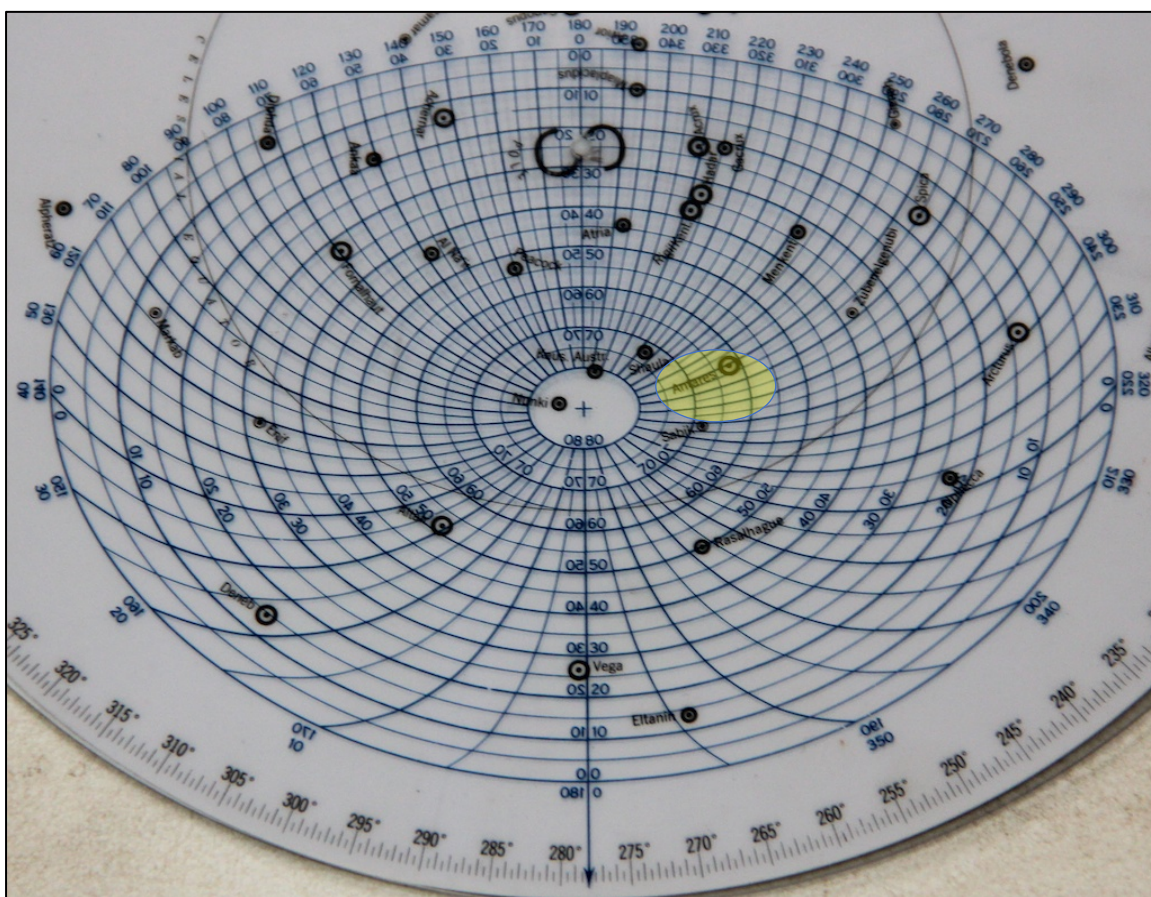
- Step 1: Determine the correct chronometer time of the sight.  
 Chronometer: 7h 34m 12s  
 Chronometer error: 1m 54s slow  
 Correct chronometer time:  $07:34:12 + 00:01:54 = 07:36:06$
- Step 2: Determine the GMT of the sight.  
 Chronometer: 07h 36m 06s  
 1836 ZT DR Longitude:  $162^\circ 36.0'$  E corresponds to (-11 ZD)  
 GMT of sight: 07:36:06
- Step 3: Determine the GHA of Aries for the time of the sight.  
 GHA Aries (hours):  $107^\circ 02.4'$   
 GHA Aries (increment):  $9^\circ 03.0'$   
 GHA Aries (Total):  $107^\circ 02.4' + 9^\circ 03.0' = 116^\circ 05.4'$
- Step 4: Determine the LHA of Aries for the time of the sight.  
 GHA Aries:  $116^\circ 05.4'$   
 DR Longitude:  $162^\circ 36.0'$  E (E longitude add, W longitude subtract)  
 LHA Aries:  $116^\circ 05.4' + 162^\circ 36.0' \text{ W} = \underline{278^\circ 41.4'}$
- Step 5: Set up the Starfinder.  
 LHA Aries:  $278^\circ 41.4'$   
 Observer's Latitude (nearest incremental degree):  $25^\circ$  S
- Step 6: Search the Starfinder field based on the given altitude and azimuth.  
 Observed altitude (ho):  $61^\circ 35.0'$   
 Observed azimuth:  $261^\circ$  T
- Step 7: Identify the observed body.  
**Antares** is the closest body to the observed altitude and azimuth.

|    |    |          |
|----|----|----------|
| 23 | 00 | 1 45.2   |
|    | 01 | 16 47.6  |
|    | 02 | 31 50.1  |
|    | 03 | 46 52.6  |
|    | 04 | 61 55.0  |
|    | 05 | 76 57.5  |
|    | 06 | 92 00.0  |
|    | 07 | 107 02.4 |
| W  | 08 | 122 04.9 |
| E  | 09 | 137 07.4 |
| D  | 10 | 152 09.8 |
| N  | 11 | 167 12.3 |
| E  | 12 | 182 14.7 |
| S  | 13 | 197 17.2 |
| D  | 14 | 212 19.7 |
| A  | 15 | 227 22.1 |
| Y  | 16 | 242 24.6 |
|    | 17 | 257 27.1 |
|    | 18 | 272 29.5 |
|    | 19 | 287 32.0 |
|    | 20 | 302 34.5 |
|    | 21 | 317 36.9 |
|    | 22 | 332 39.4 |
|    | 23 | 347 41.9 |

| 36 | SUN<br>PLANETS | ARIES  |
|----|----------------|--------|
| 00 | 9 00-0         | 9 01-5 |
| 01 | 9 00-3         | 9 01-7 |
| 02 | 9 00-5         | 9 02-0 |
| 03 | 9 00-8         | 9 02-2 |
| 04 | 9 01-0         | 9 02-5 |
| 05 | 9 01-3         | 9 02-7 |
| 06 | 9 01-5         | 9 03-0 |
| 07 | 9 01-8         | 9 03-2 |
| 08 | 9 02-0         | 9 03-5 |
| 09 | 9 02-3         | 9 03-7 |



# Star Identification Problems



## Star Identification Problems

SID D3. On 12 June 1981, your DR 1845 position is LAT  $21^{\circ} 47' N$ , LONG  $46^{\circ} 52' W$  when you observe a faint unidentifiable star through a break in the clouds. The star bears  $313^{\circ} T$  at a sextant altitude (Hs) of  $14^{\circ} 56.3'$ . The index error is  $0.5'$  on the arc and the height of eye is 45 feet. The chronometer reads 09:43:27 and the chronometer error is 1m 46s slow. What star did you observe?

Answer: Menkalinan (Minor Star)

- Step 1: Determine the correct chronometer time of the sight.  
 Chronometer: 9h 43m 27s  
 Chronometer error: 1m 46s slow  
 Correct chronometer time: 09:45:13
- Step 2: Determine the GMT of the sight.  
 1845 ZT DR Longitude:  $46^{\circ} 52' W$  corresponds to (+3 ZD)  
 GMT of sight: 21:45:13
- Step 3: Determine the GHA of Aries for the time of the sight.  
 GHA Aries (hours):  $216^{\circ} 05.6'$   
 GHA Aries (increment):  $11^{\circ} 20.1'$   
 GHA Aries (Total):  $227^{\circ} 25.7'$
- Step 4: Determine the LHA of Aries for the time of the sight.  
 GHA Aries:  $227^{\circ} 25.7'$   
 DR Longitude:  $46^{\circ} 52' W$  (E longitude add, W longitude subtract)  
 LHA Aries:  $180^{\circ} 33.7'$
- Step 5: Set up the Starfinder.  
 LHA Aries:  $180^{\circ} 33.7'$   
 Observer's Latitude (nearest incremental degree):  $25^{\circ} S$
- Step 6: Determine the Height Observed (Ho) by applying index error, height of eye and apparent altitude corrections.

$$\begin{aligned}
 H_s &= 14^{\circ} 56.3' \\
 IC &= +0.5' \\
 Dip &= -6.5' \\
 H_a &= 14^{\circ} 50.3' \\
 Alt\ Corr &= -3.6' \\
 H_o &= 14^{\circ} 46.7'
 \end{aligned}$$

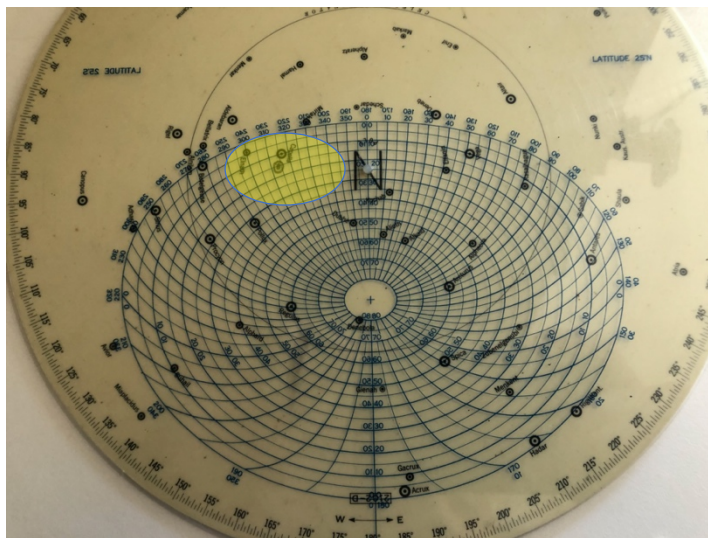
118

| G.M.T. | ARIES    |    | V |
|--------|----------|----|---|
|        | G.H.A.   |    |   |
| 12 00  | 260 13.9 | 16 |   |
| 01     | 275 16.4 | 17 |   |
| 02     | 290 18.8 | 15 |   |
| 03     | 305 21.3 | 20 |   |
| 04     | 320 23.8 | 22 |   |
| 05     | 335 26.2 | 23 |   |
| 06     | 350 28.7 | 25 |   |
| 07     | 5 31.1   | 26 |   |
| 08     | 20 33.6  | 28 |   |
| F 09   | 35 36.1  | 25 |   |
| R 10   | 50 38.5  | 31 |   |
| I 11   | 65 41.0  | 32 |   |
| D 12   | 80 43.5  | 34 |   |
| A 13   | 95 45.9  | 35 |   |
| Y 14   | 110 48.4 | 1  |   |
| 15     | 125 50.9 | 2  |   |
| 16     | 140 53.3 | 4  |   |
| 17     | 155 55.8 | 5  |   |
| 18     | 170 58.3 | 7  |   |
| 19     | 186 00.7 | 8  |   |
| 20     | 201 03.2 | 10 |   |
| 21     | 216 05.6 | 11 |   |
| 22     | 231 08.1 | 13 |   |
| 23     | 246 10.6 | 14 |   |

| m  | SUN PLANETS |   |
|----|-------------|---|
|    | s           | i |
| 00 | 11 15-0     |   |
| 01 | 11 15-3     |   |
| 02 | 11 15-5     |   |
| 03 | 11 15-8     |   |
| 04 | 11 16-0     |   |
| 05 | 11 16-3     |   |
| 06 | 11 16-5     |   |
| 07 | 11 16-8     |   |
| 08 | 11 17-0     |   |
| 09 | 11 17-3     |   |
| 10 | 11 17-5     |   |
| 11 | 11 17-8     |   |
| 12 | 11 18-0     |   |
| 13 | 11 18-3     |   |
| 14 | 11 18-5     |   |

## Star Identification Problems

- Step 7: Make a mark on the Starfinder plate at the appropriate Ho and Azimuth.  
Observed altitude (ho):  $14^{\circ} 46.7'$   
Observed azimuth:  $313^{\circ}$  T
- Step 8: Find the Right Ascension and Declination of the body.  
Put the red template on the Starfinder.  
Align  $0^{\circ}$  line with mark you made in Step 8.  
RA is the outer number on the Starfinder =  $87^{\circ}$   
Declination is based on location on the red plate =  $45^{\circ}$  N
- Step 9: Find the SHA.  
 $\text{SHA} = 360 - \text{RA} = 273^{\circ}$
- Step 10: Look in the back of the Nautical Almanac for the best match (note more accuracy can be obtained by averaging the  $25^{\circ}$  and  $15^{\circ}$  plate, which is rarely necessary to answer the exam question).  
**B Auriga, or Menkalinan.**



## STARS, JANUARY—JUNE

| Mag.   | Name and Number    | S.H.A. |      |      |      |      |      |      | Dec.  |      |      |      |      |      |      |
|--------|--------------------|--------|------|------|------|------|------|------|-------|------|------|------|------|------|------|
|        |                    | JAN.   | FEB. | MAR. | APR. | MAY  | JUNE |      | JAN.  | FEB. | MAR. | APR. | MAY  | JUNE |      |
| 1·6    | α Geminorum        | 246    | 39·0 | 39·0 | 39·1 | 39·2 | 39·4 | 39·4 | N. 31 | 55·7 | 55·8 | 55·8 | 55·9 | 55·9 | 55·8 |
| 3·3    | σ Puppis           | 247    | 50·2 | 50·2 | 50·4 | 50·6 | 50·8 | 50·9 | S. 43 | 15·9 | 16·0 | 16·1 | 16·1 | 16·1 | 16·0 |
| 3·1    | β Canis Minoris    | 248    | 28·0 | 28·0 | 28·1 | 28·2 | 28·3 | 28·4 | N. 8  | 19·6 | 19·6 | 19·5 | 19·6 | 19·6 | 19·6 |
| 2·4    | η Canis Majoris    | 249    | 09·6 | 09·6 | 09·7 | 09·9 | 10·0 | 10·1 | S. 29 | 16·1 | 16·2 | 16·3 | 16·3 | 16·2 | 16·1 |
| 2·7    | π Puppis           | 250    | 52·6 | 52·6 | 52·8 | 53·0 | 53·1 | 53·2 | S. 37 | 03·9 | 04·0 | 04·1 | 04·1 | 04·1 | 04·0 |
| 2·0    | δ Canis Majoris    | 253    | 05·5 | 05·5 | 05·6 | 05·8 | 05·9 | 06·0 | S. 26 | 21·9 | 22·0 | 22·1 | 22·1 | 22·0 | 21·9 |
| 3·1    | ο Canis Majoris    | 254    | 26·3 | 26·3 | 26·4 | 26·6 | 26·7 | 26·8 | S. 23 | 48·4 | 48·6 | 48·6 | 48·6 | 48·6 | 48·5 |
| 1·6    | ε Canis Majoris 19 | 255    | 31·6 | 31·6 | 31·7 | 31·9 | 32·0 | 32·1 | S. 28 | 56·9 | 57·0 | 57·1 | 57·1 | 57·0 | 56·9 |
| 2·8    | τ Puppis           | 257    | 37·6 | 37·7 | 37·9 | 38·1 | 38·4 | 38·5 | S. 50 | 35·7 | 35·8 | 35·9 | 35·9 | 35·8 | 35·7 |
| -1·6   | α Canis Majoris 18 | 258    | 55·2 | 55·2 | 55·3 | 55·5 | 55·6 | 55·6 | S. 16 | 41·6 | 41·7 | 41·7 | 41·7 | 41·6 | 41·5 |
| 1·9    | γ Geminorum        | 260    | 50·6 | 50·7 | 50·8 | 50·9 | 51·0 | 51·0 | N. 16 | 24·9 | 24·9 | 24·9 | 24·9 | 24·9 | 24·9 |
| -0·9   | α Carinæ 17        | 264    | 06·6 | 06·7 | 06·9 | 07·2 | 07·4 | 07·5 | S. 52 | 41·3 | 41·4 | 41·5 | 41·5 | 41·4 | 41·3 |
| 2·0    | β Canis Majoris    | 264    | 31·9 | 31·9 | 32·0 | 32·2 | 32·3 | 32·3 | S. 17 | 56·9 | 57·0 | 57·1 | 57·0 | 57·0 | 56·9 |
| 2·7    | θ Aurigæ           | 270    | 23·4 | 23·5 | 23·7 | 23·8 | 23·9 | 23·9 | N. 37 | 12·7 | 12·7 | 12·7 | 12·7 | 12·7 | 12·7 |
| 2·1    | β Aurigæ           | 270    | 27·8 | 27·9 | 28·0 | 28·2 | 28·3 | 28·3 | N. 44 | 56·8 | 56·8 | 56·9 | 56·8 | 56·8 | 56·7 |
| Var. † | α Orionis 16       | 271    | 27·7 | 27·8 | 27·9 | 28·0 | 28·1 | 28·1 | N. 7  | 24·1 | 24·1 | 24·1 | 24·1 | 24·1 | 24·2 |
| 2·2    | κ Orionis          | 273    | 17·0 | 17·1 | 17·2 | 17·4 | 17·4 | 17·4 | S. 9  | 40·7 | 40·8 | 40·8 | 40·8 | 40·7 | 40·6 |
| 1·9    | ζ Orionis          | 275    | 02·9 | 02·9 | 03·1 | 03·2 | 03·3 | 03·2 | S. 1  | 57·3 | 57·3 | 57·3 | 57·3 | 57·3 | 57·2 |
| 2·8    | α Columbæ          | 275    | 15·4 | 15·5 | 15·6 | 15·8 | 15·9 | 15·9 | S. 34 | 05·3 | 05·4 | 05·4 | 05·4 | 05·3 | 05·1 |
| 3·0    | ζ Tauri            | 275    | 52·2 | 52·3 | 52·4 | 52·6 | 52·6 | 52·6 | N. 21 | 07·8 | 07·8 | 07·8 | 07·8 | 07·8 | 07·8 |

## Star and Planet Identification Problems

### Star Identification of Navigational Stars

SID B1. At 0520 zone time, on 17 March while taking stars for a morning fix, you observe an unidentified star bearing  $050^{\circ}$  T at an observed altitude (ho) of  $45^{\circ} 00.0'$ . Your DR position at the time of the sight is latitude  $27^{\circ} 23.0'$  N, longitude  $39^{\circ} 42.0'$  W. The chronometer time of the sight is 08h 22m 15s and the chronometer error is 1m 45s fast. Your vessel is steaming on a course of  $300^{\circ}$  T at a speed of 18 knots. What star did you observe?

- a) Altair
- b) Alkaid
- c) Arcturus
- d) **Deneb - correct**

SID B2. At 1845 zone time on 17 March, while taking stars for an evening fix, you observe an unidentified star bearing  $200^{\circ}$  T at an observed altitude of  $53^{\circ} 45.0'$ . Your DR position at the time of the sight is latitude  $25^{\circ} 10.0'$  N, longitude  $66^{\circ} 48.0'$  W. The chronometer time of the sight is 10h 47m 49s and the chronometer error is 1m 54s fast. Your vessel is steaming on a course of  $290^{\circ}$  at a speed of 18 knots. What star did you observe?

- a) Altair
- b) Mirfak
- c) Pollux
- d) **Rigel - correct**

SID B3. On 14 January your 0550 zone time DR position is latitude  $25^{\circ} 26.0'$  N, longitude  $38^{\circ} 16.0'$  W. You observe an unidentifiable star bearing  $004.5^{\circ}$  T, at an observed altitude (ho) of  $40^{\circ} 10.0'$ . The chronometer reads 08h 48m 51s and is 01m 22s slow. What star did you observe?

- a) Gienah
- b) **Kochab - correct**
- c) Gacrux
- d) Eltanin

SID B4. On 22 April, your 1852 zone time DR position is latitude  $23^{\circ} 54.5'$  N, longitude  $117^{\circ} 36.8'$  W. You observe an unidentifiable star bearing  $259^{\circ}$  T at an observed altitude (ho) of  $41^{\circ} 15.2'$ . The chronometer reads 02h 54m 53s and is 02m 51s fast. What star did you observe?

- a) Diphda
- b) **Betelgeuse - correct**
- c) Gienah
- d) Arcturus



### Star Identification of Minor Stars

SID B5. On 12 June, your 1945 DR position is latitude  $21^{\circ} 47.0'$  N, longitude  $46^{\circ} 52.0'$  W when you observe a faint unidentifiable star through a break in the clouds. The star bears  $130^{\circ}$  T at a sextant altitude (hs) of  $45^{\circ} 21.2'$ . The index error is  $0.5'$  on the arc and the height of eye is 45 feet. The chronometer reads 10h 43m 27s and the chronometer error is 1m 46s slow. What star did you observe?

- a) Theta Carinae
- b) Epsilon Leonis
- c) **Beta Librae - correct**
- d) Zeta Puppis

SID B6. On 12 June, your 1845 DR position is latitude  $21^{\circ} 47.0'$  N, longitude  $46^{\circ} 52.0'$  W when you observe a faint unidentifiable star through a break in the clouds. The star bears  $162^{\circ}$  T at a sextant altitude (hs) of  $28^{\circ} 36.5'$ . The index error is  $0.5'$  on the arc and the height of eye is 45 feet. The chronometer reads 09h 43m 27s and the chronometer error is 1m 46s slow. What star did you observe?

- a) Gamma Virginis
- b) **Iota Centauri - correct**
- c) Spica
- d) Mimosa

SID B7. On 12 June, your 1845 DR position is latitude  $21^{\circ} 47.0'$  N, longitude  $46^{\circ} 52.0'$  W when you observe a faint unidentifiable star through a break in the clouds. The star bears  $031^{\circ}$  T at a sextant altitude (hs) of  $70^{\circ} 10.3'$ . The index error is  $0.5'$  on the arc and the height of eye is 45 feet. The chronometer reads 09h 43m 27s and the chronometer error is 1m 46s slow. What star did you observe?

- a) Sheratan
- b) Ruchbah
- c) Mimosa
- d) **Cor Caroli - correct**



## **Star Selection Problems**



## Star Selection Problems

- When selecting stars for a fix, look for objects equally distributed throughout the sky in terms of azimuth, and at an elevation between about 20° - 60°. Remember that objects on opposite azimuths will yield similar lines of position.
- Planets and the Moon move at different rates across the background celestial sphere compared to planets. When solving problems involving planets or the moon using the Starfinder, the red RA/Dec template is necessary to plot the bodies on the white template.

SSL D1. On 28 February, your 1850 zone time DR position is latitude 27° 49.0' N, longitude 159° 24.0' W. Considering their magnitude, azimuth, and altitude, which group includes the three stars best suited for a fix at star time?

- Rigel, Schedar, Regulus- correct
- Sirius, Mirfak, Elnath
- Hamal, Alkaid, Canopus
- Bellatrix, Vega, Regulus

Step 1: Determine the approximate time of star time.  
In this problem, no course or speed is given, so you may assume that star time is approximately 1850 ZT.

Step 2: Determine the GMT of the sight.  
Chronometer: 1850 ZT  
DR Longitude: 159° 24.0' W corresponds to (+11 ZD)  
GMT of sight: 0550 GMT, 1 March

Step 3: Determine the GHA of Aries for the time of the sight.  
GHA Aries (hours): 233° 54.9'  
GHA Aries (increment): 12° 32.1'  
GHA Aries (Total): 233° 54.9' + 12° 32.1' = 246° 27.0'

Step 4: Determine the LHA of Aries for the time of the sight.  
GHA Aries: 246° 27.0'  
DR Longitude: 159° 24.0' W (W longitude subtract, E longitude add)  
LHA Aries: 246° 27.0' - 159° 24.0' W = 87° 03.0'

|          |    | ARIES    |      |
|----------|----|----------|------|
| G. M. T. |    | G. H. A. |      |
| 1        | 00 | 158      | 42.6 |
|          | 01 | 173      | 45.1 |
|          | 02 | 188      | 47.5 |
|          | 03 | 203      | 50.0 |
|          | 04 | 218      | 52.5 |
|          | 05 | 233      | 54.9 |
|          | 06 | 248      | 57.4 |
|          | 07 | 263      | 59.9 |
|          | 08 | 279      | 02.3 |
| S        | 09 | 294      | 04.8 |
| U        | 10 | 309      | 07.3 |
| N        | 11 | 324      | 09.7 |
| D        | 12 | 339      | 12.2 |
| A        | 13 | 354      | 14.7 |
| Y        | 14 | 9        | 17.1 |
|          | 15 | 24       | 19.6 |
|          | 16 | 39       | 22.0 |
|          | 17 | 54       | 24.5 |
|          | 18 | 69       | 27.0 |
|          | 19 | 84       | 29.4 |
|          | 20 | 99       | 31.9 |
|          | 21 | 114      | 34.4 |
|          | 22 | 129      | 36.8 |
|          | 23 | 144      | 39.3 |

| 50 | SUN<br>PLANETS | ARIES   |
|----|----------------|---------|
| s  | o              | o       |
| 00 | 12 30-0        | 12 32-1 |
| 01 | 12 30-3        | 12 32-3 |
| 02 | 12 30-5        | 12 32-6 |
| 03 | 12 30-8        | 12 32-8 |
| 04 | 12 31-0        | 12 33-1 |

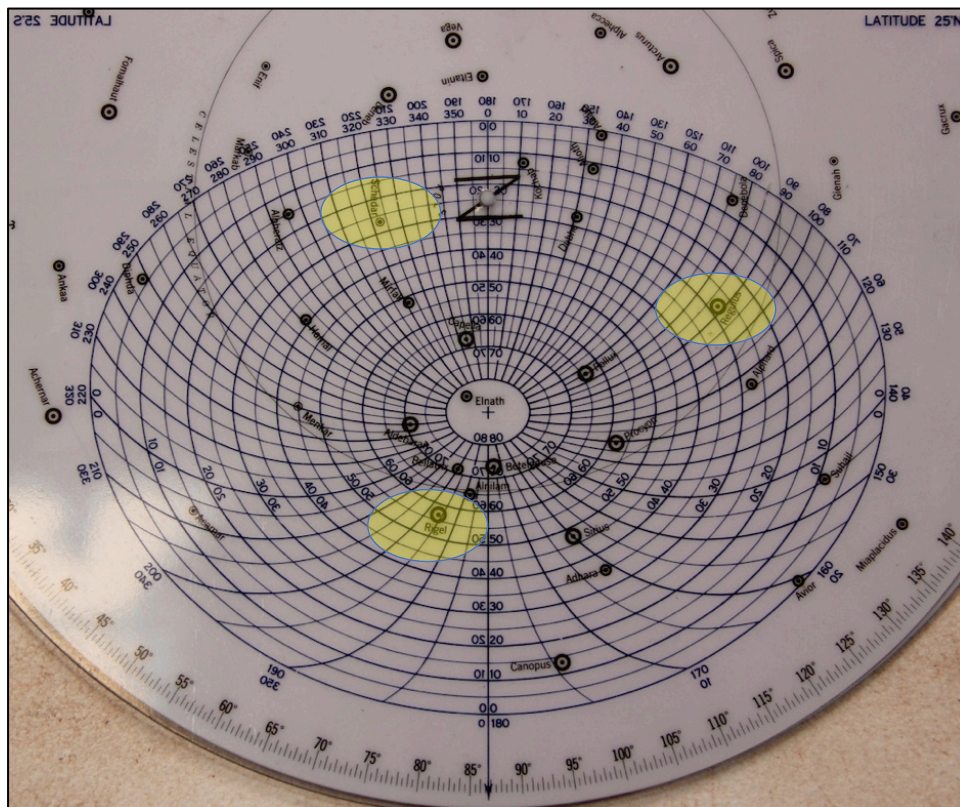
## Star Selection Problems

Step 5: Set up the Starfinder.  
LHA Aries:  $87^{\circ} 03.0'$

Observer's Latitude (nearest incremental degree):  $25^{\circ}$  N

Step 6: Examine the given stars on the Starfinder and make the best selection.

- Rigel, Schedar, Regulus**: distributed at appropriate azimuths and altitudes.
- Sirius, Mirfak, Elnath**: Elnath is too high in the sky, and Sirius/Mirfak are nearly exactly opposite in the sky.
- Hamal, Alkaid, Canopus**: Canopus is too low in the sky and Alkaid is on the horizon.
- Bellatrix, Vega, Regulus**: Bellatrix is too high in the sky and Vega is below the horizon.



## Star Selection Problems

SSL D2. On 23 March, your 1600 zone time DR position is latitude  $27^{\circ} 16.3' \text{ N}$ , longitude  $156^{\circ} 48.2' \text{ W}$ . You are on course  $063^{\circ} \text{ T}$  at a speed of 18 knots. Considering their magnitude, azimuth, and altitude, which group includes the three best stars suited for a fix at star time?

- a) Arcturus, Regulus, Sirius
- b) Procyon, Sirius, Capella
- c) Hamal, Rigel, Alpheratz - correct
- d) Betelgeuse, Dubhe, Regulus

Step 1: Determine the approximate time of star time.  
Based on the DR position, star time is close to 1900 for 23 March.

Step 2: Advance the ship's DR position from 1600 to 1900 (for detailed explanation, see Part 5, Great Circles and Sailings Problems, or Part 9, Time of Phenomenon Problems).  
1600 DR position:  $27^{\circ} 16.3' \text{ N}$ ,  $156^{\circ} 48.2' \text{ W}$   
1900 DR position:  $27^{\circ} 40.8' \text{ N}$ ,  $155^{\circ} 54.0' \text{ W}$

Step 3: Determine the GMT of the sight.  
Chronometer: 1900 ZT  
DR Longitude:  $155^{\circ} 54.0' \text{ W}$  corresponds to (+10 ZD)  
GMT of sight: 0500 GMT, 24 March

Step 4: Determine the GHA of Aries for the time of the sight.  
GHA Aries (hours/total):  $256^{\circ} 35.1'$

Step 5: Determine the LHA of Aries for the time of the sight.  
GHA Aries:  $256^{\circ} 35.1'$   
DR Longitude:  $155^{\circ} 54.0' \text{ W}$  (W longitude subtract, E longitude add)  
LHA Aries:  $256^{\circ} 35.1' - 155^{\circ} 54.0' \text{ W} = \underline{100^{\circ} 41.1'}$

| Lat. | Sunset |       | Twilight |       | Moonset |       |       |     |
|------|--------|-------|----------|-------|---------|-------|-------|-----|
|      |        |       | Civil    | Naut. | 23      | 24    | 25    | 26  |
| N 72 | h m    | h m   | h m      | h m   | h m     | h m   | h m   | h m |
| N 70 | 18 37  | 19 47 | 21 25    | 06 28 | 06 15   | 05 57 | 05 24 |     |
| 68   | 18 34  | 19 36 | 21 00    | 06 39 | 06 33   | 06 26 | 06 18 |     |
| 66   | 18 31  | 19 28 | 20 41    | 06 47 | 06 47   | 06 48 | 06 51 |     |
| 64   | 18 29  | 19 21 | 20 27    | 06 54 | 06 59   | 07 05 | 07 15 |     |
| 62   | 18 27  | 19 15 | 20 15    | 07 01 | 07 09   | 07 19 | 07 34 |     |
| 60   | 18 25  | 19 10 | 20 05    | 07 06 | 07 17   | 07 31 | 07 49 |     |
| 58   | 18 24  | 19 06 | 19 57    | 07 11 | 07 25   | 07 41 | 08 02 |     |
| 56   | 18 23  | 19 02 | 19 50    | 07 15 | 07 31   | 07 50 | 08 14 |     |
| 54   | 18 22  | 18 59 | 19 44    | 07 18 | 07 37   | 07 58 | 08 23 |     |
| 52   | 18 21  | 18 56 | 19 39    | 07 22 | 07 42   | 08 05 | 08 32 |     |
| 50   | 18 20  | 18 54 | 19 34    | 07 25 | 07 47   | 08 11 | 08 40 |     |
| 48   | 18 19  | 18 51 | 19 30    | 07 27 | 07 51   | 08 17 | 08 47 |     |
| 46   | 18 17  | 18 47 | 19 21    | 07 33 | 08 00   | 08 29 | 09 02 |     |
| 44   | 18 16  | 18 43 | 19 15    | 07 38 | 08 08   | 08 39 | 09 14 |     |
| 42   | 18 15  | 18 40 | 19 10    | 07 43 | 08 14   | 08 48 | 09 25 |     |
| 40   | 18 14  | 18 38 | 19 06    | 07 47 | 08 20   | 08 56 | 09 34 |     |
| 38   | 18 12  | 18 34 | 19 00    | 07 53 | 08 30   | 09 09 | 09 50 |     |
| 36   | 18 11  | 18 32 | 18 56    | 07 59 | 08 39   | 09 21 | 10 04 |     |
| 34   | 18 10  | 18 30 | 18 54    | 08 05 | 08 48   | 09 32 | 10 17 |     |
| 32   | 18 08  | 18 29 | 18 54    | 08 10 | 08 56   | 09 43 | 10 30 |     |
| 30   | 18 07  | 18 29 | 18 55    | 08 16 | 09 05   | 09 54 | 10 44 |     |
| 28   | 18 06  | 18 30 | 18 58    | 08 23 | 09 15   | 10 08 | 11 00 |     |
| 26   | 18 06  | 18 31 | 19 00    | 08 27 | 09 21   | 10 16 | 11 10 |     |
| 24   | 18 05  | 18 32 | 19 04    | 08 31 | 09 28   | 10 24 | 11 21 |     |
| 22   | 18 05  | 18 34 | 19 08    | 08 36 | 09 36   | 10 35 | 11 33 |     |
| 20   | 18 04  | 18 36 | 19 14    | 08 42 | 09 45   | 10 48 | 11 49 |     |
| 18   | 18 03  | 18 37 | 19 16    | 08 45 | 09 50   | 10 53 | 11 56 |     |
| 16   | 18 03  | 18 38 | 19 20    | 08 48 | 09 55   | 11 00 | 12 04 |     |
| 14   | 18 03  | 18 40 | 19 23    | 08 52 | 10 00   | 11 07 | 12 13 |     |
| 12   | 18 02  | 18 41 | 19 28    | 08 56 | 10 06   | 11 15 | 12 23 |     |
| 10   | 18 02  | 18 43 | 19 32    | 09 00 | 10 13   | 11 25 | 12 35 |     |

|       |          |
|-------|----------|
| 24 00 | 181 22.8 |
| 01    | 196 25.3 |
| 02    | 211 27.7 |
| 03    | 226 30.2 |
| 04    | 241 32.7 |
| 05    | 256 35.1 |
| 06    | 271 37.6 |
| 07    | 286 40.1 |
| 08    | 301 42.5 |
| 09    | 316 45.0 |
| 10    | 331 47.5 |
| 11    | 346 49.9 |
| 12    | 1 52.4   |
| 13    | 16 54.8  |
| 14    | 31 57.3  |
| 15    | 46 59.8  |
| 16    | 62 02.2  |
| 17    | 77 04.7  |
| 18    | 92 07.2  |
| 19    | 107 09.6 |
| 20    | 122 12.1 |
| 21    | 137 14.6 |
| 22    | 152 17.0 |
| 23    | 167 19.5 |



## Star Selection Problems

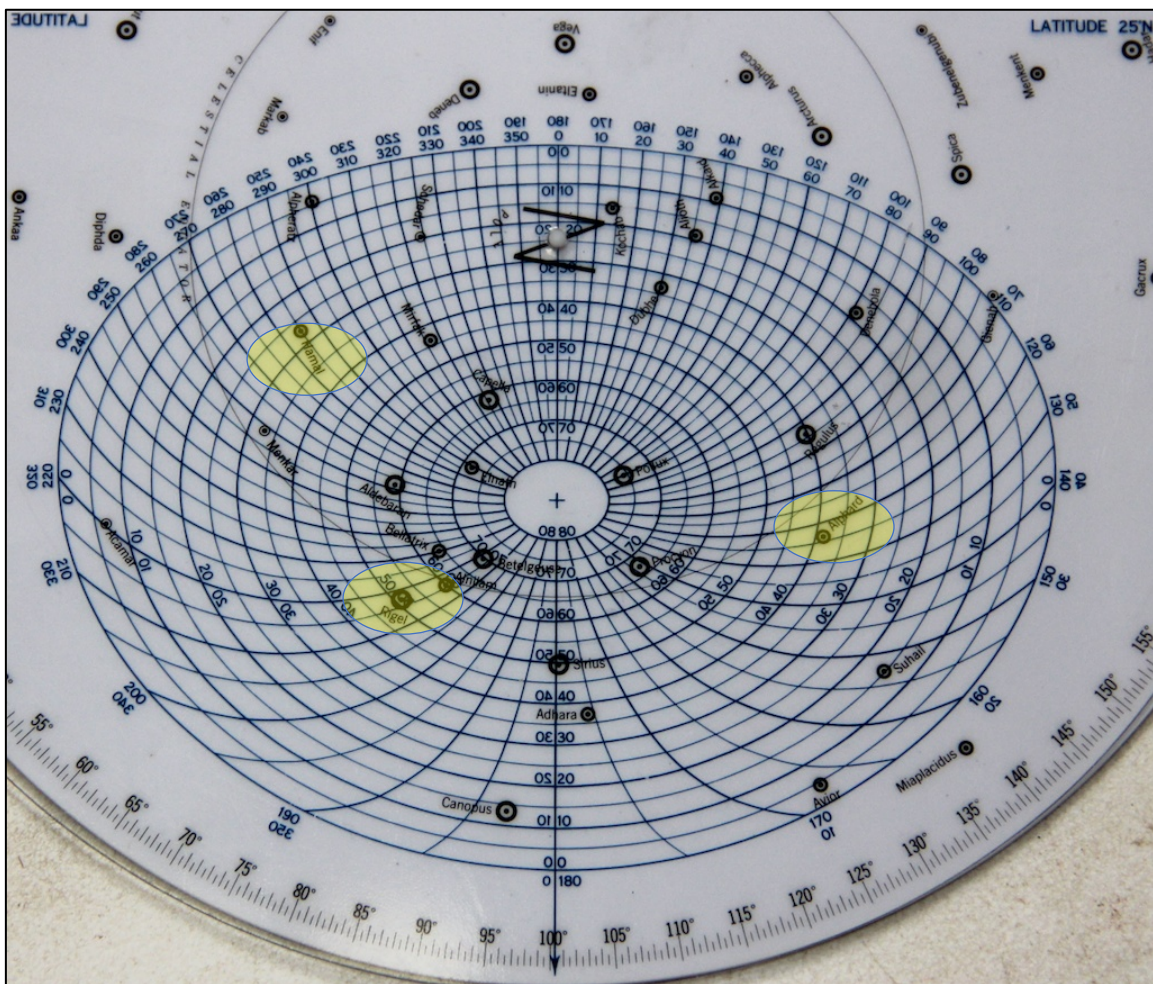
Step 6: Set up the Starfinder.

LHA Aries:  $100^{\circ} 41.1'$

Observer's Latitude (nearest incremental degree):  $25^{\circ}$  N

Step 7: Examine the given stars on the Starfinder and make the best selection.

- Arcturus, Regulus, Sirius: Arcturus is below the horizon.
- Procyon, Sirius, Capella: Capella and Procyon are nearly opposite.
- Hamal, Rigel, Alpherat**: distributed at appropriate azimuths and altitudes.
- Betelgeuse, Dubhe, Regulus: Betelgeuse is too high in the sky and nearly opposite Dubhe.





## Star Selection Problems

SSL D3. On 16 July, your 1920 zone time DR position is latitude  $25^{\circ} 36.0' \text{ N}$ , longitude  $172^{\circ} 18.9' \text{ W}$ . Considering their magnitude, azimuth, and altitude, which group includes the three bodies best suited for a fix at star time?

- a) Rassalhague, Spica, Arcturus
- b) Venus, Antares, Vega- correct
- c) Vega, Mars, Antares
- d) Saturn, Acrux, Spica

Step 1: Determine the approximate time of star time.  
In this problem, no course or speed is given, so you may assume that star time is approximately 1920 ZT.

Step 2: Determine the GMT of the sight.  
Chronometer: 1920 ZT  
DR Longitude:  $172^{\circ} 18.9' \text{ W}$  corresponds to (+11 ZD)  
GMT of sight: 0620 GMT, 17 July

| <sup>m</sup><br>20 | SUN<br>PLANETS | ARIES  |
|--------------------|----------------|--------|
| <sup>s</sup><br>00 | 5 00.0         | 5 00.8 |
| 01                 | 5 00.3         | 5 01.1 |
| 02                 | 5 00.5         | 5 01.3 |
| 03                 | 5 00.8         | 5 01.6 |
| 04                 | 5 01.0         | 5 01.8 |

Step 3: Determine the GHA of Aries for the time of the sight.  
GHA Aries (hours):  $24^{\circ} 58.5'$   
GHA Aries (increment):  $5^{\circ} 00.8'$   
GHA Aries (Total):  $24^{\circ} 58.5' + 5^{\circ} 00.8' = 29^{\circ} 59.3'$

Step 4: Determine the LHA of Aries for the time of the sight.  
GHA Aries:  $29^{\circ} 59.3'$   
DR Longitude:  $172^{\circ} 18.9' \text{ W}$  (W longitude subtract, E longitude add)  
LHA Aries:  $29^{\circ} 59.3' (+360^{\circ}) - 172^{\circ} 18.9' \text{ W} = \underline{217^{\circ} 40.4'}$

Step 5: Determine the SHA, Right Ascension and Declination of each planet listed.

Venus:

SHA =  $217^{\circ} 26.2'$   
RA =  $360^{\circ} - 217^{\circ} 26.2' = \underline{142^{\circ} 33.8'}$   
Declination = N  $15^{\circ} 58.9'$

Mars:

SHA =  $271^{\circ} 45.4'$   
RA =  $360 - 271^{\circ} 45.4 = \underline{88^{\circ} 14.6'}$   
Declination = N  $23^{\circ} 54.4'$

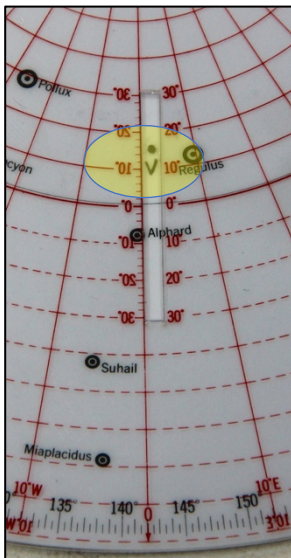
Saturn:

SHA =  $175^{\circ} 03.9'$   
RA =  $360^{\circ} - 175^{\circ} 03.9 = \underline{184^{\circ} 56.1'}$   
Declination = N  $0^{\circ} 23.2'$

# Star Selection Problems

| G.M.T.     | ARIES      | VENUS -3.3 |               | MARS +1.7 |             | JUPITER -1.5 |             | SATURN +1.2 |             |             |                   |
|------------|------------|------------|---------------|-----------|-------------|--------------|-------------|-------------|-------------|-------------|-------------------|
|            | G.H.A.     | G.H.A.     | Dec.          | G.H.A.    | Dec.        | G.H.A.       | Dec.        | G.H.A.      | Dec.        |             |                   |
| 17 00      | 294 43.8   | 150 58.3   | N16 05.2      | 205 44.6  | N23 54.2    | 110 36.8     | S 0 25.8    | 109 44.1    | N 0 23.7    | Mirfak      | 309 15.5 N49 47.5 |
| 01         | 309 46.2   | 165 57.8   | 04.2          | 220 45.3  | 54.3        | 125 39.0     | 25.9        | 124 46.4    | 23.6        | Nunki       | 76 28.1 S26 19.2  |
| 02         | 324 48.7   | 180 57.3   | 03.2          | 235 45.9  | 54.3        | 140 41.2     | 26.0        | 139 48.8    | 23.5        | Peacock     | 53 56.9 S56 47.6  |
| 03         | 339 51.1   | 195 56.8   | 02.3          | 250 46.5  | 54.3        | 155 43.3     | 26.2        | 154 51.1    | 23.4        | Pollux      | 243 57.9 N28 04.3 |
| 04         | 354 53.6   | 210 56.2   | 01.3          | 265 47.1  | 54.4        | 170 45.5     | 26.3        | 169 53.4    | 23.4        | Procyon     | 245 25.5 N 5 16.4 |
| 05         | 9 56.1     | 225 55.7   | 16 00.3       | 280 47.7  | 54.4        | 185 47.7     | 26.5        | 184 55.7    | 23.3        |             |                   |
| 06         | 24 58.5    | 240 55.2   | N15 59.3      | 295 48.3  | N23 54.4    | 200 49.8     | S 0 26.6    | 199 58.0    | N 0 23.2    | Rasalhague  | 96 28.8 N12 34.5  |
| 07         | 40 01.0    | 255 54.7   | 58.3          | 310 48.9  | 54.5        | 215 52.0     | 26.7        | 215 00.3    | 23.1        | Regulus     | 208 09.7 N12 03.6 |
| 08         | 55 03.5    | 270 54.2   | 57.3          | 325 49.5  | 54.5        | 230 54.2     | 26.9        | 230 02.7    | 23.1        | Rigel       | 281 35.7 S 8 13.4 |
| F 09       | 70 05.9    | 285 53.7   | 56.3          | 340 50.2  | 54.6        | 245 56.3     | 27.0        | 245 05.0    | 23.0        | Rigel Kent. | 140 24.8 S60 45.6 |
| R 10       | 85 08.4    | 300 53.2   | 55.3          | 355 50.8  | 54.6        | 260 58.5     | 27.1        | 260 07.3    | 22.9        | Sabik       | 102 40.2 S15 42.1 |
| I 11       | 100 10.9   | 315 52.7   | 54.3          | 10 51.4   | 54.6        | 276 00.7     | 27.3        | 275 09.6    | 22.8        |             |                   |
| D 12       | 115 13.3   | 330 52.2   | N15 53.4      | 25 52.0   | N23 54.7    | 291 02.8     | S 0 27.4    | 290 11.9    | N 0 22.8    | Schedar     | 350 08.2 N56 25.8 |
| A 13       | 130 15.8   | 345 51.7   | 52.4          | 40 52.6   | 54.7        | 306 05.0     | 27.6        | 305 14.2    | 22.7        | Shaula      | 96 54.6 S37 05.4  |
| Y 14       | 145 18.2   | 0 51.2     | 51.4          | 55 53.2   | 54.7        | 321 07.2     | 27.7        | 320 16.5    | 22.6        | Sirius      | 258 55.5 S16 41.4 |
| 15         | 160 20.7   | 15 50.6    | 50.4          | 70 53.8   | 54.8        | 336 09.3     | 27.8        | 335 18.9    | 22.6        | Spica       | 158 56.9 S11 03.8 |
| 16         | 175 23.2   | 30 50.1    | 49.4          | 85 54.5   | 54.8        | 351 11.5     | 28.0        | 350 21.2    | 22.5        | Suhail      | 223 10.8 S43 21.5 |
| 17         | 190 25.6   | 45 49.6    | 48.4          | 100 55.1  | 54.8        | 6 13.6       | 28.1        | 5 23.5      | 22.4        |             |                   |
| 18         | 205 28.1   | 60 49.1    | N15 47.4      | 115 55.7  | N23 54.9    | 21 15.8      | S 0 28.3    | 20 25.8     | N 0 22.3    | Vega        | 80 55.0 N38 46.1  |
| 19         | 220 30.6   | 75 48.6    | 46.4          | 130 56.3  | 54.9        | 36 18.0      | 28.4        | 35 28.1     | 22.3        | Zuben'ubi   | 137 32.3 S15 57.9 |
| 20         | 235 33.0   | 90 48.1    | 45.4          | 145 56.9  | 54.9        | 51 20.1      | 28.5        | 50 30.4     | 22.2        |             | S.H.A. Mer. Pass. |
| 21         | 250 35.5   | 105 47.6   | 44.4          | 160 57.5  | 54.9        | 66 22.3      | 28.7        | 65 32.7     | 22.1        |             | h m               |
| 22         | 265 38.0   | 120 47.1   | 43.4          | 175 58.1  | 55.0        | 81 24.5      | 28.8        | 80 35.1     | 22.0        | Venus       | 217 26.2 13 56    |
| 23         | 280 40.4   | 135 46.6   | 42.4          | 190 58.8  | 55.0        | 96 26.6      | 28.9        | 95 37.4     | 22.0        | Mars        | 271 45.4 10 18    |
|            |            |            |               |           |             |              |             |             |             | Jupiter     | 176 00.1 16 39    |
|            |            |            |               |           |             |              |             |             |             | Saturn      | 175 03.9 16 42    |
| Mer. Pass. | h m 4 24.3 |            | i' -0.5 d 1.0 |           | v 0.6 d 0.0 |              | v 2.2 d 0.1 |             | v 2.3 d 0.1 |             |                   |

Step 6: Plot the planets on the Starfinder using the planet disk.



## Star Selection Problems

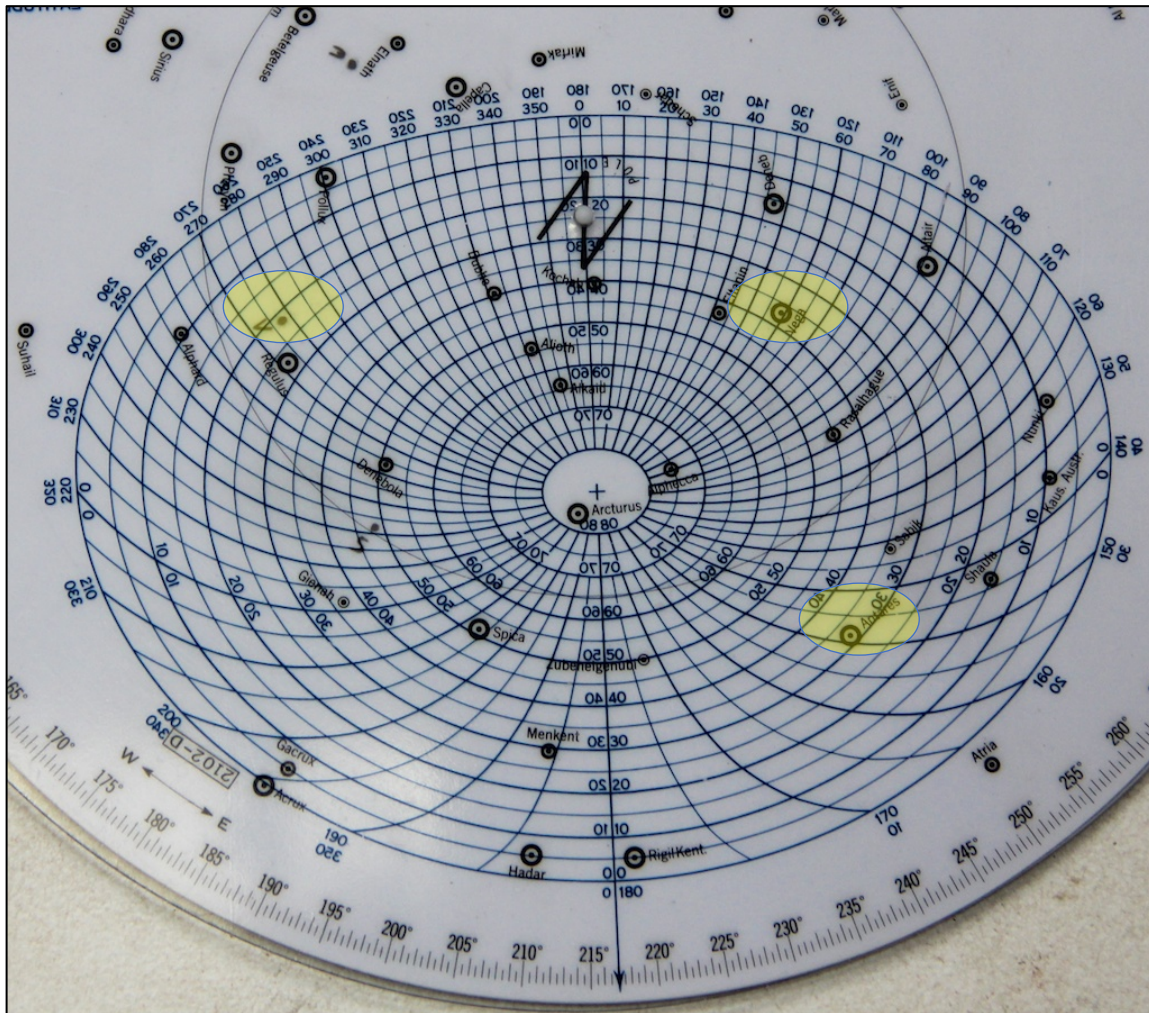
Step 7: Set up the Starfinder.

LHA Aries:  $217^{\circ} 40.4'$

Observer's latitude (nearest incremental degree):  $25^{\circ}$  N

Step 8: Use the Starfinder to make the best selection.

- Rassalhague, Spica, Arcturus: Arcturus is too high in the sky.
- Venus, Antares, Vega**: distributed at appropriate altitudes and azimuths.
- Vega, Mars, Antares: Mars is below the horizon.
- Saturn, Acrux, Spica: Acrux is below the horizon.



## Star Selection Problems

### Star Selection Problems

SSL B1. On 20 June, your 1742 zone time DR position is latitude  $24^{\circ} 55.0'$  S, longitude  $8^{\circ} 19.6'$  E. Considering their magnitude, azimuth, and altitude, which three stars are best suited for a fix at star time?

- a) **Regulus, Canopus, Antares - correct**
- b) Spica, Arcturus, Alioth
- c) Arcturus, Achernar, Pollux
- d) Avoir, Sabik, Formalhaut

SSL B2. On 24 July your 1912 zone time DR position is latitude  $24^{\circ} 28.0'$  N, longitude  $73^{\circ} 46.5'$  W. Considering their magnitude, azimuth, and altitude, which group includes the three stars best suited for a fix at star time?

- a) Fomalhaut, Rigel, Pollux
- b) Arcturus, Acrux, Hadar
- c) **Spica, Altair, Alioth - correct**
- d) Vega, Deneb, Regulus

SSL B3. On 4 September, your 1813 zone time DR position is latitude  $24^{\circ} 18.0'$  S, longitude  $95^{\circ} 16'$  E. Considering their magnitude, azimuth, and altitude, which group includes the three stars best suited for a fix at star time?

- a) Enif, Miaplacidus, Alkaid
- b) Betelgeuse, Acrux, Hamal
- c) **Rasalhague, Fomalhaut, Spica - correct**
- d) Deneb, Altair, Vega

SSL B4. On 28 October, morning twilight will occur around 0524 ZT in position latitude  $25^{\circ} 25'$  N, longitude  $32^{\circ} 33.3'$  W. Which group will be the three best stars to observe for a star fix at star time?

- a) Sirius, Hamal, Denebola
- b) Sirius, Denebola, Dubhe
- c) **Sirius, Capella, Denebola - correct**
- d) Sirius, Mirfak, Hamal



### Star Selection Problems with Planets/Moon

SSL B5. On 11 November, your 0200 zone time DR position is latitude  $26^{\circ} 32'$  S, longitude  $154^{\circ} 16'$  E. You are on course  $058^{\circ}$  T at a speed of 21 knots. Considering their magnitude, azimuth, and altitude, which group includes the three bodies best suited for a fix at star time?

- a) Polaris, Regulus, Rigel
- b) Jupiter, Spica, Canopus
- c) Saturn, Peacock, Rigel
- d) **Mars, Betelgeuse, Miaplacidus - correct**

SSL B6. On 17 July your 1951 zone time DR position is latitude  $24^{\circ} 26.0'$  N, longitude  $51^{\circ} 16.0'$  W. Considering their magnitude, azimuth, and altitude, which group includes the three bodies best suited for a fix at star time?

- a) Hadar, Deneb, Alpheratz
- b) Regulus, Venus, Antares
- c) Mars, Vega, Dubhe
- d) **Kochab, Jupiter, Rasalhague - correct**

SSL B7. On 2 February your 0400 zone time DR position is latitude  $24^{\circ} 14.0'$  N, longitude  $163^{\circ} 28.0'$  W. You are on course  $322^{\circ}$  T at a speed of 22 knots. Considering their magnitude, azimuth, and altitude, which group includes the three bodies best suited for a fix at star time?

- a) **Saturn, Antares, Rasalhague - correct**
- b) Jupiter, Saturn, Polaris
- c) Saturn, Polaris, Zubenelgenubi
- d) Jupiter, Spica, Denebola

SSL B8. On 29 April your 0300 zone time DR position is latitude  $28^{\circ} 39'$  N, longitude  $168^{\circ} 03'$  E. You are on course  $108^{\circ}$  T at a speed of 22 knots. Considering their magnitude, azimuth, and altitude, which group includes the three bodies best suited for a fix at star time?

- a) **Moon, Alpheratz, Polaris - correct**
- b) Deneb, Dubhe, Zubenelgenubi
- c) Venus, Polaris, Arcturus
- d) Moon, Altair, Sabik



## **Sight Reduction (Individual) Problems**





## Sight Reduction Individual Problems

- For more details on any portion of these sights, see the applicable sections such as mid-latitude sailings, sextant basics, or refer to Bowditch's glossary.
- Apparent Altitude Correction is also termed "Main Correction" in this text.

### Sextant Correction (Hs to Ho) Problems

RED D1. On 4 July you observe the lower limb of the Sun at a sextant altitude (hs) of  $25^{\circ} 29.8'$ . The index error is  $3.1'$  off the arc. The height of eye is 48 feet. What is the observed altitude (ho)?

Answer:  $25^{\circ} 40.2'$ .

Step 1: Determine the sextant altitude (hs).  
hs =  $25^{\circ} 29.8'$  (Given)

Step 2: Determine the index correction (IC).  
Index error:  $3.1'$  off the arc.  
Index correction:  $+3.1'$

Step 3: Determine the dip correction.  
Height of eye: 48 feet.  
Dip correction:  $-6.7'$

Step 4: Determine the apparent altitude (ha).  
Apparent altitude (ha) = hs  $\pm$  IC  $\pm$  dip  
ha =  $25^{\circ} 29.8' + 3.1' - 6.7' = \underline{25^{\circ} 26.2'}$

Step 5: Determine the main correction.  
ha =  $25^{\circ} 26.2'$   
MC =  $+14.0'$

Step 6: Determine the observed altitude (ho).  
Observed altitude = ha  $\pm$  MC  
Observed altitude =  $25^{\circ} 26.2' + 14.0' = \underline{25^{\circ} 40.2'}$

| DIP           |                   |               |                                 |
|---------------|-------------------|---------------|---------------------------------|
| Ht. of<br>Eye | Corr <sup>n</sup> | Ht. of<br>Eye | Ht. of<br>Eye Corr <sup>n</sup> |
| 13.8          | -6.6              | 45.5          | 85 - 8.9                        |
| 14.2          | -6.7              | 46.9          | 90 - 9.2                        |
| 14.7          | -6.8              | 48.4          | 95 - 9.5                        |
| 15.1          | -6.8              | 49.8          |                                 |

| OCT.—MAR. SUN |               |               | APR.—SEPT.   |               |               |
|---------------|---------------|---------------|--------------|---------------|---------------|
| App.<br>Alt.  | Lower<br>Limb | Upper<br>Limb | App.<br>Alt. | Lower<br>Limb | Upper<br>Limb |
| 23 42         | +14.1         | -18.2         | 23 51        | +13.9         | -17.9         |
| 24 21         | +14.2         | -18.1         | 24 53        | +14.0         | -17.8         |
| 25 26         | +14.3         | -18.0         | 26 00        | +14.1         | -17.7         |
| 26 36         | +14.4         | -17.9         | 27 13        | +14.2         | -17.6         |

## Sight Reduction Individual Problems

RED D2. During evening twilight on 28 December, a sextant altitude (hs) of the planet Venus was  $29^{\circ} 43.2'$ . The height of eye was 40 feet and the index error was  $2.0'$  on the arc. What was the observed altitude?

Answer:  $29^{\circ} 34.1'$ .

- Step 1: Determine the sextant altitude (hs).  
hs =  $29^{\circ} 43.2'$  (Given)
- Step 2: Determine the index correction (IC).  
Index error:  $2.0'$  on the arc.  
Index correction:  $-2.0'$
- Step 3: Determine the dip correction.  
Height of eye: 40 feet.  
Dip correction:  $-6.1'$
- Step 4: Determine the apparent altitude (ha).  
Apparent altitude (ha) = hs  $\pm$  IC  $\pm$  dip  
ha =  $29^{\circ} 43.2' - 2.0' - 6.1' = \underline{29^{\circ} 35.1'}$
- Step 5: Determine the main correction.  
ha =  $29^{\circ} 35.1'$   
MC (stars and planets):  $-1.7'$   
Additional Venus correction:  $+0.7'$   
MC =  $-1.7' + 0.7' = -1.0'$
- Step 6: Determine the observed altitude (ho).  
Observed altitude = ha  $\pm$  MC  
Observed altitude =  $29^{\circ} 35.1' - 1.0' = \underline{29^{\circ} 34.1'}$

| DIP        |                   |            |            |                   |  |
|------------|-------------------|------------|------------|-------------------|--|
| Ht. of Eye | Corr <sup>n</sup> | Ht. of Eye | Ht. of Eye | Corr <sup>n</sup> |  |
| 11.8       | 6.0               | 38.9       | ←          |                   |  |
| 12.2       | 6.1               | 40.1       |            |                   |  |
| 12.6       | 6.2               | 41.5       | 70         | 8.1               |  |
| 13.0       | 6.3               | 42.8       | 75         | 8.4               |  |
|            | 6.4               |            |            |                   |  |

| STARS AND PLANETS |                   |           |                              |
|-------------------|-------------------|-----------|------------------------------|
| App. Alt.         | Corr <sup>n</sup> | App. Alt. | Additional Corr <sup>n</sup> |
| <b>1981</b>       |                   |           |                              |
| <b>VENUS</b>      |                   |           |                              |
| Jan. 1-Sept. 27   |                   |           |                              |
| 9 56              | 5.3               | 0         | 0.1                          |
| 10 08             | 5.2               | 42        | 0.1                          |
| 10 20             | 5.1               |           |                              |
| 10 33             | 5.0               |           |                              |
| 10 46             | 4.9               |           |                              |
| 11 00             | 4.8               |           |                              |
| 11 14             | 4.7               |           |                              |
| 11 29             | 4.6               |           |                              |
| 11 45             | 4.5               |           |                              |
| 12 01             | 4.4               |           |                              |
| 12 18             | 4.3               |           |                              |
| 12 35             | 4.2               |           |                              |
| 12 54             | 4.1               |           |                              |
| 13 13             | 4.0               |           |                              |
| 13 33             | 3.9               |           |                              |
| 13 54             | 3.8               |           |                              |
| 14 16             | 3.7               |           |                              |
| 14 40             | 3.6               |           |                              |
| 15 04             | 3.5               |           |                              |
| 15 30             | 3.4               |           |                              |
| 15 57             | 3.3               |           |                              |
| 16 26             | 3.2               |           |                              |
| 16 56             | 3.1               |           |                              |
| 17 28             | 3.0               |           |                              |
| 18 02             | 2.9               |           |                              |
| 18 38             | 2.8               |           |                              |
| 19 17             | 2.7               |           |                              |
| 19 58             | 2.6               |           |                              |
| 20 42             | 2.5               |           |                              |
| 21 28             | 2.4               |           |                              |
| 22 19             | 2.3               |           |                              |
| 23 13             | 2.2               |           |                              |
| 24 11             | 2.1               |           |                              |
| 25 14             | 2.0               |           |                              |
| 26 22             | 1.9               |           |                              |
| 27 36             | 1.8               |           |                              |
| 28 56             | 1.7               |           |                              |
| 30 24             | 1.6               |           |                              |
| 32 00             | 1.5               |           |                              |
| <b>MARS</b>       |                   |           |                              |
| Jan. 1-Dec. 31    |                   |           |                              |
|                   |                   | 0         | 0.1                          |
|                   |                   | 60        | 0.1                          |

## Sight Reduction Individual Problems

RED D3. On 25 December you observe the Sun's lower limb. The sextant altitude (hs) is  $4^{\circ} 06.9'$ . The height of eye is 47 feet and the index error is  $1.6'$  on the arc. The temperature is  $19^{\circ} \text{F}$  and the barometer reads 1030.8 millibars. What is the observed altitude?

Answer:  $4^{\circ} 01.9'$ .

Step 1: Determine the sextant altitude (hs).  
hs =  $4^{\circ} 06.9'$  (Given)

Step 2: Determine the index correction (IC).  
Index error:  $1.6'$  on the arc.  
Index correction:  $-1.6'$

| DIP        |                   |            |
|------------|-------------------|------------|
| Ht. of Eye | Corr <sup>n</sup> | Ht. of Eye |
| 13.8       | -6.5              | 45.5       |
| 14.2       | -6.6              | 46.9       |
| 14.7       | -6.7              | 48.4       |
| 15.1       | -6.8              | 49.8       |

Step 3: Determine the dip correction.  
Height of eye: 47 feet.  
Dip correction:  $-6.7'$

Step 4: Determine the apparent altitude (ha).  
Apparent altitude (ha) = hs  $\pm$  IC  $\pm$  dip  
ha =  $4^{\circ} 06.9' - 1.6' - 6.7' = 3^{\circ} 58.6'$

| App. Alt. | OCT.-MAR. SUN APP.-SEPT. |            |            |            |
|-----------|--------------------------|------------|------------|------------|
|           | Lower Limb               | Upper Limb | Lower Limb | Upper Limb |
| 3 30      | + 3.3                    | -29.0      | + 3.1      | -28.7      |
| 3 35      | 3.6                      | 28.7       | 3.3        | 28.5       |
| 4 0       | 3.8                      | 28.5       | 3.5        | 28.3       |
| 4 5       | 4.0                      | 28.3       | 3.7        | 28.1       |
| 5 0       | 4.2                      | 28.1       | 3.9        | 27.9       |
| 3 55      | 4.4                      | 27.9       | 4.1        | 27.7       |
| 4 00      | + 4.5                    | -27.8      | + 4.3      | -27.5      |
| 0 5       | 4.7                      | 27.6       | 4.5        | 27.3       |
| 1 0       | 4.9                      | 27.4       | 4.6        | 27.2       |
| 1 5       | 5.1                      | 27.2       | 4.8        | 27.0       |
| 2 0       | 5.2                      | 27.1       | 5.0        | 26.8       |
| 2 5       | 5.4                      | 26.9       | 5.1        | 26.7       |

Step 5: Determine the main correction, using the altitude correction tables for altitudes less than  $10^{\circ}$ .  
ha:  $3^{\circ} 58.6'$   
MC (Sun):  $+4.5'$

Step 6: Determine the additional correction for non-standard conditions.  
Temperature:  $19^{\circ} \text{F}$   
Barometer: 1030.8mb  
Additional correction category: C  
Apparent altitude :  $3^{\circ} 58.6'$   
Additional correction:  $-1.2'$

| A4 ALTITUDE CORRECTION TABLE<br>ADDITIONAL REFRACTION CORRECTION                                                            |      |      |      |      |      |      |
|-----------------------------------------------------------------------------------------------------------------------------|------|------|------|------|------|------|
| <div> <div> -20° F. -10° 0° +10° 20° </div> <div> -30° C. -20° -10° 0° +10° 20° </div> </div>                               |      |      |      |      |      |      |
| <div> <div>Pressure in millibars</div> <div>1050</div> <div>1030</div> <div>1010</div> <div>990</div> <div>970</div> </div> |      |      |      |      |      |      |
| App. Alt.                                                                                                                   | A    | B    | C    | D    | E    | F    |
| 0 00                                                                                                                        | -6.9 | -5.7 | -4.6 | -3.4 | -2.3 | -1.1 |
| 0 30                                                                                                                        | 5.2  | 4.4  | 3.5  | 2.6  | 1.7  | 0.9  |
| 1 00                                                                                                                        | 4.3  | 3.5  | 2.8  | 2.1  | 1.4  | 0.7  |
| 1 30                                                                                                                        | 3.5  | 2.9  | 2.4  | 1.8  | 1.2  | 0.6  |
| 2 00                                                                                                                        | 3.0  | 2.5  | 2.0  | 1.5  | 1.0  | 0.5  |
| 2 30                                                                                                                        | -2.5 | -2.1 | -1.6 | -1.2 | -0.8 | -0.4 |
| 3 00                                                                                                                        | -2.2 | -1.8 | -1.5 | -1.1 | -0.7 | -0.4 |
| 3 30                                                                                                                        | -2.0 | -1.6 | -1.3 | -1.0 | -0.7 | -0.3 |
| 4 00                                                                                                                        | -1.8 | -1.5 | -1.2 | -0.9 | -0.6 | -0.3 |
| 4 30                                                                                                                        | -1.6 | -1.4 | -1.1 | -0.8 | -0.5 | -0.3 |

Step 7: Determine the observed altitude (ho).  
Observed altitude = ha  $\pm$  MC  $\pm$  Additional Correction  
Observed altitude =  $3^{\circ} 58.6' + 4.5' - 1.2' = 4^{\circ} 01.9'$

## Sight Reduction Individual Problems

RED D4. In the Bay of Fundy, during twilight, you take a sight of Mars. The sextant altitude (hs) is  $3^{\circ} 35.5'$ . Your height of eye is 32 feet and there is no index error. The air temperature is  $-10^{\circ}$  C and the barometer reads 1010 millibars. What is the observed altitude (ho)?

Answer:  $03^{\circ} 15.7'$ .

Step 1: Determine the sextant altitude (hs).  
hs =  $3^{\circ} 35.5'$  (Given)

Step 2: Determine the index correction (IC).  
Index error: none  
Index correction:  $0.0'$

Step 3: Determine the dip correction.  
Height of eye: 32 feet.  
Dip correction:  $-5.5'$

| DIP        |                   |            |
|------------|-------------------|------------|
| Ht. of Eye | Corr <sup>n</sup> | Ht. of Eye |
| 9.2        | -5.4              | 30.4       |
| 9.5        | -5.5              | 31.5       |
| 9.9        | -5.6              | 32.7       |
| 10.3       | -5.7              | 33.9       |
| 10.6       | -5.7              | 35.1       |

Step 4: Determine the apparent altitude (ha).  
Apparent altitude (ha) = hs  $\pm$  IC  $\pm$  dip  
ha =  $3^{\circ} 35.5' - 0.0' - 5.5' = \underline{3^{\circ} 30.0'}$

| App. Alt. | OCT.-MAR. SUN |            | APR.-SEPT. |            | STARS PLANETS |
|-----------|---------------|------------|------------|------------|---------------|
|           | Lower Limb    | Upper Limb | Lower Limb | Upper Limb |               |
| 0         | +3.3          | -29.0      | +3.1       | -28.7      | -13.0         |
| 30        | 3.6           | 28.7       | 3.3        | 28.5       | 12.7          |
| 40        | 3.8           | 28.5       | 3.5        | 28.3       | 12.5          |
| 45        | 4.0           | 28.3       | 3.7        | 28.1       | 12.3          |
| 50        | 4.2           | 28.1       | 3.9        | 27.9       | 12.1          |
| 55        | 4.4           | 27.9       | 4.1        | 27.7       | 11.9          |

Step 5: Determine the main correction, using the altitude correction tables for planet altitudes less than  $10^{\circ}$ .  
ha:  $3^{\circ} 30.0'$   
MC (Planets):  $\underline{-13.0'}$

Step 6: Determine the additional correction for non-standard conditions.  
Temperature:  $10^{\circ}$  C  
Barometer: 1010mb  
Additional correction category: C  
Apparent altitude:  $3^{\circ} 30.0'$   
Additional correction:  $\underline{-1.3'}$

Step 7: Determine the observed altitude (ho).  
Observed altitude = ha  $\pm$  MC  $\pm$  Additional Correction  
Observed altitude =  $3^{\circ} 30.0' - 13.0' - 1.3' = \underline{3^{\circ} 15.7'}$

| A4 ALTITUDE CORRECTION                                                                                                                                                                                     |      |      |      |      |      |
|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------|------|------|------|------|
| ADDITIONAL REFRACTION CORRECTION                                                                                                                                                                           |      |      |      |      |      |
| <div style="display: flex; justify-content: space-between;"> <span>-20° F. -10° 0° +10° 2</span> </div> <div style="display: flex; justify-content: space-between;"> <span>-30° C. -20° -10°</span> </div> |      |      |      |      |      |
| App. Alt.                                                                                                                                                                                                  | A    | B    | C    | D    | E    |
| 0 00                                                                                                                                                                                                       | -6.9 | -5.7 | -4.6 | -3.4 | -2.3 |
| 0 30                                                                                                                                                                                                       | 5.2  | 4.4  | 3.5  | 2.6  | 1.7  |
| 1 00                                                                                                                                                                                                       | 4.3  | 3.5  | 2.8  | 2.1  | 1.4  |
| 1 30                                                                                                                                                                                                       | 3.5  | 2.9  | 2.4  | 1.8  | 1.2  |
| 2 00                                                                                                                                                                                                       | 3.0  | 2.5  | 2.0  | 1.5  | 1.0  |
| 2 30                                                                                                                                                                                                       | 2.5  | 2.1  | 1.6  | 1.2  | 0.8  |
| 3 00                                                                                                                                                                                                       | 2.2  | 1.8  | 1.5  | 1.1  | 0.7  |
| 3 30                                                                                                                                                                                                       | 2.0  | 1.6  | 1.3  | 1.0  | 0.7  |
| 4 00                                                                                                                                                                                                       | 1.8  | 1.5  | 1.2  | 0.9  | 0.6  |
| 4 30                                                                                                                                                                                                       | 1.6  | 1.4  | 1.1  | 0.8  | 0.5  |

## Sight Reduction Individual Problems

### Sight Reduction of the Sun Problems

RED D5. On 10 January at 0550 zone time, morning stars were observed, and the vessels position was determined to be latitude  $25^{\circ} 16' \text{ N}$ , longitude  $123^{\circ} 18' \text{ W}$ . Your vessel is steaming at 22 knots on a course of  $295^{\circ} \text{ T}$ . A sextant observation of the Sun's lower limb is made at 0915 zone time. The chronometer reads 05h 14m 02s and the sextant altitude is  $24^{\circ} 00.7'$ . The index error is  $2.6'$  off the arc, and the chronometer error is 01m 34s slow. Your height of eye on the bridge is 55 feet. What is the azimuth (zn) and computed altitude (hc) of this sight?

Answer: zn =  $131.4^{\circ} \text{ T}$ , hc =  $23^{\circ} 14.4'$ .

Step 1: Determine the DR position of the ship for the time of the sight by mid-latitude sailing.

a. Perform preliminary calculations.

0550 fix position:  $25^{\circ} 16' \text{ N}$ ,  $123^{\circ} 18' \text{ W}$

Course/Speed:  $295^{\circ} \text{ T}$ , 22 knots

Morning Sun sight: 0915

0550 to 0915 = 3 hours 25 minutes = 3.42 hours

3.42 hours at 22 knots =  $D = 75.24$  miles covered.

b. Determine the difference in latitude ( $l$ ).

$$l = D \cos C$$

$$l = (75.24) \cos (295^{\circ})$$

$$l = (75.24) (0.4226)$$

$$l = 31.796 = 0.5299^{\circ}$$

c. Determine the mid-latitude ( $Lm$ ) and the 0915 DR latitude position.

Latitude 1 =  $25^{\circ} 16' \text{ N} = 25.266^{\circ} \text{ N}$

$l = 31.796' = 0.5299^{\circ}$  (to the north)

Latitude 2 =  $25.266^{\circ} \text{ N} + 0.5299^{\circ} = 25.796^{\circ} \text{ N} = \underline{25^{\circ} 47.8' \text{ N}}$

$$Lm = \frac{25.266^{\circ} + 25.796^{\circ}}{2} = 25.531^{\circ} \text{ N}$$

d. Determine the departure ( $p$ ).

$$p = D \sin C$$

$$p = (75.24) \sin 295^{\circ}$$

$$p = (75.24) (-0.9063)$$

$$p = -68.190$$

## Sight Reduction Individual Problems

- e. Determine the difference in longitude (*DLo*) and the 0915 DR longitude position.

$$DLo = \frac{p}{\cos Lm}$$

$$DLo = \frac{-68.190}{\cos(25.531)}$$

$$DLo = \frac{-68.190}{0.9024}$$

$$DLo = -75.57' = 1.260^\circ \text{ (to the west)}$$

$$\text{Longitude 1} = 123^\circ 18' \text{ W} = 123.300^\circ \text{ W}$$

$$\text{Longitude 2} = 123.300^\circ \text{ W} + 1.260^\circ = 124.560^\circ \text{ W} = \underline{124^\circ 33.6' \text{ W}}$$

0915 DR position:  $25^\circ 47.8' \text{ N}$ ,  $124^\circ 33.6' \text{ W}$

- Step 2: Determine the GMT of the sight.  
 Chronometer time: 05h 14m 02s  
 Chronometer error: 01m 34s slow  
 Correct chronometer time: 05h 15m 36s  
 Ship time of sight: 0915 zone time  
 DR Longitude:  $124^\circ 33.6' \text{ W}$  corresponds to (+8 ZD).  
 GMT of sight: 17:15:36, 10 January

- Step 3: Given the sextant altitude (*hs*), index error and height of eye, determine the apparent altitude (*ha*).  
*hs*:  $24^\circ 00.7'$  (Given)  
 Index error (Index correction):  $2.6'$  off the arc (+ $2.6'$  correction)  
 Height of eye (dip correction): 55 feet ( $-7.2'$  correction)  
 Apparent altitude (*ha*):  $24^\circ 00.7' + 2.6' - 7.2' = 23^\circ 56.1'$

- Step 4: Determine the observed altitude.  
 Apparent altitude (*ha*):  $23^\circ 56.1'$   
 Main correction:  $+14.1'$   
 Observed altitude (*ho*):  $23^\circ 56.1' + 14.1' = \underline{24^\circ 10.2'}$

- Step 5: Determine the declination of the Sun for the time of sight.  
 Declination (hours):  $S 21^\circ 53.6'$  (d number = 0.4')  
 Declination (increments):  $-0.1'$   
 Declination (total):  $S 21^\circ 53.6' - 0.1' = \underline{S 21^\circ 53.5'}$

- Step 6: Determine the GHA of the Sun for the time of sight.  
 GHA (hours):  $73^\circ 04.5'$   
 GHA (increment):  $3^\circ 54.0'$   
 GHA (total):  $73^\circ 04.5' + 3^\circ 54.0' = \underline{76^\circ 58.5'}$

| m  | SUN<br>PLANETS | ARIES  | MOON   | $\frac{v}{d}$<br>or Corr <sup>n</sup> |
|----|----------------|--------|--------|---------------------------------------|
| 32 | 3 53-0         | 3 53-6 | 3 42-4 | 3-2 0-8                               |
| 33 | 3 53-3         | 3 53-9 | 3 42-6 | 3-3 0-9                               |
| 34 | 3 53-5         | 3 54-1 | 3 42-9 | 3-4 0-9                               |
| 35 | 3 53-8         | 3 54-4 | 3 43-1 | 3-5 0-9                               |
| 36 | 3 54-0         | 3 54-6 | 3 43-3 | 3-6 0-9                               |
| 37 | 3 54-3         | 3 54-9 | 3 43-6 | 3-7 1-0                               |
| 38 | 3 54-5         | 3 55-1 | 3 43-8 | 3-8 1-0                               |
| 39 | 3 54-8         | 3 55-4 | 3 44-1 | 3-9 1-0                               |
| 40 | 3 55-0         | 3 55-6 | 3 44-3 | 4-0 1-0                               |

| G.M.T.                    | SUN          |              |              |              |
|---------------------------|--------------|--------------|--------------|--------------|
|                           | G.H.A.       |              | Dec.         |              |
| <sup>d</sup> <sup>h</sup> | <sup>°</sup> | <sup>'</sup> | <sup>°</sup> | <sup>'</sup> |
| 10 00                     | 178          | 08.8         | S21          | 59.9         |
| 01                        | 193          | 08.5         |              | 59.6         |
| 02                        | 208          | 08.3         |              | 59.2         |
| 03                        | 223          | 08.0         | ..           | 58.8         |
| 04                        | 238          | 07.8         |              | 58.5         |
| 05                        | 253          | 07.5         |              | 58.1         |
| 06                        | 268          | 07.2         | S21          | 57.7         |
| 07                        | 283          | 07.0         |              | 57.4         |
| S 08                      | 298          | 06.7         |              | 57.0         |
| A 09                      | 313          | 06.5         | ..           | 56.6         |
| T 10                      | 328          | 06.2         |              | 56.2         |
| U 11                      | 343          | 06.0         |              | 55.9         |
| R 12                      | 358          | 05.7         | S21          | 55.5         |
| D 13                      | 13           | 05.5         |              | 55.1         |
| A 14                      | 28           | 05.2         |              | 54.7         |
| Y 15                      | 43           | 05.0         | ..           | 54.4         |
| 16                        | 58           | 04.7         |              | 54.0         |
| 17                        | 73           | 04.5         |              | 53.6         |
| 18                        | 88           | 04.2         | S21          | 53.2         |
| 19                        | 103          | 04.0         |              | 52.8         |
| 20                        | 118          | 03.7         |              | 52.4         |
| 21                        | 133          | 03.5         | ..           | 52.1         |
| 22                        | 148          | 03.2         |              | 51.7         |
| 23                        | 163          | 03.0         |              | 51.3         |
| 24                        | 178          | 02.8         | S21          | 51.0         |
|                           | S.D.         | 16.3         | d            | 0.4          |

# Sight Reduction Individual Problems

- Step 7: Determine the assumed position (AP) of the ship.  
 DR latitude based on nearest whole latitude: 26° N  
 DR long chosen such that GHA – long. is a whole value: 124° 58.5' W
- Step 8: Determine the LHA of the Sun for the time of sight and AP.  
 GHA (Sun): 76° 58.5'  
 DR Longitude: 124° 58.5' W  
 LHA = 76° 58.5' (+360°) – 124° 58.5' = 312° (subtract west, add east).
- Step 9: Entering publication HO229 with assumed latitude, declination, and LHA,  
 retrieve the computed altitude (hc), altitude difference (d), and azimuth (z) for the  
 assumed position.  
 Assumed latitude: 26° N  
 Declination: S 21°  
 LHA: 312° (Contrary Pages)
- HO 229 values:  
 Computed altitude (hc): 23° 51.1'  
 Altitude difference (d): -41.1'  
 Azimuth (z): 130.7°

| LATITUDE CONTRARY NAME TO DECLINATION |         |       |       |         |       |       |         |       |       |         |       |       | L.H.A. 48°, 312° |       |       |         |       |       |         |       |       |         |       |       |      |
|---------------------------------------|---------|-------|-------|---------|-------|-------|---------|-------|-------|---------|-------|-------|------------------|-------|-------|---------|-------|-------|---------|-------|-------|---------|-------|-------|------|
| Dec.                                  | 23°     |       |       | 24°     |       |       | 25°     |       |       | 26°     |       |       | 27°              |       |       | 28°     |       |       | 29°     |       |       | 30°     |       |       | Dec. |
|                                       | Hc      | d     | Z     | Hc      | d     | Z     | Hc      | d     | Z     | Hc      | d     | Z     | Hc               | d     | Z     | Hc      | d     | Z     | Hc      | d     | Z     | Hc      | d     | Z     |      |
| 0                                     | 38 01.2 | -30.1 | 109.4 | 37 40.9 | -31.1 | 110.1 | 37 19.9 | -32.1 | 110.8 | 36 58.3 | -33.2 | 111.5 | 36 35.9          | -34.2 | 112.2 | 36 12.9 | -35.2 | 112.9 | 35 49.2 | -36.1 | 113.6 | 35 24.9 | -37.1 | 114.2 | 0    |
| 1                                     | 37 31.1 | -30.6 | 110.5 | 37 09.8 | -31.7 | 111.2 | 36 47.8 | -32.8 | 111.9 | 36 25.1 | -33.8 | 112.6 | 36 01.7          | -34.7 | 113.3 | 35 37.7 | -35.7 | 113.9 | 35 13.1 | -36.6 | 114.6 | 34 47.8 | -37.5 | 115.2 | 1    |
| 2                                     | 37 00.5 | -31.3 | 111.6 | 36 38.1 | -32.3 | 112.3 | 36 15.0 | -33.2 | 112.9 | 35 51.3 | -34.2 | 113.6 | 35 27.0          | -35.2 | 114.3 | 35 02.0 | -36.1 | 114.9 | 34 36.5 | -37.1 | 115.5 | 34 10.3 | -37.9 | 116.1 | 2    |
| 3                                     | 36 29.2 | -31.8 | 112.6 | 36 05.8 | -32.8 | 113.3 | 35 41.8 | -33.8 | 114.0 | 35 17.1 | -34.7 | 114.6 | 34 51.8          | -35.7 | 115.2 | 34 25.9 | -36.6 | 115.9 | 33 59.4 | -37.4 | 116.5 | 33 32.4 | -38.3 | 117.1 | 3    |
| 4                                     | 35 57.4 | -32.3 | 113.7 | 35 33.0 | -33.3 | 114.3 | 35 08.0 | -34.3 | 115.0 | 34 42.4 | -35.3 | 115.6 | 34 16.1          | -36.1 | 116.2 | 33 49.3 | -37.0 | 116.8 | 33 22.0 | -37.9 | 117.4 | 32 54.1 | -38.7 | 118.0 | 4    |
| 5                                     | 35 25.1 | -32.9 | 114.7 | 34 59.7 | -33.8 | 115.4 | 34 33.7 | -34.7 | 116.0 | 34 07.1 | -35.6 | 116.6 | 33 40.0          | -36.6 | 117.2 | 33 12.3 | -37.4 | 117.8 | 32 44.1 | -38.3 | 118.3 | 32 15.4 | -39.2 | 118.9 | 5    |
| 6                                     | 34 52.2 | -33.4 | 115.7 | 34 25.9 | -34.3 | 116.4 | 33 59.0 | -35.3 | 117.0 | 33 31.5 | -36.2 | 117.6 | 33 03.4          | -37.0 | 118.1 | 32 34.9 | -37.9 | 118.7 | 32 05.8 | -38.7 | 119.3 | 31 36.2 | -39.4 | 119.8 | 6    |
| 7                                     | 34 18.8 | -33.8 | 116.7 | 33 51.6 | -34.8 | 117.3 | 33 23.7 | -35.7 | 117.9 | 32 55.3 | -36.5 | 118.5 | 32 26.4          | -37.4 | 119.1 | 31 57.0 | -38.2 | 119.6 | 31 27.1 | -39.0 | 120.2 | 30 56.8 | -39.9 | 120.7 | 7    |
| 8                                     | 33 45.0 | -34.4 | 117.7 | 33 16.8 | -35.3 | 118.3 | 32 48.0 | -36.1 | 118.9 | 32 18.8 | -37.0 | 119.5 | 31 49.0          | -37.8 | 120.0 | 31 18.8 | -38.6 | 120.5 | 30 48.1 | -39.4 | 121.0 | 30 16.9 | -40.1 | 121.5 | 8    |
| 9                                     | 33 10.6 | -34.8 | 118.7 | 32 41.5 | -35.6 | 119.3 | 32 11.9 | -36.5 | 119.8 | 31 41.8 | -37.3 | 120.4 | 31 11.2          | -38.1 | 120.9 | 30 40.2 | -39.0 | 121.4 | 30 08.7 | -39.8 | 121.9 | 29 36.8 | -40.5 | 122.4 | 9    |
| 10                                    | 32 35.8 | -35.2 | 119.7 | 32 05.9 | -36.1 | 120.2 | 31 35.4 | -36.9 | 120.8 | 31 04.5 | -37.8 | 121.3 | 30 33.1          | -38.6 | 121.8 | 30 01.2 | -39.3 | 122.3 | 29 28.9 | -40.0 | 122.8 | 28 56.3 | -40.9 | 123.3 | 10   |
| 11                                    | 32 00.6 | -35.7 | 120.7 | 31 29.8 | -36.5 | 121.2 | 30 58.5 | -37.3 | 121.7 | 30 26.7 | -38.1 | 122.2 | 29 54.5          | -38.9 | 122.7 | 29 21.9 | -39.6 | 123.2 | 28 48.9 | -40.4 | 123.6 | 28 15.4 | -41.1 | 124.1 | 11   |
| 12                                    | 31 24.9 | -36.0 | 121.6 | 30 53.3 | -36.9 | 122.1 | 30 21.2 | -37.7 | 122.6 | 29 48.6 | -38.5 | 123.1 | 29 15.6          | -39.2 | 123.6 | 28 42.3 | -40.0 | 124.0 | 28 08.5 | -40.7 | 124.5 | 27 34.3 | -41.4 | 124.9 | 12   |
| 13                                    | 30 48.9 | -36.5 | 122.5 | 30 16.4 | -37.3 | 123.0 | 29 43.5 | -38.1 | 123.5 | 29 10.1 | -38.8 | 124.0 | 28 36.4          | -39.6 | 124.4 | 28 02.3 | -40.3 | 124.9 | 27 27.8 | -41.0 | 125.3 | 26 52.9 | -41.7 | 125.7 | 13   |
| 14                                    | 30 12.4 | -36.9 | 123.5 | 29 39.1 | -37.6 | 123.9 | 28 05.4 | -38.4 | 124.4 | 28 31.3 | -39.1 | 124.8 | 27 56.8          | -39.8 | 125.3 | 27 22.0 | -40.6 | 125.7 | 26 46.8 | -41.3 | 126.1 | 26 11.2 | -41.9 | 126.5 | 14   |
| 15                                    | 29 35.5 | -37.2 | 124.4 | 29 01.5 | -38.0 | 124.8 | 28 27.0 | -38.7 | 125.3 | 27 52.2 | -39.5 | 125.7 | 27 17.0          | -40.2 | 126.1 | 26 41.4 | -40.8 | 126.5 | 26 05.5 | -41.5 | 126.9 | 25 29.3 | -42.2 | 127.3 | 15   |
| 16                                    | 28 58.3 | -37.6 | 125.3 | 28 23.5 | -38.4 | 125.7 | 27 48.3 | -39.1 | 126.1 | 27 12.7 | -39.8 | 126.6 | 26 36.8          | -40.5 | 127.0 | 26 00.6 | -41.2 | 127.4 | 25 24.0 | -41.8 | 127.7 | 24 47.1 | -42.4 | 128.1 | 16   |
| 17                                    | 28 20.7 | -37.9 | 126.1 | 27 45.1 | -38.6 | 126.6 | 27 09.2 | -39.3 | 127.0 | 26 32.9 | -40.0 | 127.4 | 25 56.3          | -40.7 | 127.8 | 25 19.4 | -41.4 | 128.2 | 24 42.2 | -42.0 | 128.5 | 24 04.7 | -42.7 | 128.9 | 17   |
| 18                                    | 27 42.8 | -38.2 | 127.0 | 27 06.5 | -39.0 | 127.4 | 26 29.9 | -39.7 | 127.8 | 25 52.9 | -40.3 | 128.2 | 25 15.6          | -41.0 | 128.6 | 24 38.0 | -41.6 | 129.0 | 24 00.2 | -42.3 | 129.3 | 23 22.0 | -42.9 | 129.7 | 18   |
| 19                                    | 27 04.6 | -38.6 | 127.9 | 26 27.5 | -39.2 | 128.3 | 25 50.2 | -39.9 | 128.7 | 25 12.6 | -40.6 | 129.0 | 24 34.6          | -41.2 | 129.4 | 23 56.4 | -41.9 | 129.8 | 23 17.9 | -42.5 | 130.1 | 22 39.1 | -43.1 | 130.4 | 19   |
| 20                                    | 26 26.0 | -38.9 | 128.8 | 25 48.3 | -39.6 | 129.1 | 25 10.3 | -40.3 | 129.5 | 24 32.0 | -40.9 | 129.9 | 23 53.4          | -41.5 | 130.2 | 23 14.5 | -42.1 | 130.5 | 22 35.4 | -42.7 | 130.9 | 21 56.0 | -43.3 | 131.2 | 20   |
| 21                                    | 25 47.1 | -39.1 | 129.6 | 25 08.7 | -39.8 | 130.0 | 24 30.0 | -40.4 | 130.3 | 23 51.1 | -41.1 | 130.7 | 23 11.9          | -41.8 | 131.0 | 22 32.4 | -42.4 | 131.3 | 21 52.7 | -43.0 | 131.6 | 21 12.7 | -43.5 | 131.9 | 21   |
| 22                                    | 25 08.0 | -39.5 | 130.4 | 24 28.9 | -40.1 | 130.8 | 23 49.6 | -40.8 | 131.1 | 23 10.0 | -41.4 | 131.5 | 22 30.1          | -41.9 | 131.8 | 21 50.0 | -42.5 | 132.1 | 21 09.7 | -43.1 | 132.4 | 20 29.2 | -43.7 | 132.6 | 22   |
| 23                                    | 24 28.5 | -39.7 | 131.3 | 23 48.8 | -40.3 | 131.6 | 23 08.8 | -40.9 | 131.9 | 22 28.6 | -41.5 | 132.2 | 21 48.2          | -42.2 | 132.5 | 21 07.5 | -42.7 | 132.8 | 20 26.6 | -43.3 | 133.1 | 19 45.5 | -43.9 | 133.4 | 23   |
| 24                                    | 23 48.6 | -40.0 | 132.1 | 23 08.5 | -40.6 | 132.4 | 22 27.9 | -41.2 | 132.7 | 21 47.1 | -41.8 | 133.0 | 21 06.0          | -42.4 | 133.3 | 20 24.8 | -43.0 | 133.6 | 19 43.3 | -43.5 | 133.8 | 19 01.6 | -44.0 | 134.1 | 24   |

## Sight Reduction Individual Problems

Step 10: Determine the azimuth correction for the sight (to account for increments of declination ignored in step 9).

|                 | Base Value | Base Z | Next incremental Z | Difference in Z | Increment | Correction<br>(Diff Z x Increment) / 60 |
|-----------------|------------|--------|--------------------|-----------------|-----------|-----------------------------------------|
| Latitude – N    | 26°        | 130.7° | -                  | -               | 00.0'     | 0                                       |
| Declination - S | 21°        | 130.7° | 131.5°             | 0.8'            | 53.5'     | 0.71°                                   |
| LHA             | 312°       | 130.7° | -                  | -               | 00.0'     | 0                                       |

Total correction = 0.7°

Step 11: Apply the correction to the base values to determine true azimuth.

Base azimuth: 130.7°

Correction: +0.7°

Corrected azimuth:  $130.7^\circ + 0.7^\circ = \mathbf{131.4^\circ}$

*Note - Check azimuth rules: if LHA greater than 180°, then  $zn = z$ .*

Step 12: Determine the computed altitude.

Tabular computed altitude (Hc): 23° 51.1'

Altitude difference (d): -41.1

Declination: S 21° 53.5'

Declination increments: 53.5'

Altitude difference correction:

Tens: 35.7'

Units/decimals: 1.0'

Total correction:  $35.7' + 1.0' = \mathbf{36.7'}$

|              |     | Altitude Difference (d) |      |      |      |     |          |     |     |     |     |       |     |     |     |     |     |
|--------------|-----|-------------------------|------|------|------|-----|----------|-----|-----|-----|-----|-------|-----|-----|-----|-----|-----|
| Dec.<br>Inc. |     | Tens                    |      |      |      |     | Decimals |     |     |     |     | Units |     |     |     |     |     |
|              |     | 10'                     | 20'  | 30'  | 40'  | 50' | ↓        | 0'  | 1'  | 2'  | 3'  | 4'    | 5'  | 6'  | 7'  | 8'  | 9'  |
| 52.0         | 8.6 | 17.3                    | 26.0 | 34.6 | 43.3 |     | .0       | 0.0 | 0.9 | 1.7 | 2.6 | 3.5   | 4.4 | 5.2 | 6.1 | 7.0 | 7.9 |
| 52.1         | 8.7 | 17.3                    | 26.0 | 34.7 | 43.4 |     | .1       | 0.1 | 1.0 | 1.8 | 2.7 | 3.6   | 4.5 | 5.3 | 6.2 | 7.1 | 8.0 |
| 52.2         | 8.7 | 17.4                    | 26.1 | 34.8 | 43.5 |     | .2       | 0.2 | 1.0 | 1.9 | 2.8 | 3.7   | 4.5 | 5.4 | 6.3 | 7.2 | 8.0 |
| 52.3         | 8.7 | 17.4                    | 26.1 | 34.9 | 43.6 |     | .3       | 0.3 | 1.1 | 2.0 | 2.9 | 3.8   | 4.6 | 5.5 | 6.4 | 7.3 | 8.1 |
| 52.4         | 8.7 | 17.5                    | 26.2 | 34.9 | 43.7 |     | .4       | 0.3 | 1.2 | 2.1 | 3.0 | 3.8   | 4.7 | 5.6 | 6.5 | 7.3 | 8.2 |
| 52.5         | 8.8 | 17.5                    | 26.3 | 35.0 | 43.8 |     | .5       | 0.4 | 1.3 | 2.2 | 3.1 | 3.9   | 4.8 | 5.7 | 6.6 | 7.4 | 8.3 |
| 52.6         | 8.8 | 17.5                    | 26.3 | 35.1 | 43.8 |     | .6       | 0.5 | 1.4 | 2.3 | 3.1 | 4.0   | 4.9 | 5.8 | 6.6 | 7.5 | 8.4 |
| 52.7         | 8.8 | 17.6                    | 26.4 | 35.2 | 43.9 |     | .7       | 0.6 | 1.5 | 2.4 | 3.2 | 4.1   | 5.0 | 5.9 | 6.7 | 7.6 | 8.5 |
| 52.8         | 8.8 | 17.6                    | 26.4 | 35.2 | 44.0 |     | .8       | 0.7 | 1.6 | 2.4 | 3.3 | 4.2   | 5.1 | 5.9 | 6.8 | 7.7 | 8.6 |
| 52.9         | 8.9 | 17.7                    | 26.5 | 35.3 | 44.1 |     | .9       | 0.8 | 1.7 | 2.5 | 3.4 | 4.3   | 5.2 | 6.0 | 6.9 | 7.8 | 8.7 |
| 53.0         | 8.8 | 17.6                    | 26.5 | 35.3 | 44.1 |     | .0       | 0.0 | 0.9 | 1.8 | 2.7 | 3.6   | 4.5 | 5.3 | 6.2 | 7.1 | 8.0 |
| 53.1         | 8.8 | 17.7                    | 26.5 | 35.4 | 44.2 |     | .1       | 0.1 | 1.0 | 1.9 | 2.8 | 3.7   | 4.5 | 5.4 | 6.3 | 7.2 | 8.1 |
| 53.2         | 8.8 | 17.7                    | 26.6 | 35.4 | 44.3 |     | .2       | 0.2 | 1.1 | 2.0 | 2.9 | 3.7   | 4.6 | 5.5 | 6.4 | 7.3 | 8.2 |
| 53.3         | 8.9 | 17.8                    | 26.6 | 35.5 | 44.4 |     | .3       | 0.3 | 1.2 | 2.1 | 2.9 | 3.8   | 4.7 | 5.6 | 6.5 | 7.4 | 8.3 |
| 53.4         | 8.9 | 17.8                    | 26.7 | 35.6 | 44.5 |     | .4       | 0.4 | 1.2 | 2.1 | 3.0 | 3.9   | 4.8 | 5.7 | 6.6 | 7.5 | 8.4 |
| 53.5         | 8.9 | 17.8                    | 26.8 | 35.7 | 44.6 |     | .5       | 0.4 | 1.3 | 2.2 | 3.1 | 4.0   | 4.9 | 5.8 | 6.7 | 7.6 | 8.5 |
| 53.6         | 8.9 | 17.9                    | 26.8 | 35.7 | 44.7 |     | .6       | 0.5 | 1.4 | 2.3 | 3.2 | 4.1   | 5.0 | 5.9 | 6.8 | 7.7 | 8.6 |
| 53.7         | 9.0 | 17.9                    | 26.9 | 35.8 | 44.8 |     | .7       | 0.6 | 1.5 | 2.4 | 3.3 | 4.2   | 5.1 | 6.0 | 6.9 | 7.8 | 8.6 |
| 53.8         | 9.0 | 18.0                    | 26.9 | 35.9 | 44.9 |     | .8       | 0.7 | 1.6 | 2.5 | 3.4 | 4.3   | 5.2 | 6.1 | 7.0 | 7.8 | 8.7 |
| 53.9         | 9.0 | 18.0                    | 27.0 | 36.0 | 45.0 |     | .9       | 0.8 | 1.7 | 2.6 | 3.5 | 4.4   | 5.3 | 6.2 | 7.0 | 7.9 | 8.8 |

*Note this step can be completed without the interpolation table by using the formula:*

$$\text{Correction} = (\text{Altitude Difference (d)}) \frac{\text{Declination Increment}}{60}$$

Tabular Hc: 23° 51.1'

Alt correction: -36.7'

hc:  $23^\circ 51.1' - 36.7' = \mathbf{23^\circ 14.4'}$

S. Lat.  $\begin{cases} \text{L.H.A. greater than } 180^\circ \dots \text{Zn} = 180^\circ - \text{Z} \\ \text{L.H.A. less than } 180^\circ \dots \text{Zn} = 180^\circ + \text{Z} \end{cases}$



## Sight Reduction Individual Problems

### Sight Reduction of the Moon Problems

RED D6. On 25 February at 0622 zone time, you observe the upper limb of the Moon with a sextant altitude of  $59^{\circ} 58.6'$ . Your DR position is latitude  $30^{\circ} 28.3' S$ , longitude  $102^{\circ} 39.3' E$ . The chronometer reading at the time of the sight is 11h 21m 18s and the chronometer is 48s slow. The height of eye is 59 feet and the index error is  $2.5'$  on the arc. What are the azimuth (Zn) and intercept (a) of this sight using the assumed position?

Answer:  $Zn = 304.1^{\circ} T$ ,  $a = 4.2'$  towards.

- Step 1: Determine the GMT of the sight.  
 Chronometer time: 11h 21m 18s  
 Chronometer error: 48s slow  
 Correct chronometer time: 11h 21m 18s + 48s = 11:22:06  
 Ship time: 0622 zone time.  
 DR longitude:  $102^{\circ} 39.3' E$  corresponds to (-7 ZD)  
 GMT of sight: 23:22:06 GMT, 24 February

- Step 2: Determine the sextant altitude (hs).  
 $hs = 59^{\circ} 58.6'$  (Given)

- Step 3: Determine the index correction (IC).  
 Index error:  $2.5'$  on the arc.  
 Index correction:  $-2.5'$

- Step 4: Determine the dip correction.  
 Height of eye: 59 feet.  
 Dip correction:  $-7.5'$

- Step 5: Determine the apparent altitude (ha).  
 $Apparent\ altitude\ (ha) = hs \pm IC \pm dip$   
 $ha = 59^{\circ} 58.6' - 2.5' - 7.5' = \underline{59^{\circ} 48.6'}$

| G.M.T.    | SUN               |      |  | MOON                    |         |      |      |      |  |  |
|-----------|-------------------|------|--|-------------------------|---------|------|------|------|--|--|
|           | G.H.A.            | Dec. |  | G.H.A.                  | $\nu$   | Dec. | $d$  | H.P. |  |  |
| <b>24</b> | 176 40.2 S 9 34.3 |      |  | 302 07.8 15.3 S         | 7 19.3  | 9.7  | 54.2 |      |  |  |
| <b>01</b> | 191 40.3 33.3     |      |  | 316 42.1 15.2           | 7 29.0  | 9.6  | 54.2 |      |  |  |
| <b>02</b> | 206 40.4 32.4     |      |  | 331 16.3 15.2           | 7 38.6  | 9.6  | 54.2 |      |  |  |
| <b>03</b> | 221 40.5 31.5     |      |  | 345 50.5 15.2           | 7 48.2  | 9.6  | 54.2 |      |  |  |
| <b>04</b> | 236 40.6 30.6     |      |  | 0 24.7 15.1             | 7 57.8  | 9.6  | 54.2 |      |  |  |
| <b>05</b> | 251 40.6 29.6     |      |  | 14 58.8 15.2            | 8 07.4  | 9.5  | 54.2 |      |  |  |
| <b>06</b> | 266 40.7 S 9 28.7 |      |  | 29 33.0 15.1 S          | 8 16.9  | 9.5  | 54.2 |      |  |  |
| <b>07</b> | 281 40.8 27.8     |      |  | 44 07.1 15.1            | 8 26.4  | 9.4  | 54.2 |      |  |  |
| <b>08</b> | 296 40.9 26.9     |      |  | 58 41.2 15.1            | 8 35.8  | 9.4  | 54.2 |      |  |  |
| <b>09</b> | 311 41.0 26.0     |      |  | 73 15.3 15.1            | 8 45.2  | 9.4  | 54.2 |      |  |  |
| <b>10</b> | 326 41.1 25.0     |      |  | 87 49.4 15.1            | 8 54.6  | 9.3  | 54.2 |      |  |  |
| <b>11</b> | 341 41.2 24.1     |      |  | 102 23.5 15.0           | 9 03.9  | 9.3  | 54.2 |      |  |  |
| <b>12</b> | 356 41.3 S 9 23.2 |      |  | 116 57.5 15.0 S         | 9 13.2  | 9.3  | 54.2 |      |  |  |
| <b>13</b> | 11 41.4 22.3      |      |  | 131 31.5 15.0           | 9 22.5  | 9.2  | 54.2 |      |  |  |
| <b>14</b> | 26 41.5 21.3      |      |  | 146 05.5 15.0           | 9 31.7  | 9.1  | 54.2 |      |  |  |
| <b>15</b> | 41 41.6 20.4      |      |  | 160 39.5 14.9           | 9 40.8  | 9.2  | 54.2 |      |  |  |
| <b>16</b> | 56 41.7 19.5      |      |  | 175 13.4 14.9           | 9 50.0  | 9.1  | 54.2 |      |  |  |
| <b>17</b> | 71 41.8 18.6      |      |  | 189 47.3 14.9           | 9 59.1  | 9.0  | 54.2 |      |  |  |
| <b>18</b> | 86 41.9 S 9 17.6  |      |  | 204 21.2 14.9 S 10 08.1 | 9.1     | 54.2 |      |      |  |  |
| <b>19</b> | 101 42.0 16.7     |      |  | 218 55.1 14.9           | 10 17.2 | 8.9  | 54.2 |      |  |  |
| <b>20</b> | 116 42.1 15.8     |      |  | 233 29.0 14.8           | 10 26.1 | 9.0  | 54.2 |      |  |  |
| <b>21</b> | 131 42.2 14.8     |      |  | 248 02.8 14.8           | 10 35.1 | 8.8  | 54.2 |      |  |  |
| <b>22</b> | 146 42.3 13.9     |      |  | 262 36.6 14.7           | 10 43.9 | 8.9  | 54.2 |      |  |  |
| <b>23</b> | 161 42.4 13.0     |      |  | 277 10.3 14.8           | 10 52.8 | 8.8  | 54.2 |      |  |  |

- Step 6: Determine the horizontal parallax (HP) of the Moon.  
 For 24 February at 2322, the HP is 54.2'

- Step 7: Determine main correction.  
 Apparent altitude:  $59^{\circ} 48.6'$   
 Apparent altitude correction 1:  $+39.1'$   
 Horizontal parallax: 54.2'  
 Limb observed (correction): Upper ( $-30'$ )  
 Apparent altitude correction 2:  $+2.7'$   
 Total altitude correction:  $39.1' + 2.7' - 30.0' = +11.8'$

- Step 8: Determine the observed altitude (ho).  
 Observed altitude =  $59^{\circ} 48.6' + 11.8' = \underline{60^{\circ} 00.4'}$

# Sight Reduction Individual Problems

- Step 9: Determine the declination of the Moon.  
Declination (hours): S 10° 52.8' (d number: 8.8)  
Declination (increment): 3.3'  
Declination (total): 10° 52.8' + 3.3' = S 10° 56.1'
- Step 10: Determine the GHA of the Moon.  
GHA (hours): 277° 10.3' (v number: 14.8)  
GHA (increment): 5° 16.4'  
GHA (v correction): 5.6'  
GHA (total): 277° 10.3' + 5° 16.4' + 5.6' = 282° 32.3'
- Step 11: Determine the assumed position of the ship.  
DR latitude: 30° 28.3' S  
Assumed latitude: 30° S  
DR longitude: 102° 39.3' E  
Assumed longitude (to ensure whole number of LHA): 102° 27.7' E
- Step 12: Determine the LHA for the Moon for the time of sight.  
GHA (Moon): 282° 32.3'  
Assumed longitude: 102° 27.7' E  
LHA (Moon): 282° 32.3' + 102° 27.7' E (-360°) = 25° (-west, +east)

| <sup>m</sup> | <sup>s</sup> | SUN    | ARIES  | MOON    | <sup>v</sup><br>or<br><sup>d</sup> | <sup>v</sup><br>or<br><sup>d</sup> | <sup>v</sup><br>or<br><sup>d</sup> | <sup>v</sup><br>or<br><sup>d</sup> |
|--------------|--------------|--------|--------|---------|------------------------------------|------------------------------------|------------------------------------|------------------------------------|
| 22           | PLANETS      |        |        |         |                                    |                                    |                                    |                                    |
| 00           | 5 30.0       | 5 30.9 | 5 15.0 | 0.0 0.0 | 6.0 2.3                            | 12.0 4.5                           |                                    |                                    |
| 01           | 5 30.3       | 5 31.2 | 5 15.2 | 0.1 0.0 | 6.1 2.3                            | 12.1 4.5                           |                                    |                                    |
| 02           | 5 30.5       | 5 31.4 | 5 15.4 | 0.2 0.1 | 6.2 2.3                            | 12.2 4.6                           |                                    |                                    |
| 03           | 5 30.8       | 5 31.7 | 5 15.7 | 0.3 0.1 | 6.3 2.4                            | 12.3 4.6                           |                                    |                                    |
| 04           | 5 31.0       | 5 31.9 | 5 15.9 | 0.4 0.2 | 6.4 2.4                            | 12.4 4.7                           |                                    |                                    |
| 05           | 5 31.3       | 5 32.2 | 5 16.2 | 0.5 0.2 | 6.5 2.4                            | 12.5 4.7                           |                                    |                                    |
| 06           | 5 31.5       | 5 32.4 | 5 16.4 | 0.6 0.2 | 6.6 2.5                            | 12.6 4.7                           |                                    |                                    |
| 07           | 5 31.8       | 5 32.7 | 5 16.6 | 0.7 0.3 | 6.7 2.5                            | 12.7 4.8                           |                                    |                                    |
| 08           | 5 32.0       | 5 32.9 | 5 16.9 | 0.8 0.3 | 6.8 2.6                            | 12.8 4.8                           |                                    |                                    |
| 09           | 5 32.3       | 5 33.2 | 5 17.1 | 0.9 0.3 | 6.9 2.6                            | 12.9 4.8                           |                                    |                                    |
| 10           | 5 32.5       | 5 33.4 | 5 17.4 | 1.0 0.4 | 7.0 2.6                            | 13.0 4.9                           |                                    |                                    |
| 11           | 5 32.8       | 5 33.7 | 5 17.6 | 1.1 0.4 | 7.1 2.7                            | 13.1 4.9                           |                                    |                                    |
| 12           | 5 33.0       | 5 33.9 | 5 17.8 | 1.2 0.5 | 7.2 2.7                            | 13.2 5.0                           |                                    |                                    |
| 13           | 5 33.3       | 5 34.2 | 5 18.1 | 1.3 0.5 | 7.3 2.7                            | 13.3 5.0                           |                                    |                                    |
| 14           | 5 33.5       | 5 34.4 | 5 18.3 | 1.4 0.5 | 7.4 2.8                            | 13.4 5.0                           |                                    |                                    |
| 15           | 5 33.8       | 5 34.7 | 5 18.5 | 1.5 0.6 | 7.5 2.8                            | 13.5 5.1                           |                                    |                                    |
| 16           | 5 34.0       | 5 34.9 | 5 18.8 | 1.6 0.6 | 7.6 2.9                            | 13.6 5.1                           |                                    |                                    |
| 17           | 5 34.3       | 5 35.2 | 5 19.0 | 1.7 0.6 | 7.7 2.9                            | 13.7 5.1                           |                                    |                                    |
| 18           | 5 34.5       | 5 35.4 | 5 19.3 | 1.8 0.7 | 7.8 2.9                            | 13.8 5.2                           |                                    |                                    |
| 19           | 5 34.8       | 5 35.7 | 5 19.5 | 1.9 0.7 | 7.9 3.0                            | 13.9 5.2                           |                                    |                                    |
| 20           | 5 35.0       | 5 35.9 | 5 19.7 | 2.0 0.8 | 8.0 3.0                            | 14.0 5.3                           |                                    |                                    |
| 21           | 5 35.3       | 5 36.2 | 5 20.0 | 2.1 0.8 | 8.1 3.0                            | 14.1 5.3                           |                                    |                                    |
| 22           | 5 35.5       | 5 36.4 | 5 20.2 | 2.2 0.8 | 8.2 3.1                            | 14.2 5.3                           |                                    |                                    |
| 23           | 5 35.8       | 5 36.7 | 5 20.5 | 2.3 0.9 | 8.3 3.1                            | 14.3 5.4                           |                                    |                                    |
| 24           | 5 36.0       | 5 36.9 | 5 20.7 | 2.4 0.9 | 8.4 3.2                            | 14.4 5.4                           |                                    |                                    |
| 25           | 5 36.3       | 5 37.2 | 5 20.9 | 2.5 0.9 | 8.5 3.2                            | 14.5 5.4                           |                                    |                                    |
| 26           | 5 36.5       | 5 37.4 | 5 21.2 | 2.6 1.0 | 8.6 3.2                            | 14.6 5.5                           |                                    |                                    |
| 27           | 5 36.8       | 5 37.7 | 5 21.4 | 2.7 1.0 | 8.7 3.3                            | 14.7 5.5                           |                                    |                                    |
| 28           | 5 37.0       | 5 37.9 | 5 21.6 | 2.8 1.1 | 8.8 3.3                            | 14.8 5.6                           |                                    |                                    |
| 29           | 5 37.3       | 5 38.2 | 5 21.9 | 2.9 1.1 | 8.9 3.3                            | 14.9 5.6                           |                                    |                                    |

| ALTITUDE CORRECTION |                   |                   |                   |                   |                   |  |  |  |  |  |
|---------------------|-------------------|-------------------|-------------------|-------------------|-------------------|--|--|--|--|--|
| App. Alt.           | 35°-39°           | 40°-44°           | 45°-49°           | 50°-54°           | 55°-59°           |  |  |  |  |  |
|                     | Corr <sup>n</sup> | Corr <sup>n</sup> | Corr <sup>n</sup> | Corr <sup>n</sup> | Corr <sup>n</sup> |  |  |  |  |  |
| 00                  | 35 56.5           | 40 53.7           | 45 50.5           | 50 46.9           | 55 43.1           |  |  |  |  |  |
| 10                  | 56.4              | 53.6              | 50.4              | 46.8              | 42.9              |  |  |  |  |  |
| 20                  | 56.3              | 53.5              | 50.2              | 46.7              | 42.8              |  |  |  |  |  |
| 30                  | 56.2              | 53.4              | 50.1              | 46.5              | 42.7              |  |  |  |  |  |
| 40                  | 56.2              | 53.3              | 50.0              | 46.4              | 42.5              |  |  |  |  |  |
| 50                  | 56.1              | 53.2              | 49.9              | 46.3              | 42.4              |  |  |  |  |  |
| 00                  | 36 56.0           | 41 53.1           | 46 49.8           | 51 46.2           | 56 42.3           |  |  |  |  |  |
| 10                  | 55.9              | 53.0              | 49.7              | 46.0              | 42.1              |  |  |  |  |  |
| 20                  | 55.8              | 52.8              | 49.5              | 45.9              | 42.0              |  |  |  |  |  |
| 30                  | 55.7              | 52.7              | 49.4              | 45.8              | 41.8              |  |  |  |  |  |
| 40                  | 55.6              | 52.6              | 49.3              | 45.7              | 41.7              |  |  |  |  |  |
| 50                  | 55.5              | 52.5              | 49.2              | 45.5              | 41.6              |  |  |  |  |  |
| 00                  | 37 55.4           | 42 52.4           | 47 49.1           | 52 45.4           | 57 41.4           |  |  |  |  |  |
| 10                  | 55.3              | 52.3              | 49.0              | 45.3              | 41.3              |  |  |  |  |  |
| 20                  | 55.2              | 52.2              | 48.8              | 45.2              | 41.2              |  |  |  |  |  |
| 30                  | 55.1              | 52.1              | 48.7              | 45.0              | 41.0              |  |  |  |  |  |
| 40                  | 55.0              | 52.0              | 48.6              | 44.9              | 40.9              |  |  |  |  |  |
| 50                  | 55.0              | 51.9              | 48.5              | 44.8              | 40.8              |  |  |  |  |  |
| 00                  | 38 54.9           | 43 51.8           | 48 48.4           | 53 44.6           | 58 40.6           |  |  |  |  |  |
| 10                  | 54.8              | 51.7              | 48.2              | 44.5              | 40.5              |  |  |  |  |  |
| 20                  | 54.7              | 51.6              | 48.1              | 44.4              | 40.3              |  |  |  |  |  |
| 30                  | 54.6              | 51.5              | 48.0              | 44.2              | 40.2              |  |  |  |  |  |
| 40                  | 54.5              | 51.4              | 47.9              | 44.1              | 40.1              |  |  |  |  |  |
| 50                  | 54.4              | 51.2              | 47.8              | 44.0              | 39.9              |  |  |  |  |  |
| 00                  | 39 54.3           | 44 51.1           | 49 47.6           | 54 43.9           | 59 39.8           |  |  |  |  |  |
| 10                  | 54.2              | 51.0              | 47.5              | 43.7              | 39.6              |  |  |  |  |  |
| 20                  | 54.1              | 50.9              | 47.4              | 43.6              | 39.5              |  |  |  |  |  |
| 30                  | 54.0              | 50.8              | 47.3              | 43.5              | 39.4              |  |  |  |  |  |
| 40                  | 53.9              | 50.7              | 47.2              | 43.3              | 39.2              |  |  |  |  |  |
| 50                  | 53.8              | 50.6              | 47.0              | 43.2              | 39.1              |  |  |  |  |  |
| H.P.                | L U L U           | L U L U           | L U L U           | L U L U           | L U L U           |  |  |  |  |  |
| 54.0                | 1.1 1.7           | 1.3 1.9           | 1.5 2.1           | 1.7 2.4           | 2.0 2.6           |  |  |  |  |  |
| 54.3                | 1.4 1.8           | 1.6 2.0           | 1.8 2.2           | 2.0 2.5           | 2.3 2.7           |  |  |  |  |  |
| 54.6                | 1.7 2.0           | 1.9 2.2           | 2.1 2.4           | 2.3 2.6           | 2.5 2.8           |  |  |  |  |  |
| 54.9                | 2.0 2.2           | 2.2 2.3           | 2.3 2.5           | 2.5 2.7           | 2.7 2.9           |  |  |  |  |  |
| 55.2                | 2.3 2.3           | 2.5 2.4           | 2.6 2.6           | 2.8 2.8           | 3.0 2.9           |  |  |  |  |  |

## Sight Reduction Individual Problems

| 25°, 335° L.H.A. |         | LATITUDE SAME NAME AS DECLINATION |       |         |       |       |         |       |       |         |       | N. Lat. { L.H.A. greater than 180° ..... Zn=Z<br>L.H.A. less than 180° ..... Zn=360°-Z |         |       |       |         |       |       |         |       |       |         |       |       |      |
|------------------|---------|-----------------------------------|-------|---------|-------|-------|---------|-------|-------|---------|-------|----------------------------------------------------------------------------------------|---------|-------|-------|---------|-------|-------|---------|-------|-------|---------|-------|-------|------|
|                  | 23°     |                                   |       | 24°     |       |       | 25°     |       |       | 26°     |       |                                                                                        | 27°     |       |       | 28°     |       |       | 29°     |       |       | 30°     |       |       |      |
| Dec.             | Hc      | d                                 | Z     | Hc      | d     | Z     | Hc      | d     | Z     | Hc      | d     | Z                                                                                      | Hc      | d     | Z     | Hc      | d     | Z     | Hc      | d     | Z     | Hc      | d     | Z     | Dec. |
| 0                | 56 32.3 | +42                               | 130.0 | 55 53.3 | +43   | 131.1 | 55 13.5 | +44   | 132.2 | 54 32.8 | +45   | 133.2                                                                                  | 53 51.3 | +45.9 | 134.2 | 53 09.1 | +46   | 135.2 | 52 26.2 | +47   | 136.1 | 51 42.6 | +48   | 137.0 | 0    |
| 1                | 57 14.5 | +41.2                             | 128.7 | 56 36.5 | +42.3 | 129.8 | 55 57.6 | +43.4 | 131.0 | 55 17.8 | +44.3 | 132.1                                                                                  | 54 37.2 | +45.2 | 133.1 | 53 55.8 | +46.1 | 134.1 | 53 13.6 | +47   | 135.1 | 52 30.8 | +47.7 | 136.0 | 1    |
| 2                | 57 55.7 | +40.4                             | 127.3 | 57 18.8 | +41.6 | 128.5 | 56 41.0 | +42.8 | 129.7 | 56 02.1 | +43.7 | 130.9                                                                                  | 55 22.4 | +44.6 | 132.0 | 54 41.9 | +45.5 | 133.0 | 54 00.6 | +46.3 | 134.1 | 53 18.5 | +47.1 | 135.0 | 2    |
| 3                | 58 36.1 | +39.4                             | 125.9 | 58 00.4 | +40.6 | 127.2 | 57 23.6 | +41.8 | 128.4 | 56 45.8 | +42.8 | 129.6                                                                                  | 56 07.0 | +43.9 | 130.8 | 55 27.4 | +44.8 | 131.9 | 54 46.9 | +45.7 | 133.0 | 54 05.6 | +46.6 | 134.0 | 3    |
| 4                | 59 15.5 | +38.4                             | 124.4 | 58 41.0 | +39.7 | 125.8 | 58 05.4 | +40.9 | 127.1 | 57 28.6 | +42.1 | 128.4                                                                                  | 56 50.9 | +43.1 | 129.6 | 56 12.2 | +44.2 | 130.7 | 55 32.6 | +45.1 | 131.8 | 54 52.2 | +46.0 | 132.9 | 4    |
| 5                | 59 53.9 | +37.3                             | 122.9 | 59 20.7 | +38.7 | 124.3 | 58 46.3 | +39.9 | 125.7 | 58 10.7 | +41.2 | 127.0                                                                                  | 57 34.0 | +42.3 | 128.3 | 56 56.4 | +43.3 | 129.5 | 56 17.7 | +44.4 | 130.6 | 55 38.2 | +45.4 | 131.8 | 5    |
| 6                | 60 31.2 | +36.2                             | 121.3 | 59 59.4 | +37.6 | 122.8 | 59 26.2 | +39.0 | 124.3 | 58 51.9 | +40.2 | 125.6                                                                                  | 58 16.3 | +41.5 | 126.9 | 57 39.7 | +42.6 | 128.2 | 57 02.1 | +43.7 | 129.4 | 56 23.6 | +44.6 | 130.6 | 6    |
| 7                | 61 07.4 | +34.9                             | 119.7 | 60 37.0 | +36.4 | 121.3 | 60 05.2 | +37.8 | 122.7 | 59 32.1 | +39.2 | 124.2                                                                                  | 58 57.8 | +40.5 | 125.6 | 58 22.3 | +41.7 | 126.9 | 57 45.8 | +42.8 | 128.2 | 57 08.2 | +43.9 | 129.4 | 7    |
| 8                | 61 42.3 | +33.6                             | 118.0 | 61 13.4 | +35.2 | 119.6 | 60 43.0 | +36.8 | 121.2 | 60 11.3 | +38.2 | 122.7                                                                                  | 59 38.3 | +39.5 | 124.1 | 59 04.0 | +40.8 | 125.5 | 58 28.6 | +42.0 | 126.8 | 57 52.1 | +43.2 | 128.1 | 8    |
| 9                | 62 15.9 | +32.2                             | 116.2 | 61 48.6 | +33.9 | 117.9 | 61 19.8 | +35.5 | 119.5 | 60 49.5 | +37.0 | 121.1                                                                                  | 60 17.8 | +38.5 | 122.6 | 59 44.8 | +39.8 | 124.1 | 59 10.6 | +41.1 | 125.4 | 58 35.3 | +42.3 | 126.8 | 9    |
| 10               | 62 48.1 | +30.8                             | 114.4 | 62 22.5 | +32.5 | 116.2 | 61 55.3 | +34.2 | 117.8 | 61 26.5 | +35.8 | 119.5                                                                                  | 60 56.3 | +37.3 | 121.0 | 60 24.6 | +38.8 | 122.6 | 59 51.7 | +40.1 | 124.0 | 59 17.6 | +41.3 | 125.4 | 10   |
| 11               | 63 18.9 | +29.2                             | 112.5 | 62 55.0 | +31.1 | 114.3 | 62 29.5 | +32.8 | 116.1 | 62 02.3 | +34.5 | 117.8                                                                                  | 61 33.6 | +36.1 | 119.4 | 61 03.4 | +37.6 | 121.0 | 60 31.8 | +39.1 | 122.5 | 59 58.9 | +40.4 | 124.0 | 11   |
| 12               | 63 48.1 | +27.5                             | 110.6 | 63 26.1 | +29.5 | 112.4 | 63 02.3 | +31.4 | 114.3 | 62 36.8 | +33.2 | 116.0                                                                                  | 62 09.7 | +34.8 | 117.7 | 61 41.0 | +36.5 | 119.4 | 61 10.9 | +37.9 | 121.0 | 60 39.3 | +39.4 | 122.5 | 12   |
| 13               | 64 15.6 | +25.8                             | 108.5 | 63 55.6 | +27.8 | 110.5 | 63 33.7 | +29.8 | 112.4 | 63 10.0 | +31.6 | 114.2                                                                                  | 62 44.5 | +33.5 | 116.0 | 62 17.5 | +35.1 | 117.7 | 61 48.8 | +36.8 | 119.3 | 61 18.7 | +38.3 | 120.9 | 13   |
| 14               | 64 41.4 | +23.9                             | 106.4 | 64 23.4 | +26.1 | 108.4 | 64 03.5 | +28.1 | 110.4 | 63 41.6 | +30.1 | 112.3                                                                                  | 63 18.0 | +32.0 | 114.1 | 62 52.6 | +33.8 | 115.9 | 62 25.6 | +35.4 | 117.6 | 61 57.0 | +37.0 | 119.3 | 14   |

Step 13: Entering publication HO229 with assumed latitude, declination, and LHA, retrieve the computed altitude (hc), altitude difference (d), and azimuth (z) for the assumed position.

Assumed latitude: 30° S

Declination: S 10° (increments solved in step 14)

LHA: 25° (Same Pages)

HO 229 values:

Computed altitude (hc): 59° 17.6'

Altitude difference (d): + 41.3'

Azimuth (z): 125.4°

Step 14: Determine the azimuth correction for the sight (to account for increments of declination ignored in step 13).

|                 | Base Value | Base Z | Next incremental Z | Difference in Z | Increment | Correction<br>(Diff Z x Increment) / 60 |
|-----------------|------------|--------|--------------------|-----------------|-----------|-----------------------------------------|
| Latitude – S    | 30°        | 125.4° | -                  | -               | 00.0'     | 0                                       |
| Declination – S | 10°        | 125.4° | 124.0°             | -1.4°           | 56.1'     | -1.3°                                   |
| LHA             | 25°        | 125.4° | -                  | -               | 00.0'     | 0                                       |

Total correction = -1.3°

Step 15: Apply the correction to the base values to determine true azimuth.

Base azimuth: 125.4°

Correction: -1.3°

Corrected azimuth: 125.4° - 1.3° = 124.1°

*Note - Check azimuth rules: if LHA less than 180°, then zn = 180° + z.*

Corrected azimuth: 180° + 124.1° = **304.1° T**

## Sight Reduction Individual Problems

Step 16: Determine the computed altitude (hc).

Tabular computed altitude:  $59^{\circ} 17.6'$

Altitude difference (d):  $+41.3'$

Declination:  $S 10^{\circ} 56.1'$

Declination increments:  $56.1'$

Altitude difference correction:

Tens:  $37.4'$

Units/decimals:  $1.2'$

Total correction:  $37.4' + 1.2' = \underline{38.6'}$

Tabular hc:  $59^{\circ} 17.6'$

Altitude difference correction:  $+38.6'$

hc:  $59^{\circ} 17.6' + 38.6' = \underline{59^{\circ} 56.2'}$

Step 17: Determine the intercept (a).

Computed altitude (hc):  $59^{\circ} 56.2'$

Observed altitude (ho):  $60^{\circ} 00.4'$

Intercept (a):  $ho - hc = 60^{\circ} 00.4' - 59^{\circ} 56.2' = \underline{4.2'}$

If ho is greater, intercept is **towards**.

If hc is greater, intercept is away.

| Dec.<br>Inc. | Altitude Difference (d) |      |      |      |      |          |     |     |     |     |       |     |     |     |     |     |                     | Double<br>Second<br>Diff.<br>and<br>Corr. |
|--------------|-------------------------|------|------|------|------|----------|-----|-----|-----|-----|-------|-----|-----|-----|-----|-----|---------------------|-------------------------------------------|
|              | Tens                    |      |      |      |      | Decimals |     |     |     |     | Units |     |     |     |     |     |                     |                                           |
|              | 10'                     | 20'  | 30'  | 40'  | 50'  | ↓        | 0'  | 1'  | 2'  | 3'  | 4'    | 5'  | 6'  | 7'  | 8'  | 9'  |                     |                                           |
| 56.0         | 9.3                     | 18.6 | 28.0 | 37.3 | 46.6 | .0       | 0.0 | 0.9 | 1.9 | 2.8 | 3.8   | 4.7 | 5.6 | 6.6 | 7.5 | 8.5 | 3.6<br>10.9<br>18.2 | 0.1<br>0.2<br>0.3                         |
| 56.1         | 9.3                     | 18.7 | 28.0 | 37.4 | 46.7 | .1       | 0.1 | 1.0 | 2.0 | 2.9 | 3.9   | 4.8 | 5.7 | 6.7 | 7.6 | 8.6 |                     |                                           |
| 56.2         | 9.3                     | 18.7 | 28.1 | 37.4 | 46.8 | .2       | 0.2 | 1.1 | 2.1 | 3.0 | 4.0   | 4.9 | 5.8 | 6.8 | 7.7 | 8.7 |                     |                                           |
| 56.3         | 9.4                     | 18.8 | 28.1 | 37.5 | 46.9 | .3       | 0.3 | 1.2 | 2.2 | 3.1 | 4.0   | 5.0 | 5.9 | 6.9 | 7.8 | 8.8 |                     |                                           |
| 56.4         | 9.4                     | 18.8 | 28.2 | 37.6 | 47.0 | .4       | 0.4 | 1.3 | 2.3 | 3.2 | 4.1   | 5.1 | 6.0 | 7.0 | 7.9 | 8.9 |                     |                                           |

## Sight Reduction Individual Problems

RED D7. On 25 May your vessel's 1858 zone time DR position is latitude  $21^{\circ} 05' N$ , longitude  $143^{\circ} 27' E$ . At that time a sextant observation of the planet Venus was made. The sextant altitude is  $12^{\circ} 53.4'$  and the chronometer reads 08h 59m 15s. The index error is  $4.5'$  off the arc and the chronometer error is 1m 25s fast. Your height of eye is determined to be 55 feet. What is the azimuth ( $Z_n$ ) of the sight using the assumed position?

Answer:  $290.3^{\circ} T$ . Note that several steps are not required to answer the specific question posed but are shown here for training purposes.

- Step 1: Determine the GMT of the sight.  
 Chronometer time: 08h 59m 15s  
 Chronometer error: 1m 25s fast  
 Correct chronometer time: 08h 59m 15s – 1m 25s = 08:57:50  
 Ship time: 1858 zone time.  
 DR longitude:  $143^{\circ} 27' E$  corresponds to (-10 ZD)  
 GMT of sight: 08:57:50 GMT, 25 May

| r, M T    | ARIES    |                | VENUS -3.4 |  |
|-----------|----------|----------------|------------|--|
|           | GHA      | GHA            | Dec.       |  |
| 25 00     | 242 29.4 | 167 32.4 N23   | 09.5       |  |
| 01        | 257 31.9 | 182 31.6       | 09.9       |  |
| 02        | 272 34.3 | 197 30.7       | 10.3       |  |
| 03        | 287 36.8 | 212 29.9       | 10.8       |  |
| 04        | 302 39.3 | 227 29.0       | 11.2       |  |
| 05        | 317 41.7 | 242 28.2       | 11.6       |  |
| 06        | 332 44.2 | 257 27.4 N23   | 12.0       |  |
| 07        | 347 46.7 | 272 26.5       | 12.4       |  |
| 08        | 2 49.1   | 287 25.7       | 12.8       |  |
| M 09      | 17 51.6  | 302 24.8       | 13.2       |  |
| O 10      | 32 54.0  | 317 24.0       | 13.6       |  |
| N 11      | 47 56.5  | 332 23.1       | 14.0       |  |
| D 12      | 62 59.0  | 347 22.3 N23   | 14.4       |  |
| A 13      | 78 01.4  | 2 21.4         | 14.8       |  |
| Y 14      | 93 03.9  | 17 20.6        | 15.2       |  |
| 15        | 108 06.4 | 32 19.7        | 15.6       |  |
| 16        | 123 08.8 | 47 18.9        | 16.0       |  |
| 17        | 138 11.3 | 62 18.0        | 16.4       |  |
| 18        | 153 13.8 | 77 17.2 N23    | 16.8       |  |
| 19        | 168 16.2 | 92 16.4        | 17.2       |  |
| 20        | 183 18.7 | 107 15.5       | 17.6       |  |
| 21        | 198 21.2 | 122 14.7       | 18.0       |  |
| 22        | 213 23.6 | 137 13.8       | 18.4       |  |
| 23        | 228 26.1 | 152 13.0       | 18.8       |  |
| Mer. Pass | 7 44.8   | $\bar{v}$ -0.9 | d 0.4      |  |

- Step 2: Determine the apparent altitude ( $h_a$ ).  
 $h_s = 12^{\circ} 53.4'$  (Given)  
 Index error:  $4.5'$  off the arc (IC =  $+4.5'$ )  
 Height of eye: 55 ft (dip correction =  $-7.2'$ )  
 $h_a = 12^{\circ} 53.4' + 4.5' - 7.2' = \underline{12^{\circ} 50.7'}$

- Step 3: Determine observed altitude.  
 Apparent altitude:  $12^{\circ} 50.7'$   
 Apparent altitude correction:  $-4.2'$   
 Additional Venus correction:  $+0.1'$   
 Total main correction:  $-4.2' + 0.1' = -4.1'$   
 Observed altitude ( $h_o$ ):  $12^{\circ} 50.7' - 4.1' = \underline{12^{\circ} 46.6'}$

| m  | SUN PLANETS | ARIES      |         | MOON       |     | $\bar{v}$ or Corr <sup>n</sup> |      | $\bar{v}$ or Corr <sup>n</sup> |     |
|----|-------------|------------|---------|------------|-----|--------------------------------|------|--------------------------------|-----|
|    |             | $^{\circ}$ | $'$     | $^{\circ}$ | $'$ | $^{\circ}$                     | $'$  | $^{\circ}$                     | $'$ |
| 57 |             |            |         |            |     |                                |      |                                |     |
| 00 | 14 15.0     | 14 17.3    | 13 36.1 | 0.0        | 0.0 | 6.0                            | 5.8  |                                |     |
| 01 | 14 15.3     | 14 17.6    | 13 36.3 | 0.1        | 0.1 | 6.1                            | 5.8  |                                |     |
| 02 | 14 15.5     | 14 17.8    | 13 36.5 | 0.2        | 0.2 | 6.2                            | 5.9  |                                |     |
| 03 | 14 15.8     | 14 18.1    | 13 36.8 | 0.3        | 0.3 | 6.3                            | 6.0  |                                |     |
| 04 | 14 16.0     | 14 18.3    | 13 37.0 | 0.4        | 0.4 | 6.4                            | 6.1  |                                |     |
| 05 | 14 16.3     | 14 18.6    | 13 37.2 | 0.5        | 0.5 | 6.5                            | 6.2  |                                |     |
| 06 | 14 16.5     | 14 18.8    | 13 37.5 | 0.6        | 0.6 | 6.6                            | 6.3  |                                |     |
| 07 | 14 16.8     | 14 19.1    | 13 37.7 | 0.7        | 0.7 | 6.7                            | 6.4  |                                |     |
| 08 | 14 17.0     | 14 19.3    | 13 38.0 | 0.8        | 0.8 | 6.8                            | 6.5  |                                |     |
| 09 | 14 17.3     | 14 19.6    | 13 38.2 | 0.9        | 0.9 | 6.9                            | 6.6  |                                |     |
| 50 | 14 27.5     | 14 29.9    | 13 48.0 | 5.0        | 4.8 | 11.0                           | 10.5 |                                |     |
| 51 | 14 27.8     | 14 30.1    | 13 48.2 | 5.1        | 4.9 | 11.1                           | 10.6 |                                |     |
| 52 | 14 28.0     | 14 30.4    | 13 48.5 | 5.2        | 5.0 | 11.2                           | 10.7 |                                |     |
| 53 | 14 28.3     | 14 30.6    | 13 48.7 | 5.3        | 5.1 | 11.3                           | 10.8 |                                |     |
| 54 | 14 28.5     | 14 30.9    | 13 48.9 | 5.4        | 5.2 | 11.4                           | 10.9 |                                |     |

- Step 4: Determine the declination of Venus.  
 Declination (hours):  $N 23^{\circ} 12.8'$  (d number:  $+0.4'$ )  
 Declination (increment):  $+0.4'$   
 Declination (total):  $N 23^{\circ} 12.8' + 0.4' = \underline{N 23^{\circ} 13.2'}$

- Step 5: Determine the GHA of Venus.  
 GHA (hours):  $287^{\circ} 25.7'$  (v number:  $-0.9'$ )  
 GHA (increment):  $14^{\circ} 27.5'$   
 GHA (v correction):  $-0.9'$   
 GHA (total):  $287^{\circ} 25.7' + 14^{\circ} 27.5' - 0.9' = \underline{301^{\circ} 52.3'}$

## Sight Reduction Individual Problems

Step 6: Determine the assumed position of the ship.

DR latitude:  $21^{\circ} 05' \text{ N}$

Assumed latitude:  $21^{\circ} \text{ N}$

DR longitude:  $143^{\circ} 27' \text{ E}$

Assumed longitude (to ensure whole number of LHA):  $143^{\circ} 07.7' \text{ E}$

Step 7: Determine the LHA for Venus for the time of sight.

GHA (Venus):  $301^{\circ} 52.3'$

Assumed longitude:  $143^{\circ} 07.7' \text{ E}$

LHA (Moon):  $301^{\circ} 52.3' + 143^{\circ} 07.7' \text{ E } (-360^{\circ}) = 85^{\circ} \text{ (-west, +east)}$

Step 8: Entering publication HO229 with assumed latitude, declination, and LHA, retrieve the computed altitude (hc), altitude difference (d), and azimuth (z) for the assumed position.

Assumed latitude:  $21^{\circ} \text{ N}$

Declination:  $\text{N } 23^{\circ}$  (increments solved in step 9)

LHA:  $85^{\circ}$  (Same Pages)

HO 229 values:

Computed altitude (hc):  $12^{\circ} 24.7'$

Altitude difference (d):  $+ 18.2'$

Azimuth (z):  $69.9^{\circ}$

| 35°, 275° L.H.A. |         |       |      | LATITUDE SAME NAME AS DECLINATION |       |      |         | N. Lat. { L.H.A. greater than 180° ..... Zn=Z<br>L.H.A. less than 180° ..... Zn=360°-Z |      |         |       |      |         |       |      |         |       |      |         |       |      |         |       |      |    |   |   |     |   |   |      |    |  |  |  |
|------------------|---------|-------|------|-----------------------------------|-------|------|---------|----------------------------------------------------------------------------------------|------|---------|-------|------|---------|-------|------|---------|-------|------|---------|-------|------|---------|-------|------|----|---|---|-----|---|---|------|----|--|--|--|
| 15°              |         |       |      | 16°                               |       |      |         | 17°                                                                                    |      |         |       | 18°  |         |       |      | 19°     |       |      |         | 20°   |      |         |       | 21°  |    |   |   | 22° |   |   |      |    |  |  |  |
| Dec.             | Hc      | d     | Z    | Hc                                | d     | Z    | Hc      | d                                                                                      | Z    | Hc      | d     | Z    | Hc      | d     | Z    | Hc      | d     | Z    | Hc      | d     | Z    | Hc      | d     | Z    | Hc | d | Z | Hc  | d | Z | Dec. |    |  |  |  |
| 0                | 4 49.8  | +15.5 | 91.3 | 4 48.4                            | +16.5 | 91.4 | 4 46.9  | +17.5                                                                                  | 91.5 | 4 45.3  | +18.5 | 91.5 | 4 43.6  | +19.6 | 91.6 | 4 41.9  | +20.5 | 91.7 | 4 40.0  | +21.6 | 91.8 | 4 38.1  | +22.5 | 91.9 | 0  |   |   |     |   |   |      | 0  |  |  |  |
| 1                | 5 05.3  | +15.5 | 90.3 | 5 04.9                            | +16.5 | 90.4 | 5 04.4  | +17.5                                                                                  | 90.5 | 5 03.8  | +18.5 | 90.6 | 5 03.2  | +19.5 | 90.7 | 5 02.4  | +20.5 | 90.8 | 5 01.6  | +21.4 | 90.9 | 5 00.6  | +22.5 | 90.9 | 1  |   |   |     |   |   |      | 1  |  |  |  |
| 2                | 5 20.8  | +15.3 | 89.4 | 5 21.4                            | +16.4 | 89.5 | 5 21.9  | +17.4                                                                                  | 89.5 | 5 22.3  | +18.4 | 89.6 | 5 22.7  | +19.3 | 89.7 | 5 22.9  | +20.4 | 89.8 | 5 23.0  | +21.4 | 89.9 | 5 23.1  | +22.3 | 90.0 | 2  |   |   |     |   |   |      | 2  |  |  |  |
| 3                | 5 36.1  | +15.3 | 88.4 | 5 37.8                            | +16.2 | 88.5 | 5 39.3  | +17.3                                                                                  | 88.6 | 5 40.7  | +18.3 | 88.7 | 5 42.0  | +19.3 | 88.8 | 5 43.3  | +20.3 | 88.9 | 5 44.4  | +21.3 | 89.0 | 5 45.4  | +22.3 | 89.1 | 3  |   |   |     |   |   |      | 3  |  |  |  |
| 4                | 5 51.4  | +15.2 | 87.4 | 5 54.0                            | +16.2 | 87.5 | 5 56.6  | +17.2                                                                                  | 87.6 | 5 59.0  | +18.2 | 87.7 | 6 01.3  | +19.2 | 87.8 | 6 03.6  | +20.2 | 87.9 | 6 05.7  | +21.1 | 88.0 | 6 07.7  | +22.1 | 88.1 | 4  |   |   |     |   |   |      | 4  |  |  |  |
| 5                | 6 06.6  | +15.0 | 86.4 | 6 10.2                            | +16.1 | 86.5 | 6 13.8  | +17.1                                                                                  | 86.7 | 6 17.2  | +18.1 | 86.8 | 6 20.5  | +19.1 | 86.9 | 6 23.8  | +20.0 | 87.0 | 6 26.8  | +21.1 | 87.1 | 6 29.8  | +22.1 | 87.2 | 5  |   |   |     |   |   |      | 5  |  |  |  |
| 6                | 6 21.6  | +15.0 | 85.5 | 6 26.3                            | +16.0 | 85.6 | 6 30.9  | +16.9                                                                                  | 85.7 | 6 35.3  | +18.0 | 85.8 | 6 39.6  | +19.0 | 85.9 | 6 43.8  | +20.0 | 86.0 | 6 47.9  | +21.0 | 86.2 | 6 51.9  | +21.9 | 86.3 | 6  |   |   |     |   |   |      | 6  |  |  |  |
| 7                | 6 36.6  | +14.8 | 84.5 | 6 42.3                            | +15.8 | 84.6 | 6 47.8  | +16.9                                                                                  | 84.7 | 6 53.3  | +17.9 | 84.8 | 6 58.6  | +18.9 | 85.0 | 7 03.8  | +19.9 | 85.1 | 7 08.9  | +20.8 | 85.2 | 7 13.8  | +21.9 | 85.3 | 7  |   |   |     |   |   |      | 7  |  |  |  |
| 8                | 6 51.4  | +14.7 | 83.5 | 6 58.1                            | +15.7 | 83.6 | 7 04.7  | +16.7                                                                                  | 83.8 | 7 11.2  | +17.7 | 83.9 | 7 17.5  | +18.7 | 84.0 | 7 23.7  | +19.7 | 84.1 | 7 29.7  | +20.8 | 84.3 | 7 35.7  | +21.7 | 84.4 | 8  |   |   |     |   |   |      | 8  |  |  |  |
| 9                | 7 06.1  | +14.6 | 82.5 | 7 13.9                            | +15.6 | 82.7 | 7 21.4  | +16.7                                                                                  | 82.8 | 7 28.9  | +17.6 | 82.9 | 7 36.2  | +18.7 | 83.1 | 7 43.4  | +19.6 | 83.2 | 7 50.5  | +20.6 | 83.3 | 7 57.4  | +21.6 | 83.5 | 9  |   |   |     |   |   |      | 9  |  |  |  |
| 10               | 7 20.7  | +14.5 | 81.6 | 7 29.5                            | +15.4 | 81.7 | 7 38.1  | +16.5                                                                                  | 81.8 | 7 46.5  | +17.5 | 82.0 | 7 54.9  | +18.4 | 82.1 | 8 03.0  | +19.5 | 82.2 | 8 11.1  | +20.4 | 82.4 | 8 19.0  | +21.4 | 82.5 | 10 |   |   |     |   |   |      | 10 |  |  |  |
| 11               | 7 35.2  | +14.3 | 80.6 | 7 44.9                            | +15.4 | 80.7 | 7 54.6  | +16.3                                                                                  | 80.9 | 8 04.0  | +17.4 | 81.0 | 8 13.3  | +18.4 | 81.1 | 8 22.5  | +19.4 | 81.3 | 8 31.5  | +20.4 | 81.4 | 8 40.4  | +21.3 | 81.6 | 11 |   |   |     |   |   |      | 11 |  |  |  |
| 12               | 7 49.5  | +14.2 | 79.6 | 8 00.3                            | +15.2 | 79.7 | 8 10.9  | +16.2                                                                                  | 79.9 | 8 21.4  | +17.2 | 80.0 | 8 31.7  | +18.2 | 80.2 | 8 41.9  | +19.2 | 80.3 | 8 51.9  | +20.2 | 80.5 | 9 01.7  | +21.2 | 80.6 | 12 |   |   |     |   |   |      | 12 |  |  |  |
| 13               | 8 03.7  | +14.1 | 78.6 | 8 15.5                            | +15.1 | 78.8 | 8 27.1  | +16.1                                                                                  | 78.9 | 8 38.6  | +17.1 | 79.1 | 8 49.9  | +18.1 | 79.2 | 9 01.1  | +19.0 | 79.4 | 9 12.1  | +20.0 | 79.5 | 9 22.9  | +21.0 | 79.7 | 13 |   |   |     |   |   |      | 13 |  |  |  |
| 14               | 8 17.8  | +13.9 | 77.6 | 8 30.6                            | +14.9 | 77.8 | 8 43.2  | +15.9                                                                                  | 77.9 | 8 55.7  | +16.9 | 78.1 | 9 08.0  | +17.9 | 78.2 | 9 20.1  | +18.9 | 78.4 | 9 32.1  | +19.9 | 78.6 | 9 43.9  | +20.9 | 78.7 | 14 |   |   |     |   |   |      | 14 |  |  |  |
| 15               | 8 31.7  | +13.8 | 76.7 | 8 45.5                            | +14.8 | 76.8 | 8 59.1  | +15.8                                                                                  | 77.0 | 9 12.6  | +16.7 | 77.1 | 9 25.9  | +17.7 | 77.3 | 9 39.0  | +18.7 | 77.4 | 9 52.0  | +19.7 | 77.6 | 10 04.8 | +20.7 | 77.8 | 15 |   |   |     |   |   |      | 15 |  |  |  |
| 16               | 8 45.5  | +13.6 | 75.7 | 9 00.3                            | +14.6 | 75.8 | 9 14.9  | +15.6                                                                                  | 76.0 | 9 29.3  | +16.6 | 76.1 | 9 43.6  | +17.6 | 76.3 | 9 57.7  | +18.6 | 76.5 | 10 11.7 | +19.5 | 76.6 | 10 25.5 | +20.5 | 76.8 | 16 |   |   |     |   |   |      | 16 |  |  |  |
| 17               | 8 59.1  | +13.5 | 74.7 | 9 14.9                            | +14.4 | 74.8 | 9 30.5  | +15.4                                                                                  | 75.0 | 9 45.9  | +16.5 | 75.2 | 10 01.2 | +17.4 | 75.3 | 10 16.3 | +18.4 | 75.5 | 10 31.2 | +19.4 | 75.7 | 10 46.0 | +20.3 | 75.9 | 17 |   |   |     |   |   |      | 17 |  |  |  |
| 18               | 9 12.6  | +13.3 | 73.7 | 9 29.3                            | +14.3 | 73.9 | 9 45.9  | +15.3                                                                                  | 74.0 | 10 02.4 | +16.2 | 74.2 | 10 18.6 | +17.3 | 74.4 | 10 34.7 | +18.2 | 74.5 | 10 50.6 | +19.2 | 74.7 | 11 06.3 | +20.2 | 74.9 | 18 |   |   |     |   |   |      | 18 |  |  |  |
| 19               | 9 25.9  | +13.1 | 72.7 | 9 43.6                            | +14.1 | 72.9 | 10 01.2 | +15.1                                                                                  | 73.0 | 10 18.6 | +16.1 | 73.2 | 10 35.9 | +17.0 | 73.4 | 10 52.9 | +18.1 | 73.6 | 11 09.8 | +19.0 | 73.8 | 11 26.5 | +20.0 | 73.9 | 19 |   |   |     |   |   |      | 19 |  |  |  |
| 20               | 9 39.0  | +13.0 | 71.7 | 9 57.7                            | +14.0 | 71.9 | 10 16.3 | +14.9                                                                                  | 72.1 | 10 34.7 | +15.9 | 72.2 | 10 52.9 | +16.9 | 72.4 | 11 11.0 | +17.8 | 72.6 | 11 28.8 | +18.8 | 72.8 | 11 46.5 | +19.7 | 73.0 | 20 |   |   |     |   |   |      | 20 |  |  |  |
| 21               | 9 52.0  | +12.8 | 70.7 | 10 11.7                           | +13.8 | 70.9 | 10 31.2 | +14.8                                                                                  | 71.1 | 10 50.6 | +15.7 | 71.3 | 11 09.8 | +16.7 | 71.4 | 11 28.8 | +17.7 | 71.6 | 11 47.6 | +18.6 | 71.8 | 12 06.2 | +19.6 | 72.0 | 21 |   |   |     |   |   |      | 21 |  |  |  |
| 22               | 10 04.8 | +12.6 | 69.7 | 10 25.5                           | +13.5 | 69.9 | 10 46.0 | +14.5                                                                                  | 70.1 | 11 06.3 | +15.5 | 70.3 | 11 26.5 | +16.5 | 70.5 | 11 46.5 | +17.4 | 70.6 | 12 06.2 | +18.5 | 70.8 | 12 25.8 | +19.4 | 71.1 | 22 |   |   |     |   |   |      | 22 |  |  |  |
| 23               | 10 17.4 | +12.4 | 68.7 | 10 39.0                           | +13.4 | 68.9 | 11 00.5 | +14.4                                                                                  | 69.1 | 11 21.8 | +15.4 | 69.3 | 11 43.0 | +16.3 | 69.5 | 12 03.9 | +17.3 | 69.7 | 12 24.7 | +18.2 | 69.9 | 12 45.2 | +19.2 | 70.1 | 23 |   |   |     |   |   |      | 23 |  |  |  |
| 24               | 10 29.8 | +12.2 | 67.8 | 10 52.4                           | +13.2 | 67.9 | 11 14.9 | +14.2                                                                                  | 68.1 | 11 37.2 | +15.1 | 68.3 | 11 59.3 | +16.1 | 68.5 | 12 21.2 | +17.0 | 68.7 | 12 42.9 | +18.0 | 68.9 | 13 04.4 | +18.9 | 69.1 | 24 |   |   |     |   |   |      | 24 |  |  |  |

## Sight Reduction Individual Problems

Step 9: Determine the azimuth correction for the sight (to account for increments of declination ignored in step 8).

|                 | Base Value | Base Z | Next incremental Z | Difference in Z | Increment | Correction<br>(Diff Z x Increment) / 60 |
|-----------------|------------|--------|--------------------|-----------------|-----------|-----------------------------------------|
| Latitude – N    | 21°        | 69.9°  | -                  | -               | 00.0'     | 0                                       |
| Declination – N | 23°        | 69.9°  | 68.9°              | -1.0'           | 13.2'     | -0.2°                                   |
| LHA             | 85°        | 69.9°  | -                  | -               | 00.0'     | 0                                       |

Total correction = -0.2°

Step 10: Apply the correction to the base values to determine true azimuth.

Base azimuth: 69.9°

Correction: -0.2°

Corrected azimuth:  $69.9^\circ - 0.2^\circ = 69.7^\circ$

*Note - Check azimuth rules: if LHA less than 180°, then  $zn = 360^\circ - z$ .*

Corrected azimuth:  $360^\circ - 69.7^\circ = \mathbf{290.3^\circ T}$

Step 11: Determine the computed altitude (hc).

Tabular computed altitude: 12° 24.7'

Altitude difference (d): 18.2'

Declination: N 23° 13.2'

Declination increments: 13.2'

Altitude difference correction:

Tens: 2.2'

Units/decimals: 1.9'

Total correction:  $2.2' + 1.8' = +\mathbf{4.0'}$

Tabular hc: 12° 24.7'

Altitude difference correction: +4.0'

hc:  $12^\circ 24.7' + 4.0' = \mathbf{12^\circ 28.7'}$

Step 12: Determine the intercept (a).

Computed altitude (hc): 12° 28.7'

Observed altitude (ho): 12° 46.6'

Intercept (a):  $12^\circ 46.6' - 12^\circ 28.7' = \mathbf{17.9'}$

If ho is greater, intercept is towards.

| Dec.<br>Inc. | Altitude Difference (d) |     |     |     |      |          |     |     |     |     |       |     |     |     |     |     |  |  |  |
|--------------|-------------------------|-----|-----|-----|------|----------|-----|-----|-----|-----|-------|-----|-----|-----|-----|-----|--|--|--|
|              | Tens                    |     |     |     |      | Decimals |     |     |     |     | Units |     |     |     |     |     |  |  |  |
|              | 10'                     | 20' | 30' | 40' | 50'  | ↓        | 0'  | 1'  | 2'  | 3'  | 4'    | 5'  | 6'  | 7'  | 8'  | 9'  |  |  |  |
| 13.0         | 2.1                     | 4.3 | 6.5 | 8.6 | 10.8 | .0       | 0.0 | 0.2 | 0.4 | 0.7 | 0.9   | 1.1 | 1.3 | 1.6 | 1.8 | 2.0 |  |  |  |
| 13.1         | 2.2                     | 4.3 | 6.5 | 8.7 | 10.9 | .1       | 0.0 | 0.2 | 0.5 | 0.7 | 0.9   | 1.1 | 1.4 | 1.6 | 1.8 | 2.0 |  |  |  |
| 13.2         | 2.2                     | 4.4 | 6.6 | 8.8 | 11.0 | .2       | 0.0 | 0.3 | 0.5 | 0.7 | 0.9   | 1.2 | 1.4 | 1.6 | 1.8 | 2.1 |  |  |  |
| 13.3         | 2.2                     | 4.4 | 6.6 | 8.9 | 11.1 | .3       | 0.1 | 0.3 | 0.5 | 0.7 | 1.0   | 1.2 | 1.4 | 1.6 | 1.9 | 2.1 |  |  |  |
| 13.4         | 2.2                     | 4.5 | 6.7 | 8.9 | 11.2 | .4       | 0.1 | 0.3 | 0.5 | 0.8 | 1.0   | 1.2 | 1.4 | 1.7 | 1.9 | 2.1 |  |  |  |

## Sight Reduction (Individual) Problems

### Hs to Ho Problems

RED B1. On 2 January you observe the lower limb of the Sun at a sextant altitude (hs) of  $35^{\circ} 50.4'$ . The index error is  $0.8'$  on the arc. The height of eye is 24 feet. What is the observed altitude?

- a)  $35^{\circ} 50.3'$
- b)  $35^{\circ} 54.7'$
- c)  $35^{\circ} 59.7'$  - correct
- d)  $36^{\circ} 05.6'$

RED B2. You observe the lower limb of the Sun at a sextant altitude (hs) of  $28^{\circ} 24.7'$  on 17 May. The index error is  $1.5'$  off the arc. The height of eye is 86 feet. What is the observed altitude (ho)?

- a)  $28^{\circ} 29.7'$
- b)  $28^{\circ} 30.6'$
- c)  $28^{\circ} 31.5'$  - correct
- d)  $28^{\circ} 32.9'$

RED B3. On 29 June you observe the star Achernar at a sextant altitude (hs) of  $54^{\circ} 18.9'$ . The index error is  $4.7'$  off the arc. The height of eye is 58 feet. What is the observed altitude?

- a)  $54^{\circ} 06.1'$
- b)  $54^{\circ} 15.5'$  - correct
- c)  $54^{\circ} 31.5'$
- d)  $54^{\circ} 43.7'$

RED B4. At about 1436 GMT on 3 December, the lower limb of the Moon is observed. The sextant has an index error of  $2.5'$  on the arc. The height of eye is 32 feet. The sextant altitude (hs) is  $3^{\circ} 38.8'$ . What is the observed altitude?

- a)  $4^{\circ} 18.6'$
- b)  $4^{\circ} 29.1'$  - correct
- c)  $4^{\circ} 36.3'$
- d)  $4^{\circ} 42.2'$



### Sight Reduction of the Sun Problems

RED B5. At 0600 zone time on 24 July, your DR position is latitude  $22^{\circ} 37' \text{ N}$ , longitude  $32^{\circ} 45' \text{ W}$ . You are steering  $185^{\circ} \text{ T}$  at 20 knots. Determine the computed altitude (hc) and azimuth (zn) for an observation of the Sun's lower limb taken at 1030 ZT. At this time the chronometer reads 00h 30m 16s and is 31s slow.

- a) hc  $64^{\circ} 27.5'$ , zn  $092.3^{\circ} \text{ T}$
- b) hc  $64^{\circ} 30.8'$ , zn  $090.1^{\circ} \text{ T}$
- c) hc  $64^{\circ} 41.7'$ , zn  $087.8^{\circ} \text{ T}$  - correct
- d) hc  $64^{\circ} 44.2'$ , zn  $094.7^{\circ} \text{ T}$

RED B6. At 1000 zone time on 21 October, your DR position is latitude  $29^{\circ} 00' \text{ N}$ , longitude  $134^{\circ} 40' \text{ E}$ . Determine the computed altitude (hc) of the Sun for the assumed position (AP) nearest to the above given latitude and longitude, given a chronometer time of 01h 00m 00s.

- a) hc  $42^{\circ} 30.6'$
- b) hc  $42^{\circ} 32.1'$
- c) hc  $42^{\circ} 34.2'$
- d) hc  $42^{\circ} 35.7'$  - correct

RED B7. On 10 January at 0550 zone time, morning stars were observed, and the vessel's position was determined to be latitude  $25^{\circ} 16' \text{ N}$ , longitude  $123^{\circ} 18' \text{ W}$ . Your vessel is steaming at 22 knots on a course of  $295^{\circ} \text{ T}$ . A sextant observation of the Sun's lower limb is made at 0915 zone time. The chronometer reads 05h 14m 02s and the sextant altitude is  $24^{\circ} 00.7'$ . The index error is  $2.6'$  off the arc, and the chronometer error is 01m 34s slow. Your height of eye on the bridge is 55 feet. What is the azimuth (zn) of this sight using the assumed position?

- a)  $127.8^{\circ} \text{ T}$
- b)  $129.8^{\circ} \text{ T}$
- c)  $131.4^{\circ} \text{ T}$  – correct, note official CG correct answer is  $131.9^{\circ} \text{ T}$  in the databank.
- d)  $133.6^{\circ} \text{ T}$

RED B8. On 12 April at 0515 zone time, morning stars were observed and the vessel's position was determined to be latitude  $21^{\circ} 05' \text{ S}$ , longitude  $16^{\circ} 30' \text{ W}$ . Your vessel is steaming at 19 knots on course  $278^{\circ} \text{ T}$ . A sextant observation of the Sun's lower limb is made at 0930 zone time. The chronometer reads 10h 28m 25s and the sextant altitude (hs) is  $40^{\circ} 15.9'$ . The index error is  $2.5'$  off the arc and the chronometer error is 2m 15s slow. Your height of eye on the bridge is 57 feet. What are the intercept (a), and azimuth (zn) from the assumed position?

- a) zn =  $057.7^{\circ} \text{ T}$ , a =  $15.4'$  towards
- b) zn =  $057.0^{\circ} \text{ T}$ , a =  $17.7'$  away - correct
- c) zn =  $122.3^{\circ} \text{ T}$ , a =  $17.7'$  away
- d) zn =  $123.0^{\circ} \text{ T}$ , a =  $22.7'$  away

RED B9. On 16 June at 0612 zone time, morning stars were observed. The vessel's position was latitude  $27^{\circ} 23.0'$  S, longitude  $56^{\circ} 22.0'$  W. The vessel is steaming at 16 knots on a course of  $212^{\circ}$  T. A sextant observation of the Sun's lower limb is made at 0850 zone time. The chronometer reads 00h 53m 19s and the sextant altitude (hs) is  $22^{\circ} 58.6'$ . The index error is  $2.0'$  off the arc and the chronometer error is 02m 43s fast. Your height of eye is 61 feet. What is the azimuth (zn) of the sight using the assumed position?

- a)  $044.3^{\circ}$  T - correct
- b)  $052.6^{\circ}$  T
- c)  $136.1^{\circ}$  T
- d)  $148.4^{\circ}$  T

RED B10. On 8 August at 0545 zone time morning stars were observed and the vessel's position was determined to be latitude  $26^{\circ} 16'$  S, longitude  $94^{\circ} 16'$  E. Your vessel is steaming at 20 knots on a course of  $346^{\circ}$  T. A sextant observation of the Sun's lower limb is made at 0905 zone time. The chronometer reads 03h 02m 52s, and the sextant altitude (hs) is  $38^{\circ} 07.5'$ . The index error is  $5.2'$  off the arc, and the chronometer error is 2m 17s slow. Your height of eye on the bridge is 72 feet. What is the observed altitude (ho) and azimuth (zn) of the sight using the assumed position?

- a)  $38^{\circ} 19.4'$ ,  $048.4^{\circ}$  T - correct
- b)  $38^{\circ} 19.4'$ ,  $131.6^{\circ}$  T
- c)  $38^{\circ} 54.9'$ ,  $048.4^{\circ}$  T
- d)  $38^{\circ} 54.9'$ ,  $131.6^{\circ}$  T

RED B11. On 21 November at 0430 zone time, morning stars were observed, and the vessel's position was latitude  $22^{\circ} 14.0'$  S, longitude  $79^{\circ} 23.0'$  E. Your vessel is steaming at 14.5 knots on a course of  $246^{\circ}$  T. A sextant observation of the Sun's lower limb is made at 0816 zone time. The chronometer reads 03h 14m 16s, and the sextant altitude (hs) is  $44^{\circ} 29.2'$ . The index error is  $1.0'$  on the arc and the chronometer error is 01m 47s slow. Your height of eye is 61 feet. What is the azimuth (zn) and intercept (a) of this sight using the assumed position?

- a) zn =  $084.2^{\circ}$  T, a =  $6.6'$  away
- b) zn =  $084.2^{\circ}$  T, a =  $6.6'$  towards
- c) zn =  $095.6^{\circ}$  T, a =  $6.6'$  away
- d) zn =  $095.6^{\circ}$  T, a =  $6.6'$  towards - correct

Sight Reduction of the Moon, Stars and Planets Problems (very few problems in database)

RED B12. On 22 July, at 0720 ZT in your DR position latitude  $20^{\circ} 38.2' \text{N}$ , longitude  $87^{\circ} 16.0' \text{W}$ , you observe the Moon's lower limb. The sextant altitude ( $H_s$ ) is  $38^{\circ} 32.6'$  and the chronometer reads 01h 18m 14s. The chronometer is 01m 28s slow and the index error is  $3.1'$  off the arc. The height of eye is 68 feet. What is the azimuth ( $Z_n$ ) and intercept ( $a$ ) of this sight from the assumed position?

- a)  $Z_n 291.4^{\circ}$ ,  $a 5.2' \text{A}$
- b)  $Z_n 111.4^{\circ}$ ,  $a 8.7' \text{A}$
- c)  **$Z_n 248.6^{\circ}$ ,  $a 5.0' \text{T}$  - correct**
- d)  $Z_n 068.6^{\circ}$ ,  $a 6.5' \text{T}$

RED B13. On 25 May your vessel's 1917 zone time position is latitude  $24^{\circ} 16' \text{N}$ , longitude  $17^{\circ} 26' \text{W}$ . At that time a sextant observation of the planet Saturn was made. The sextant altitude is  $63^{\circ} 05.1'$  and the chronometer reads 08h 18m 24s. The index error is  $4.5'$  off the arc and the chronometer error is 1m 05s fast. Your height of eye is determined to be 62 feet. What is the azimuth ( $z_n$ ) of the sight using the assumed position?

- e)  $143.8^{\circ} \text{T}$
- f)  **$147.3^{\circ} \text{T}$  - correct**
- g)  $148.7^{\circ} \text{T}$
- h)  $149.9^{\circ} \text{T}$

RED B14. On 26 May your vessel's 1906 zone time position is latitude  $27^{\circ} 16' \text{N}$ , longitude  $24^{\circ} 37' \text{W}$ . At that time a sextant observation of the planet Jupiter was made. The sextant altitude is  $63^{\circ} 27.6'$  and the chronometer reads 09h 05m 16s. The index error is  $5.2'$  on the arc and the chronometer error is 1m 25s slow. Your height of eye is determined to be 52.6 feet. What is the azimuth ( $z_n$ ) of the sight using the assumed position?

- a)  $011.3^{\circ} \text{T}$
- b)  **$168.7^{\circ} \text{T}$  - correct**
- c)  $191.3^{\circ} \text{T}$
- d)  $348.7^{\circ} \text{T}$

RED B15. On 28 April your vessel's 0515 zone time position is latitude  $23^{\circ} 26' \text{S}$ , longitude  $95^{\circ} 30' \text{E}$ . At that time a sextant observation of Rigil Kentaurus was made. The  $H_o$  is  $24^{\circ} 51.4'$ . Your chronometer reads 11h 16m 36s and is 01m 18s fast. What is the intercept ( $a$ ) based on the assumed position?

- a) 30.9 miles
- b) 32.3 miles
- c) 33.1 miles
- d) **34.4 miles - correct**



## **Sight Reduction (Running Fix) Problems**



## Celestial Fix and Running Fix Problems

### Sun Problems

FIX D1. On 8 February, your 0800 zone time position was latitude  $28^{\circ} 55.0' S$ , longitude  $52^{\circ} 27' W$ . Your vessel was steaming on course  $036^{\circ} T$  at a speed of 19 knots. An observation of the Sun's lower limb was made at 0938 zone time. The chronometer read 12h 37m 23s and was slow 01m 24s. The observed altitude (ho) was  $45^{\circ} 29.2'$ . Local apparent noon (LAN) occurred at 1240 zone time. The observed altitude (ho) was  $77^{\circ} 10.5'$ . What was the longitude of your 1200 zone time running fix?

Answer:  $51^{\circ} 36.0' W$

Step 1: Determine the GMT of the morning Sun sight.

Chronometer time: 12h 37m 23s

Chronometer error: 01m 24s slow

Correct chronometer time: 12h 37m 23s + 01m 24s = 12h 38m 47s

Ship time of sight: 0938 ZT

DR longitude:  $52^{\circ} 27' W$  corresponds to (+3 ZD)

GMT of sight: 12:38:47 GMT, 8 February

Step 2: Advance the original fix location to the morning Sun sight. Note this solution uses a plotting sheet, but the position may also be advanced by mid-latitude sailing.

Original fix time: 0800 ZT or 1100 GMT

Original fix position:  $28^{\circ} 55' S$ ,  $52^{\circ} 27' W$ .

Morning observation time: 0938 ZT or 1238 GMT

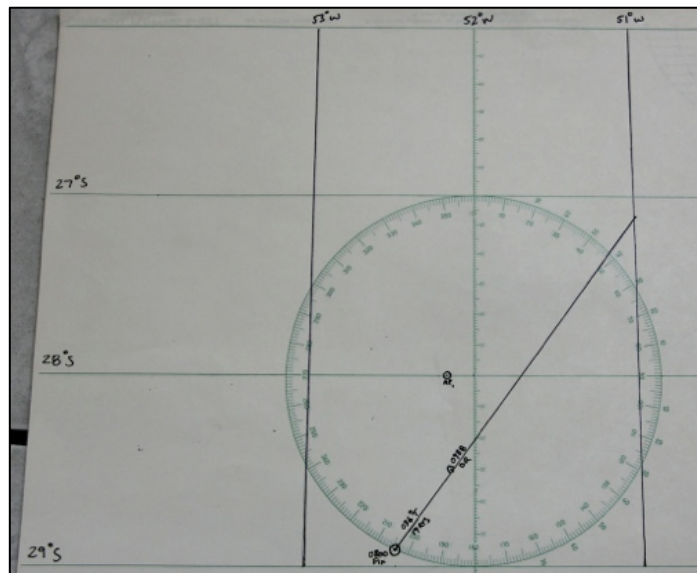
Course and speed:  $036^{\circ} T$  at 19 knots

Time underway: 0800 ZT – 0938 ZT = 1 hours, 38 minutes, or 1.6 hrs

Distance travelled: 1.6 hours for 19 knots = 31.0 miles covered

Morning DR position (original fix advanced 31 miles in direction  $036^{\circ}$ ):

$28^{\circ} 30' S$ ,  $52^{\circ} 06' W$



## Celestial Fix and Running Fix Problems

- Step 3: Determine the observed altitude of the morning Sun sight.  
 $h_o: 45^\circ 29.2'$  (Given)
- Step 4: Determine the declination of the Sun for the morning Sun sight.  
 Declination (hours):  $S 14^\circ 55.5'$  (d number -0.8)  
 Declination (increments):  $- 0.5'$   
 Declination (total):  $S 14^\circ 55.0'$
- Step 5: Determine the GHA of the Sun for the morning Sun sight.  
 GHA (hours):  $356^\circ 26.4'$   
 GHA (increments):  $9^\circ 41.8'$   
 GHA (total):  $366^\circ 08.2'$  ( $-360^\circ$ ) =  $6^\circ 08.2'$
- Step 6: Determine the assumed position of the ship.  
 DR latitude:  $28^\circ 30' S$   
 Assumed latitude:  $28^\circ S$   
 DR longitude:  $52^\circ 06' W$   
 Assumed longitude (to ensure whole number of LHA):  $52^\circ 08.2' W$
- Step 7: Determine the LHA of the Sun for the morning Sun sight.  
 GHA (Sun):  $6^\circ 08.2' W$   
 Assumed longitude:  $52^\circ 08.2' W$   
 LHA  $6^\circ 08.2' (+360^\circ) - 52^\circ 08.2' W = 314^\circ$  (subtract west, add east)

| G.M.T. | SUN       |      |      |      |
|--------|-----------|------|------|------|
|        | G.H.A.    |      | Dec. |      |
| 8 00   | 176       | 26.7 | S15  | 05.0 |
| 01     | 191       | 26.7 |      | 04.2 |
| 02     | 206       | 26.7 |      | 03.4 |
| 03     | 221       | 26.7 | ..   | 02.7 |
| 04     | 236       | 26.6 |      | 01.9 |
| 05     | 251       | 26.6 |      | 01.1 |
| 06     | 266       | 26.6 | S15  | 00.3 |
| 07     | 281       | 26.5 | 14   | 59.5 |
| 08     | 296       | 26.5 |      | 58.7 |
| S 09   | 311       | 26.5 | ..   | 57.9 |
| U 10   | 326       | 26.5 |      | 57.1 |
| N 11   | 341       | 26.4 |      | 56.3 |
| D 12   | 356       | 26.4 | S14  | 55.5 |
| A 13   | 11        | 26.4 |      | 54.7 |
| Y 14   | 26        | 26.4 | ..   | 53.9 |
| 15     | 41        | 26.4 |      | 53.1 |
| 16     | 56        | 26.3 |      | 52.3 |
| 17     | 71        | 26.3 |      | 51.5 |
| 18     | 86        | 26.3 | S14  | 50.8 |
| 19     | 101       | 26.3 |      | 50.0 |
| 20     | 116       | 26.2 |      | 49.2 |
| 21     | 131       | 26.2 | ..   | 48.4 |
| 22     | 146       | 26.2 |      | 47.6 |
| 23     | 161       | 26.2 |      | 46.8 |
|        | S.D. 16.2 |      | d    | 0.8  |

| <sup>m</sup> | SUN     | ARIES  | MOON   | <sup>v</sup><br>or<br>d | <sup>v</sup><br>or<br>d | <sup>v</sup><br>or<br>d |
|--------------|---------|--------|--------|-------------------------|-------------------------|-------------------------|
| 38           | PLANETS |        |        |                         |                         |                         |
| 00           | 9 30-0  | 9 31-6 | 9 04-0 | 0-0 0-0                 | 6-0 3-9                 | 12-0 7-7                |
| 01           | 9 30-3  | 9 31-8 | 9 04-3 | 0-1 0-1                 | 6-1 3-9                 | 12-1 7-8                |
| 02           | 9 30-5  | 9 32-1 | 9 04-5 | 0-2 0-1                 | 6-2 4-0                 | 12-2 7-8                |
| 03           | 9 30-8  | 9 32-3 | 9 04-7 | 0-3 0-2                 | 6-3 4-0                 | 12-3 7-9                |
| 04           | 9 31-0  | 9 32-6 | 9 05-0 | 0-4 0-3                 | 6-4 4-1                 | 12-4 8-0                |
| 05           | 9 31-3  | 9 32-8 | 9 05-2 | 0-5 0-3                 | 6-5 4-2                 | 12-5 8-0                |
| 06           | 9 31-5  | 9 33-1 | 9 05-5 | 0-6 0-4                 | 6-6 4-2                 | 12-6 8-1                |
| 07           | 9 31-8  | 9 33-3 | 9 05-7 | 0-7 0-4                 | 6-7 4-3                 | 12-7 8-1                |
| 08           | 9 32-0  | 9 33-6 | 9 05-9 | 0-8 0-5                 | 6-8 4-4                 | 12-8 8-2                |
| 09           | 9 32-3  | 9 33-8 | 9 06-2 | 0-9 0-6                 | 6-9 4-4                 | 12-9 8-3                |
| 45           | 9 41-3  | 9 42-8 | 9 14-8 | 4-5 2-9                 | 10-5 6-7                | 16-5 10-6               |
| 46           | 9 41-5  | 9 43-1 | 9 15-0 | 4-6 3-0                 | 10-6 6-8                | 16-6 10-7               |
| 47           | 9 41-8  | 9 43-3 | 9 15-2 | 4-7 3-0                 | 10-7 6-9                | 16-7 10-7               |
| 48           | 9 42-0  | 9 43-6 | 9 15-5 | 4-8 3-1                 | 10-8 6-9                | 16-8 10-8               |
| 49           | 9 42-3  | 9 43-8 | 9 15-7 | 4-9 3-1                 | 10-9 7-0                | 16-9 10-8               |



# Celestial Fix and Running Fix Problems

Step 8: Entering publication HO229 with assumed latitude, declination, and LHA, retrieve the computed altitude (hc), altitude difference (d), and azimuth (z) for the assumed position.

Assumed latitude: 28° S

Declination: S 14° (increments solved in step 9)

LHA: 314° (Same Pages)

HO 229 values:

Computed altitude (hc): 45° 07.8'

Altitude difference (d): +25.7'

Azimuth (z): 98.4° T

| 46°, 314° L.H.A. |         |       |       |         |       |       |         |       |       | LATITUDE SAME NAME AS DECLINATION |       |       |         |       |       |         |       |       |         | N. Lat. $\begin{cases} \text{L.H.A. greater than } 180^\circ \dots \text{Zn}=\text{Z} \\ \text{L.H.A. less than } 180^\circ \dots \text{Zn}=360^\circ-\text{Z} \end{cases}$ |       |         |       |       |      |  |  |  |  |
|------------------|---------|-------|-------|---------|-------|-------|---------|-------|-------|-----------------------------------|-------|-------|---------|-------|-------|---------|-------|-------|---------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------|---------|-------|-------|------|--|--|--|--|
| Dec.             | 23°     |       |       | 24°     |       |       | 25°     |       |       | 26°                               |       |       | 27°     |       |       | 28°     |       |       | 29°     |                                                                                                                                                                             |       | 30°     |       |       | Dec. |  |  |  |  |
|                  | Hc      | d     | Z     | Hc      | d     | Z     | Hc      | d     | Z     | Hc                                | d     | Z     | Hc      | d     | Z     | Hc      | d     | Z     | Hc      | d                                                                                                                                                                           | Z     | Hc      | d     | Z     |      |  |  |  |  |
| 0                | 39 45.0 | +30.2 | 110.7 | 39 23.4 | +31.3 | 111.4 | 39 01.1 | +32.4 | 112.2 | 38 38.1                           | +33.4 | 112.9 | 38 14.3 | +34.5 | 113.7 | 37 49.9 | +35.4 | 114.4 | 37 24.8 | +36.4                                                                                                                                                                       | 115.1 | 36 59.0 | +37.4 | 115.8 | 0    |  |  |  |  |
| 1                | 40 15.2 | +29.5 | 109.5 | 39 54.7 | +30.6 | 110.3 | 39 33.5 | +31.7 | 111.1 | 39 11.5                           | +32.8 | 111.9 | 38 48.8 | +33.8 | 112.6 | 38 25.3 | +34.8 | 113.4 | 38 01.2 | +35.8                                                                                                                                                                       | 114.1 | 37 36.4 | +36.8 | 114.8 | 1    |  |  |  |  |
| 2                | 40 44.7 | +28.8 | 108.4 | 40 25.3 | +30.0 | 109.2 | 40 05.2 | +31.1 | 110.0 | 39 44.3                           | +32.1 | 110.8 | 39 22.6 | +33.2 | 111.6 | 39 00.2 | +34.3 | 112.3 | 38 37.0 | +35.3                                                                                                                                                                       | 113.1 | 38 13.2 | +36.3 | 113.8 | 2    |  |  |  |  |
| 3                | 41 13.5 | +28.1 | 107.2 | 40 55.3 | +29.2 | 108.1 | 40 36.3 | +30.4 | 108.9 | 40 16.4                           | +31.6 | 109.7 | 39 55.8 | +32.7 | 110.5 | 39 34.5 | +33.6 | 111.3 | 39 12.3 | +34.6                                                                                                                                                                       | 112.0 | 38 49.5 | +35.7 | 112.8 | 3    |  |  |  |  |
| 4                | 41 41.6 | +27.3 | 106.1 | 41 24.5 | +28.6 | 106.9 | 41 06.7 | +29.7 | 107.7 | 40 48.0                           | +30.8 | 108.6 | 40 28.5 | +31.9 | 109.4 | 40 08.1 | +33.1 | 110.2 | 39 47.1 | +34.1                                                                                                                                                                       | 111.0 | 39 25.2 | +35.2 | 111.7 | 4    |  |  |  |  |
| 5                | 42 08.9 | +26.6 | 104.9 | 41 53.1 | +27.8 | 105.7 | 41 36.4 | +29.0 | 106.6 | 41 18.8                           | +30.2 | 107.4 | 41 00.4 | +31.4 | 108.3 | 40 41.2 | +32.5 | 109.1 | 40 21.2 | +33.6                                                                                                                                                                       | 109.9 | 40 00.4 | +34.6 | 110.7 | 5    |  |  |  |  |
| 6                | 42 35.5 | +25.9 | 103.6 | 42 20.9 | +27.1 | 104.5 | 42 05.4 | +28.3 | 105.4 | 41 49.0                           | +29.5 | 106.3 | 41 31.8 | +30.6 | 107.1 | 41 13.7 | +31.8 | 108.0 | 40 54.8 | +32.9                                                                                                                                                                       | 108.8 | 40 35.0 | +34.0 | 109.6 | 6    |  |  |  |  |
| 7                | 43 01.4 | +25.0 | 102.4 | 42 48.0 | +26.3 | 103.3 | 42 33.7 | +27.6 | 104.2 | 42 18.5                           | +28.8 | 105.1 | 42 02.4 | +30.0 | 106.0 | 41 45.5 | +31.1 | 106.8 | 41 27.7 | +32.3                                                                                                                                                                       | 107.7 | 41 09.0 | +33.4 | 108.5 | 7    |  |  |  |  |
| 8                | 43 26.4 | +24.2 | 101.2 | 43 14.3 | +25.5 | 102.1 | 43 01.3 | +26.7 | 103.0 | 42 47.3                           | +28.0 | 103.9 | 42 32.4 | +29.2 | 104.8 | 42 16.6 | +30.4 | 105.7 | 42 00.0 | +31.6                                                                                                                                                                       | 106.6 | 41 42.4 | +32.8 | 107.4 | 8    |  |  |  |  |
| 9                | 43 50.6 | +23.4 | 99.9  | 43 39.8 | +24.7 | 100.8 | 43 28.0 | +26.0 | 101.8 | 43 15.3                           | +27.2 | 102.7 | 43 01.6 | +28.5 | 103.6 | 42 47.0 | +29.7 | 104.5 | 42 31.6 | +30.8                                                                                                                                                                       | 105.4 | 42 15.2 | +32.0 | 106.3 | 9    |  |  |  |  |
| 10               | 44 14.0 | +22.4 | 98.6  | 44 04.5 | +23.8 | 99.6  | 43 54.0 | +25.1 | 100.5 | 43 42.5                           | +26.5 | 101.5 | 43 30.1 | +27.7 | 102.4 | 43 16.7 | +29.0 | 103.3 | 43 02.4 | +30.2                                                                                                                                                                       | 104.2 | 42 47.2 | +31.4 | 105.1 | 10   |  |  |  |  |
| 11               | 44 36.4 | +21.6 | 97.3  | 44 28.3 | +22.9 | 98.3  | 44 19.1 | +24.3 | 99.3  | 44 09.0                           | +25.6 | 100.2 | 43 57.8 | +26.9 | 101.2 | 43 45.7 | +28.2 | 102.1 | 43 32.6 | +29.4                                                                                                                                                                       | 103.1 | 43 18.6 | +30.6 | 104.0 | 11   |  |  |  |  |
| 12               | 44 58.0 | +20.7 | 96.0  | 44 51.2 | +22.1 | 97.0  | 44 43.4 | +23.4 | 98.0  | 44 34.6                           | +24.7 | 99.0  | 44 24.7 | +26.1 | 99.9  | 44 13.9 | +27.3 | 100.9 | 44 02.0 | +28.7                                                                                                                                                                       | 101.8 | 43 49.2 | +29.9 | 102.8 | 12   |  |  |  |  |
| 13               | 45 18.7 | +19.7 | 94.7  | 45 13.3 | +21.1 | 95.7  | 45 06.8 | +22.5 | 96.7  | 44 59.3                           | +23.9 | 97.7  | 44 50.8 | +25.2 | 98.7  | 44 41.2 | +26.6 | 99.6  | 44 30.7 | +27.8                                                                                                                                                                       | 100.6 | 44 19.1 | +29.1 | 101.6 | 13   |  |  |  |  |
| 14               | 45 38.4 | +18.8 | 93.3  | 45 34.4 | +20.2 | 94.4  | 45 29.3 | +21.6 | 95.4  | 45 23.2                           | +23.0 | 96.4  | 45 16.0 | +24.3 | 97.4  | 45 07.8 | +25.7 | 98.4  | 44 58.5 | +27.0                                                                                                                                                                       | 99.4  | 44 48.2 | +28.3 | 100.4 | 14   |  |  |  |  |
| 15               | 45 57.2 | +17.8 | 92.0  | 45 54.6 | +19.2 | 93.0  | 45 50.9 | +20.7 | 94.0  | 45 46.2                           | +22.0 | 95.1  | 45 40.3 | +23.5 | 96.1  | 45 33.5 | +24.8 | 97.1  | 45 25.5 | +26.2                                                                                                                                                                       | 98.1  | 45 16.5 | +27.5 | 99.1  | 15   |  |  |  |  |
| 16               | 46 15.0 | +16.8 | 90.6  | 46 13.8 | +18.3 | 91.6  | 46 11.6 | +19.7 | 92.7  | 46 08.2                           | +21.1 | 93.7  | 46 03.8 | +22.5 | 94.8  | 45 58.3 | +23.9 | 95.8  | 45 51.7 | +25.3                                                                                                                                                                       | 96.8  | 45 44.0 | +26.7 | 97.8  | 16   |  |  |  |  |
| 17               | 46 31.8 | +15.8 | 89.2  | 46 32.1 | +17.2 | 90.3  | 46 31.3 | +18.7 | 91.3  | 46 29.3                           | +20.2 | 92.4  | 46 26.3 | +21.6 | 93.4  | 46 22.2 | +23.0 | 94.5  | 46 17.0 | +24.3                                                                                                                                                                       | 95.5  | 46 10.7 | +25.7 | 96.5  | 17   |  |  |  |  |
| 18               | 46 47.6 | +14.7 | 87.8  | 46 49.3 | +16.2 | 88.9  | 46 50.0 | +17.6 | 89.9  | 46 48.5                           | +19.1 | 91.0  | 46 47.9 | +20.6 | 92.1  | 46 45.2 | +22.0 | 93.1  | 46 41.3 | +23.5                                                                                                                                                                       | 94.2  | 46 36.4 | +24.8 | 95.2  | 18   |  |  |  |  |
| 19               | 47 02.3 | +13.7 | 86.4  | 47 05.5 | +15.2 | 87.5  | 47 07.6 | +16.7 | 88.5  | 47 08.6                           | +18.1 | 89.6  | 47 08.5 | +19.5 | 90.7  | 47 07.2 | +21.0 | 91.8  | 47 04.8 | +22.4                                                                                                                                                                       | 92.8  | 47 01.2 | +23.9 | 93.9  | 19   |  |  |  |  |

## Celestial Fix and Running Fix Problems

- Step 9: Determine the azimuth correction for the sight (to account for increments of declination ignored in step 8).

By increasing the value of each argument by 1 whole increment, triple interpolate for the exact values of azimuth (for detailed instructions see Part 14).

|                 | Base Value | Base Z | Next incremental Z | Difference in Z | Increment | Correction<br>(Diff Z x Increment) / 60 |
|-----------------|------------|--------|--------------------|-----------------|-----------|-----------------------------------------|
| Latitude – S    | 28°        | 98.4°  | -                  | -               | 00.0'     | 0                                       |
| Declination – S | 14°        | 98.4°  | 97.1°              | -1.3°           | 55.0'     | -1.19°                                  |
| LHA             | 314°       | 98.4°  | -                  | -               | 00.0'     | 0                                       |

Total correction = -1.2°

- Step 10: Apply the correction to the base values to determine true azimuth.

Base azimuth: 98.4°

Correction: -1.2°

Corrected azimuth: 97.2°

*Note - Check azimuth rules: if LHA greater than 180°, then  $zn = 180^\circ z$ .*

Corrected azimuth:  $180^\circ - 97.2^\circ = \underline{82.8^\circ T}$

- Step 11: Determine the computed altitude.

Tabular computed altitude (hc): 45° 07.8'

Altitude difference (d): +25.7'

Declination: S 14° 55.0'

Declination increments: 55.0'

Altitude difference correction:

Tens: +18.3'

Units/decimals: +5.2'

Total correction: +23.5'

Tabular hc: 45° 07.8'

Alt correction: +23.5'

hc: 45° 31.3'

|              |     | Altitude Difference (d) |      |      |      |     |          |     |     |     |     |       |     |     |     |     |     |  |  |
|--------------|-----|-------------------------|------|------|------|-----|----------|-----|-----|-----|-----|-------|-----|-----|-----|-----|-----|--|--|
| Dec.<br>Inc. |     | Tens                    |      |      |      |     | Decimals |     |     |     |     | Units |     |     |     |     |     |  |  |
|              |     | 10'                     | 20'  | 30'  | 40'  | 50' | 0        | 1   | 2   | 3   | 4   | 5     | 6   | 7   | 8   | 9   |     |  |  |
| 55.0         | 9.1 | 18.3                    | 27.5 | 36.6 | 45.8 |     | .0       | 0.0 | 0.9 | 1.8 | 2.8 | 3.7   | 4.6 | 5.5 | 6.5 | 7.4 | 8.3 |  |  |
| 55.1         | 9.2 | 18.3                    | 27.5 | 36.7 | 45.9 |     | .1       | 0.1 | 1.0 | 1.9 | 2.9 | 3.8   | 4.7 | 5.6 | 6.6 | 7.5 | 8.4 |  |  |
| 55.2         | 9.2 | 18.4                    | 27.6 | 36.8 | 46.0 |     | .2       | 0.2 | 1.1 | 2.0 | 3.0 | 3.9   | 4.8 | 5.7 | 6.7 | 7.6 | 8.5 |  |  |
| 55.3         | 9.2 | 18.4                    | 27.6 | 36.9 | 46.1 |     | .3       | 0.3 | 1.2 | 2.1 | 3.1 | 4.0   | 4.9 | 5.8 | 6.8 | 7.7 | 8.6 |  |  |
| 55.4         | 9.2 | 18.5                    | 27.7 | 36.9 | 46.2 |     | .4       | 0.4 | 1.3 | 2.2 | 3.1 | 4.1   | 5.0 | 5.9 | 6.8 | 7.8 | 8.7 |  |  |
| 55.5         | 9.3 | 18.5                    | 27.8 | 37.0 | 46.3 |     | .5       | 0.5 | 1.4 | 2.3 | 3.2 | 4.2   | 5.1 | 6.0 | 6.9 | 7.9 | 8.8 |  |  |
| 55.6         | 9.3 | 18.5                    | 27.8 | 37.1 | 46.3 |     | .6       | 0.6 | 1.5 | 2.4 | 3.3 | 4.3   | 5.2 | 6.1 | 7.0 | 8.0 | 8.9 |  |  |
| 55.7         | 9.3 | 18.6                    | 27.9 | 37.2 | 46.4 |     | .7       | 0.6 | 1.6 | 2.5 | 3.4 | 4.3   | 5.3 | 6.2 | 7.1 | 8.0 | 9.0 |  |  |
| 55.8         | 9.3 | 18.6                    | 27.9 | 37.2 | 46.5 |     | .8       | 0.7 | 1.7 | 2.6 | 3.5 | 4.4   | 5.4 | 6.3 | 7.2 | 8.1 | 9.1 |  |  |
| 55.9         | 9.4 | 18.7                    | 28.0 | 37.3 | 46.6 |     | .9       | 0.8 | 1.8 | 2.7 | 3.6 | 4.5   | 5.5 | 6.4 | 7.3 | 8.2 | 9.2 |  |  |

- Step 12: Determine the intercept (a).

Observed altitude: 45° 29.2'

Computed altitude: 45° 31.3'

Intercept (a):  $45^\circ 31.3' - 45^\circ 29.2' = \underline{2.1'}$

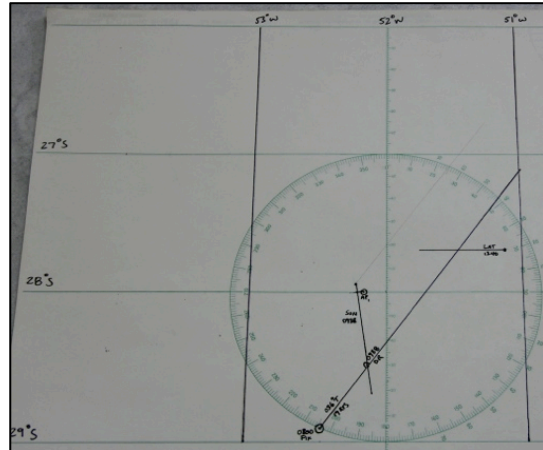
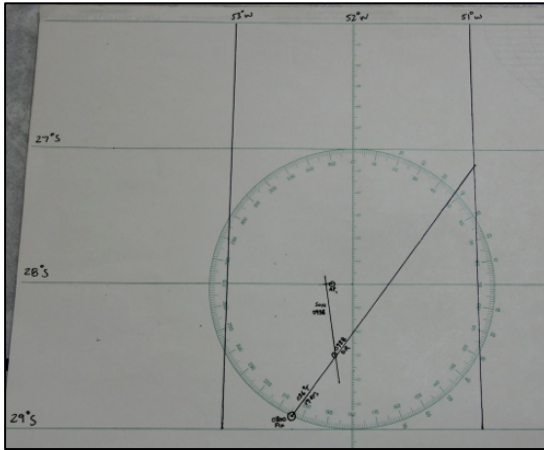
If computed altitude is greater, intercept is away.

## Celestial Fix and Running Fix Problems

- Step 13: Plot the morning Sun sight.  
 Assumed position:  $28^{\circ}$  S,  $52^{\circ} 08.2'$  W  
 Azimuth:  $082.8^{\circ}$   
 Intercept:  $2.1'$  away

| <sup>m</sup><br>40 | SUN<br>PLANETS | ARIES   | MOON   | $\begin{smallmatrix} v \\ or \\ d \end{smallmatrix}$ | Corr <sup>n</sup> | $\begin{smallmatrix} v \\ or \\ d \end{smallmatrix}$ | Corr <sup>n</sup> | $\begin{smallmatrix} v \\ or \\ d \end{smallmatrix}$ | Corr <sup>n</sup> |
|--------------------|----------------|---------|--------|------------------------------------------------------|-------------------|------------------------------------------------------|-------------------|------------------------------------------------------|-------------------|
| 00                 | 10 00-0        | 10 01-6 | 9 32-7 | 0-0                                                  | 0-0               | 6-0                                                  | 4-1               | 12-0                                                 | 8-1               |
| 01                 | 10 00-3        | 10 01-9 | 9 32-9 | 0-1                                                  | 0-1               | 6-1                                                  | 4-1               | 12-1                                                 | 8-2               |
| 02                 | 10 00-5        | 10 02-1 | 9 33-1 | 0-2                                                  | 0-1               | 6-2                                                  | 4-2               | 12-2                                                 | 8-2               |
| 03                 | 10 00-8        | 10 02-4 | 9 33-4 | 0-3                                                  | 0-2               | 6-3                                                  | 4-3               | 12-3                                                 | 8-3               |
| 04                 | 10 01-0        | 10 02-6 | 9 33-6 | 0-4                                                  | 0-3               | 6-4                                                  | 4-3               | 12-4                                                 | 8-4               |
| 05                 | 10 01-3        | 10 02-9 | 9 33-9 | 0-5                                                  | 0-3               | 6-5                                                  | 4-4               | 12-5                                                 | 8-4               |
| 06                 | 10 01-5        | 10 03-1 | 9 34-1 | 0-6                                                  | 0-4               | 6-6                                                  | 4-5               | 12-6                                                 | 8-5               |
| 07                 | 10 01-8        | 10 03-4 | 9 34-3 | 0-7                                                  | 0-5               | 6-7                                                  | 4-5               | 12-7                                                 | 8-6               |
| 08                 | 10 02-0        | 10 03-6 | 9 34-6 | 0-8                                                  | 0-5               | 6-8                                                  | 4-6               | 12-8                                                 | 8-6               |
| 09                 | 10 02-3        | 10 03-9 | 9 34-8 | 0-9                                                  | 0-6               | 6-9                                                  | 4-7               | 12-9                                                 | 8-7               |

- Step 14: Calculated the latitude at meridian passage.  
 Time of meridian passage sight: 1240 zone time or 1540 GMT  
 Observed altitude:  $77^{\circ} 10.5'$   
 Zenith Distance:  $90^{\circ} 00.0' - 77^{\circ} 10.5' = \underline{12^{\circ} 49.5'}$   
 Declination (Sun – hours):  $14^{\circ} 53.1'$  S (d number = -0.8)  
 Declination (Sun – increments):  $-0.5'$   
 Declination (Sun – total):  $\underline{14^{\circ} 52.6'}$   
 Latitude at meridian passage = zenith distance + declination =  
 $12^{\circ} 49.5' \text{ N} + 14^{\circ} 52.6' \text{ N} = \underline{27^{\circ} 42.1' \text{ S}}$
- Step 15: Plot the meridian passage latitude.  
 Latitude:  $27^{\circ} 42.1' \text{ S}$



## Celestial Fix and Running Fix Problems

Step 16: Advance the morning Sun sight (0938 zone time) and retard the meridian passage latitude (1240 zone time) both to 1200 zone time to determine the running fix.

a. Morning Sun sight: 0938 zone time to 1200 zone time = 2 hours 22 minutes = 2.36 hours

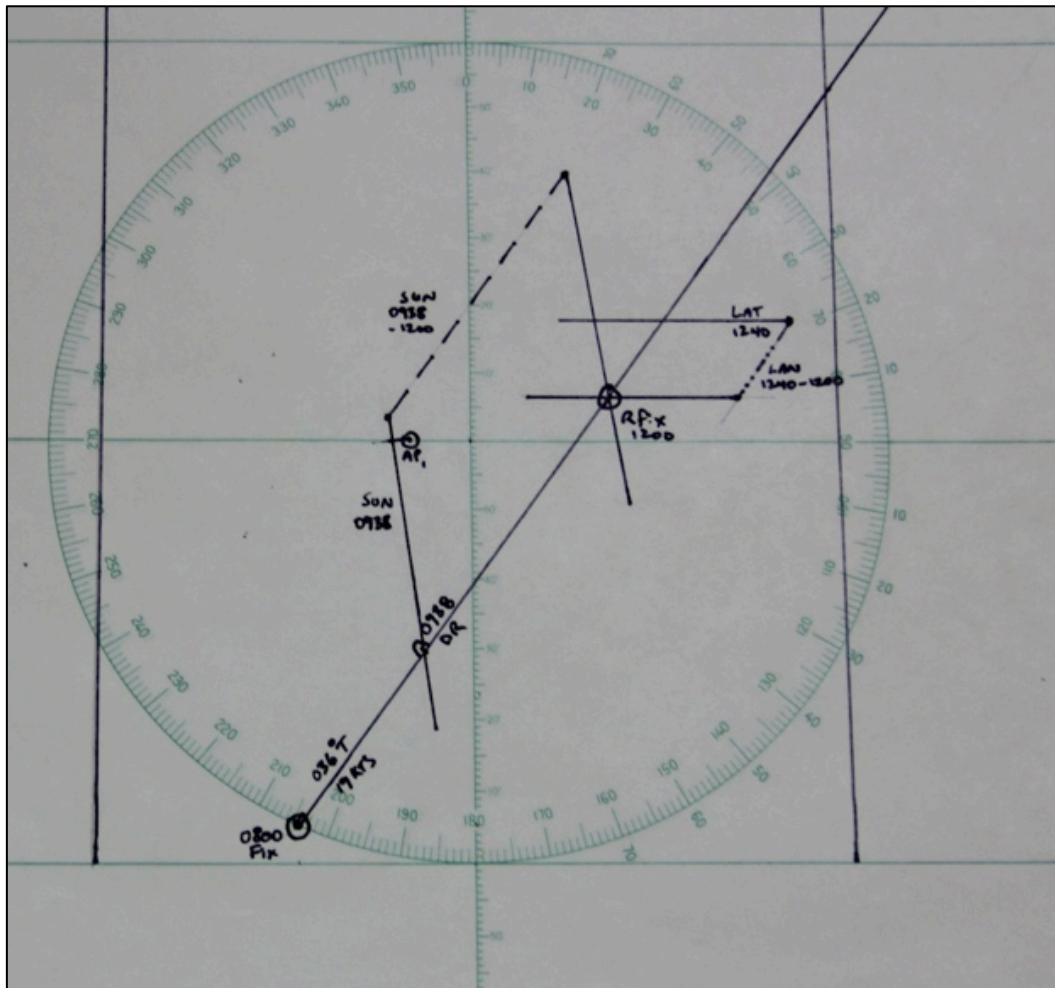
2.36 hours at 19 knots = 44.8 miles covered (course 036° T)

b. Meridian passage latitude: 1240 zone time to 1200 = 40 minutes = 0.67 hours.

0.67 hours at 19 knots = 12.67 miles covered (course 036° T reciprocal)

Step 17: Answer the required question.

Longitude = **51° 36.0' W**



## Celestial Fix and Running Fix Problems

FIX D2. At 0100 zone time on 23 September, your DR position is latitude  $24^{\circ} 25' \text{ N}$ , longitude  $83^{\circ} 00' \text{ W}$ . You are steering course  $315^{\circ} \text{ T}$ . The speed over ground is 10 knots. You observe 3 morning sun lines. Determine the latitude and longitude of your 1100 running fix.

| Body | Zone Time | GHA                | Observed Altitude  | Declination                  |
|------|-----------|--------------------|--------------------|------------------------------|
| Sun  | 0700      | $17^{\circ} 20.1'$ | $21^{\circ} 09.0'$ | $\text{S } 00^{\circ} 09.7'$ |
| Sun  | 0900      | $47^{\circ} 03.0'$ | $46^{\circ} 05.0'$ | $\text{S } 00^{\circ} 11.6'$ |
| Sun  | 1100      | $77^{\circ} 06.4'$ | $63^{\circ} 16.1'$ | $\text{S } 00^{\circ} 13.5'$ |

Answer:  $25^{\circ} 35' \text{ N}$ ,  $84^{\circ} 17' \text{ W}$

Step 1: Determine the DR position of the ship for each Sun sight. Note this solution uses a plotting sheet, but the position may also be advanced by mid-latitude sailing.

| Sight            | <i>Original Fix (0100)</i>   | <i>Sun (0700)</i>                            | <i>Sun (0900)</i>                            | <i>Sun (1100)</i>                            |
|------------------|------------------------------|----------------------------------------------|----------------------------------------------|----------------------------------------------|
| Course/Speed     | $315^{\circ}$ , 10 knots     | Same                                         | Same                                         | Same                                         |
| Time difference  | -                            | 06 hours                                     | 08 hours                                     | 10 hours                                     |
| Distance covered | -                            | 60 miles                                     | 80 miles                                     | 100 miles                                    |
| DR latitude      | $24^{\circ} 25.0' \text{ N}$ | <b><math>25^{\circ} 07' \text{ N}</math></b> | <b><math>25^{\circ} 22' \text{ N}</math></b> | <b><math>25^{\circ} 36' \text{ N}</math></b> |
| DR longitude     | $83^{\circ} 00.0' \text{ W}$ | <b><math>83^{\circ} 47' \text{ W}</math></b> | <b><math>84^{\circ} 02' \text{ W}</math></b> | <b><math>84^{\circ} 18' \text{ W}</math></b> |

Step 2: Given the GHA information presented in the question, determine the assumed position of the ship and the LHA for each Sun sight.

| Sight             |                                                               | <i>Sun (0700)</i>                              | <i>Sun (0900)</i>                              | <i>Sun (1100)</i>                              |
|-------------------|---------------------------------------------------------------|------------------------------------------------|------------------------------------------------|------------------------------------------------|
| DR latitude       |                                                               | $25^{\circ} 07' \text{ N}$                     | $25^{\circ} 22' \text{ N}$                     | $25^{\circ} 36' \text{ N}$                     |
| DR longitude      |                                                               | $83^{\circ} 47' \text{ W}$                     | $84^{\circ} 02' \text{ W}$                     | $84^{\circ} 18' \text{ W}$                     |
| Assumed latitude  |                                                               | <b><math>25^{\circ} \text{ N}</math></b>       | <b><math>25^{\circ} \text{ N}</math></b>       | <b><math>26^{\circ} \text{ N}</math></b>       |
| GHA (total)       | <i>Given</i>                                                  | $17^{\circ} 20.1'$                             | $47^{\circ} 03.0'$                             | $77^{\circ} 06.4'$                             |
| Assumed longitude | <i>To ensure whole value of LHA</i>                           | <b><math>83^{\circ} 20.1' \text{ W}</math></b> | <b><math>84^{\circ} 03.0' \text{ W}</math></b> | <b><math>84^{\circ} 06.4' \text{ W}</math></b> |
| LHA               | <i>Subtract west, add east (<math>\pm 360^{\circ}</math>)</i> | <b><math>294^{\circ}</math></b>                | <b><math>323^{\circ}</math></b>                | <b><math>353^{\circ}</math></b>                |

# Celestial Fix and Running Fix Problems

Step 3: Given the declination and altitude information presented in the question, as well as the LHA information determined in step 2, enter publication HO229 and construct a table with computed altitude (hc), altitude difference (a), and azimuth (zn).

| Sight                   |                   | <i>Sun (0700)</i> | <i>Sun (0900)</i> | <i>Sun (1100)</i> |
|-------------------------|-------------------|-------------------|-------------------|-------------------|
| Assumed latitude        |                   | 25° N             | 25° N             | 26° N             |
| Declination             |                   | S 0° 09.7'        | S 0° 11.6'        | S 0° 13.5'        |
| LHA                     |                   | 294° Contrary     | 323° Contrary     | 353° Contrary     |
| Computed altitude (hc)  | <i>From HO229</i> | 21° 37.9'         | 46° 22.2'         | 63° 08.3'         |
| Altitude difference (d) | <i>From HO229</i> | -27.5'            | -37.1'            | -58.3'            |
| Azimuth (z)             | <i>From HO229</i> | 100.7°            | 119.3°            | 164.4°            |

| LATITUDE CONTRARY NAME TO DECLINATION |         |       |       |         |       |       |         |       |       |         |       |       |         |       |       |         |       |       |         |       |       |         | L.H.A. 66°, 294° |       |      |
|---------------------------------------|---------|-------|-------|---------|-------|-------|---------|-------|-------|---------|-------|-------|---------|-------|-------|---------|-------|-------|---------|-------|-------|---------|------------------|-------|------|
| Dec.                                  | 23°     |       |       | 24°     |       |       | 25°     |       |       | 26°     |       |       | 27°     |       |       | 28°     |       |       | 29°     |       |       | 30°     |                  |       | Dec. |
|                                       | Hc      | d     | Z     | Hc      | d     | Z     | Hc      | d     | Z     | Hc      | d     | Z     | Hc      | d     | Z     | Hc      | d     | Z     | Hc      | d     | Z     | Hc      | d                | Z     |      |
| 0                                     | 21 59.2 | -25.4 | 99.9  | 21 48.8 | -26.5 | 100.3 | 21 37.9 | -27.5 | 100.7 | 21 26.6 | -28.4 | 101.0 | 21 14.9 | -29.4 | 101.4 | 21 02.8 | -30.3 | 101.8 | 20 50.3 | -31.2 | 102.2 | 20 37.5 | -32.2            | 102.6 | 0    |
| 1                                     | 21 33.8 | -25.8 | 100.8 | 21 22.3 | -26.8 | 101.2 | 21 10.4 | -27.7 | 101.6 | 20 58.2 | -28.8 | 102.0 | 20 45.5 | -29.7 | 102.4 | 20 32.5 | -30.7 | 102.7 | 20 19.1 | -31.6 | 103.1 | 20 05.3 | -32.5            | 103.5 | 1    |
| 2                                     | 21 08.0 | -26.1 | 101.8 | 20 55.5 | -27.1 | 102.2 | 20 42.7 | -28.1 | 102.6 | 20 29.4 | -29.0 | 102.9 | 20 15.8 | -30.0 | 103.3 | 20 01.8 | -30.9 | 103.6 | 19 47.5 | -31.8 | 104.0 | 19 32.8 | -32.7            | 104.3 | 2    |
| 3                                     | 20 41.9 | -26.5 | 102.8 | 20 28.4 | -27.4 | 103.1 | 20 14.6 | -28.4 | 103.5 | 20 00.4 | -29.3 | 103.9 | 19 45.8 | -30.2 | 104.2 | 19 30.9 | -31.1 | 104.6 | 19 15.7 | -32.1 | 104.9 | 19 00.1 | -33.0            | 105.2 | 3    |
| 4                                     | 20 15.4 | -26.7 | 103.7 | 20 01.0 | -27.7 | 104.1 | 19 46.2 | -28.6 | 104.4 | 19 31.1 | -29.6 | 104.8 | 19 15.6 | -30.5 | 105.1 | 18 59.8 | -31.5 | 105.5 | 18 43.6 | -32.3 | 105.8 | 18 27.1 | -33.2            | 106.1 | 4    |

| LATITUDE CONTRARY NAME TO DECLINATION |     |      |       |       |    |      |       |       |    |      |       |       |     |      |       |       |    |      |       |       |    |      | L.H.A. 37°, 323° |       |      |      |       |       |    |      |       |       |   |
|---------------------------------------|-----|------|-------|-------|----|------|-------|-------|----|------|-------|-------|-----|------|-------|-------|----|------|-------|-------|----|------|------------------|-------|------|------|-------|-------|----|------|-------|-------|---|
| Dec.                                  | 23° |      |       | 24°   |    |      | 25°   |       |    | 26°  |       |       | 27° |      |       | 28°   |    |      | 29°   |       |    | 30°  |                  |       | Dec. |      |       |       |    |      |       |       |   |
|                                       | Hc  | d    | Z     | Hc    | d  | Z    | Hc    | d     | Z  | Hc   | d     | Z     | Hc  | d    | Z     | Hc    | d  | Z    | Hc    | d     | Z  | Hc   | d                | Z     |      |      |       |       |    |      |       |       |   |
| 0                                     | 47  | 19.2 | -35.0 | 117.4 | 46 | 51.1 | -36.0 | 118.4 | 46 | 22.2 | -37.1 | 119.3 | 45  | 52.4 | -38.1 | 120.2 | 45 | 21.9 | -39.1 | 121.1 | 44 | 50.5 | -40.0            | 121.9 | 44   | 18.4 | -40.9 | 122.8 | 43 | 45.6 | -41.8 | 123.6 | 0 |
| 1                                     | 46  | 44.2 | -35.7 | 118.6 | 46 | 15.1 | -36.8 | 119.5 | 45 | 45.1 | -37.7 | 120.4 | 45  | 14.3 | -38.7 | 121.3 | 44 | 42.8 | -39.7 | 122.1 | 44 | 10.5 | -40.6            | 123.0 | 43   | 37.5 | -41.5 | 123.8 | 43 | 03.8 | -42.3 | 124.6 | 1 |
| 2                                     | 46  | 08.5 | -36.3 | 119.8 | 45 | 38.3 | -37.3 | 120.7 | 45 | 07.4 | -38.4 | 121.5 | 44  | 35.6 | -39.3 | 122.4 | 44 | 03.1 | -40.2 | 123.2 | 43 | 29.9 | -41.1            | 124.0 | 42   | 56.0 | -41.9 | 124.8 | 42 | 21.5 | -42.8 | 125.5 | 2 |
| 3                                     | 45  | 32.2 | -37.1 | 120.9 | 45 | 01.0 | -38.1 | 121.8 | 44 | 29.0 | -39.0 | 122.6 | 43  | 56.3 | -39.9 | 123.4 | 43 | 22.9 | -40.8 | 124.2 | 42 | 48.8 | -41.6            | 125.0 | 42   | 14.1 | -42.4 | 125.7 | 41 | 38.7 | -43.2 | 126.5 | 3 |
| 4                                     | 44  | 55.1 | -37.7 | 122.0 | 44 | 22.9 | -38.6 | 122.9 | 43 | 50.0 | -39.5 | 123.7 | 43  | 16.4 | -40.4 | 124.5 | 42 | 42.1 | -41.3 | 125.2 | 42 | 07.2 | -42.1            | 126.0 | 41   | 31.7 | -42.9 | 126.7 | 40 | 55.5 | -43.6 | 127.4 | 4 |

| LATITUDE CONTRARY NAME TO DECLINATION |     |      |       |       |    |      |       |       |    |      |       |       |     |      |       |       |    |      |       |       |    |      |       | L.H.A. 7°, 353° |      |      |       |       |    |      |       |       |   |
|---------------------------------------|-----|------|-------|-------|----|------|-------|-------|----|------|-------|-------|-----|------|-------|-------|----|------|-------|-------|----|------|-------|-----------------|------|------|-------|-------|----|------|-------|-------|---|
| Dec.                                  | 23° |      |       | 24°   |    |      | 25°   |       |    | 26°  |       |       | 27° |      |       | 28°   |    |      | 29°   |       |    | 30°  |       |                 | Dec. |      |       |       |    |      |       |       |   |
|                                       | Hc  | d    | Z     | Hc    | d  | Z    | Hc    | d     | Z  | Hc   | d     | Z     | Hc  | d    | Z     | Hc    | d  | Z    | Hc    | d     | Z  | Hc   | d     | Z               |      |      |       |       |    |      |       |       |   |
|                                       | °   | '    | "     | °     | '  | "    | °     | '     | "  | °    | '     | "     | °   | '    | "     | °     | '  | "    | °     | '     | "  | °    | '     | "               |      | °    | '     | "     |    |      |       |       |   |
| 0                                     | 66  | 00.8 | -57.7 | 162.6 | 65 | 03.5 | -58.0 | 163.2 | 64 | 06.0 | -58.2 | 163.8 | 63  | 08.3 | -58.3 | 164.4 | 62 | 10.4 | -58.4 | 164.9 | 61 | 12.4 | -58.5 | 165.3           | 60   | 14.3 | -58.6 | 165.8 | 59 | 16.1 | -58.7 | 166.2 | 0 |
| 1                                     | 65  | 03.1 | -57.9 | 163.2 | 64 | 05.5 | -58.0 | 163.8 | 63 | 07.8 | -58.2 | 164.4 | 62  | 10.0 | -58.4 | 164.9 | 61 | 12.0 | -58.5 | 165.3 | 60 | 13.9 | -58.6 | 165.8           | 59   | 15.7 | -58.7 | 166.2 | 58 | 17.4 | -58.9 | 166.6 | 1 |
| 2                                     | 64  | 05.2 | -58.1 | 163.8 | 63 | 07.5 | -58.3 | 164.4 | 62 | 09.6 | -58.4 | 164.9 | 61  | 11.6 | -58.5 | 165.4 | 60 | 13.5 | -58.6 | 165.8 | 59 | 15.3 | -58.7 | 166.2           | 58   | 17.0 | -58.8 | 166.6 | 57 | 18.5 | -58.8 | 167.0 | 2 |
| 3                                     | 63  | 07.1 | -58.2 | 164.4 | 62 | 09.2 | -58.3 | 164.9 | 61 | 11.2 | -58.4 | 165.4 | 60  | 13.1 | -58.5 | 165.8 | 59 | 14.9 | -58.7 | 166.2 | 58 | 16.6 | -58.8 | 166.6           | 57   | 18.2 | -58.9 | 167.0 | 56 | 19.7 | -59.0 | 167.3 | 3 |
| 4                                     | 62  | 08.9 | -58.3 | 164.9 | 61 | 10.9 | -58.4 | 165.4 | 60 | 12.8 | -58.5 | 165.8 | 59  | 14.6 | -58.7 | 166.2 | 58 | 16.2 | -58.7 | 166.6 | 57 | 17.8 | -58.8 | 167.0           | 56   | 19.3 | -58.9 | 167.3 | 55 | 20.7 | -58.9 | 167.7 | 4 |

## Celestial Fix and Running Fix Problems

Step 4: Given the azimuth information in step 3 (which does not account for increments of declination), construct a table to determine correct azimuths.

| Sight                                       |                                         | <i>Sun (0700)</i> | <i>Sun (0900)</i> | <i>Sun (1100)</i> |
|---------------------------------------------|-----------------------------------------|-------------------|-------------------|-------------------|
| <i>Base Azimuth (Z)</i>                     | <i>From HO229</i>                       | 100.7°            | 119.3°            | 164.4°            |
| <i>Next incremental Z</i>                   |                                         | 101.6°            | 120.4°            | 164.9°            |
| <i>Difference</i>                           |                                         | 0.9°              | 1.1°              | 0.5°              |
| <i>Declination Increment</i>                | <i>From given declination</i>           | 09.7'             | 11.6'             | 13.5'             |
| <i>Correction (Diff Z x Increment) / 60</i> |                                         | +0.15°            | +0.21°            | +0.11°            |
| <i>Corrected azimuth (Z)</i>                |                                         | 100.9°            | 119.5°            | 164.5°            |
| <i>Azimuth rules corrected azimuth (Zn)</i> | <i>If LHA greater than 180°, Zn = z</i> | <b>100.9°</b>     | <b>119.5°</b>     | <b>164.5°</b>     |

Step 5: Given the tabular HO229 information in step 3 determine the correct computed altitude (hc) for the three Sun sights.

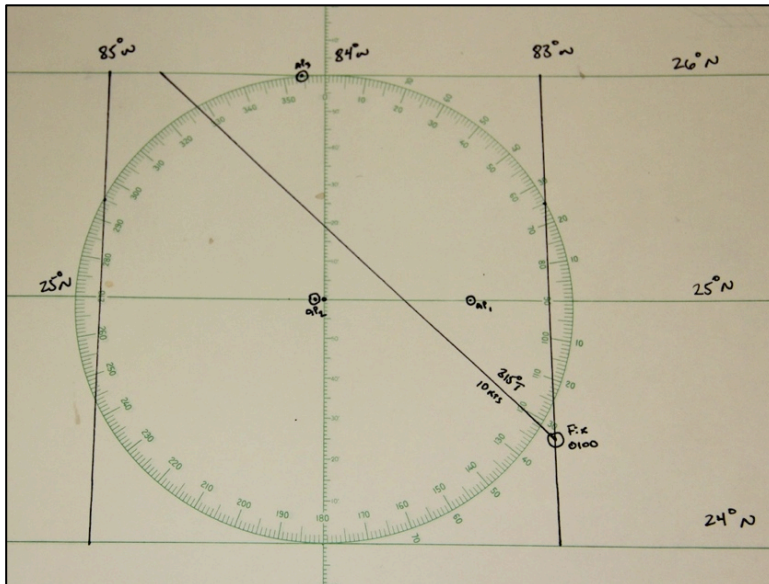
| Sight                            |                                       | <i>Sun (0700)</i> | <i>Sun (0900)</i> | <i>Sun (1100)</i> |
|----------------------------------|---------------------------------------|-------------------|-------------------|-------------------|
| <i>Tabular computed altitude</i> | <i>From step 3</i>                    | <b>21° 37.9'</b>  | <b>46° 22.2'</b>  | <b>63° 08.3'</b>  |
| <i>Altitude difference (d)</i>   | <i>From step 3</i>                    | <b>-27.5'</b>     | <b>-37.1'</b>     | <b>-58.3'</b>     |
| <i>Declination increment</i>     | <i>From given declination</i>         | 09.7'             | 11.6'             | 13.5'             |
| <i>Altitude difference</i>       | <i>From HO229 interpolation table</i> | -4.4'             | -7.2'             | -13.1'            |
| <i>Correct computed altitude</i> |                                       | <b>21° 33.5'</b>  | <b>46° 15.0'</b>  | <b>62° 55.2'</b>  |

## Celestial Fix and Running Fix Problems

Step 6: Compare the observed altitudes (given) with the computed altitudes (determined in step 5), to compute intercepts (a) for the three Sun sights.

| Sight                          |                                       | Sun (0700) | Sun (0900) | Sun (1100) |
|--------------------------------|---------------------------------------|------------|------------|------------|
| Observed altitude (ho)         | Given                                 | 21° 09.0'  | 46° 05.0'  | 63° 16.1'  |
| Correct computed altitude (hc) | From step 5                           | 21° 33.5'  | 46° 15.0'  | 62° 55.2'  |
| Intercept (a)                  | $hc - ho$                             | 24.5'      | 10.0'      | 20.9'      |
| Towards/Away                   | If hc is greater, intercept is "away" | Away       | Away       | Towards    |
| Azimuth                        | Repeated from step 4                  | 100.9° T   | 119.5° T   | 164.5° T   |

Step 7: Plot the assumed positions for each Sun sight.

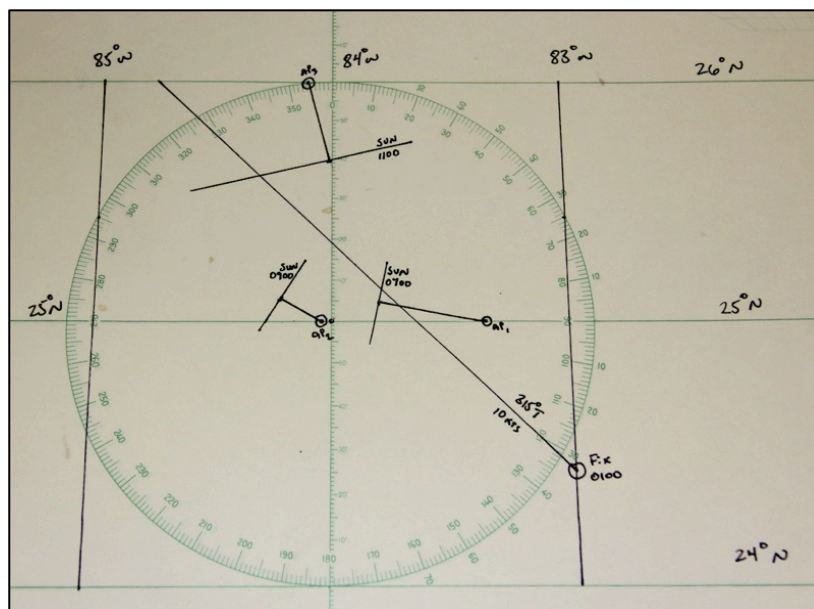


| Dec. Inc. | Altitude Difference (d) |     |     |     |      |          |   |   |   |   |       |   |   |   |   |   |   |   |    |
|-----------|-------------------------|-----|-----|-----|------|----------|---|---|---|---|-------|---|---|---|---|---|---|---|----|
|           | Tens                    |     |     |     |      | Decimals |   |   |   |   | Units |   |   |   |   |   |   |   |    |
|           | 10'                     | 20' | 30' | 40' | 50'  | 0        | 1 | 2 | 3 | 4 | 5     | 6 | 7 | 8 | 9 | 0 | 1 | 2 | 3  |
| 9.0       | 1.5                     | 3.0 | 4.5 | 6.0 | 7.5  | 0        | 0 | 0 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 14 |
| 9.1       | 1.5                     | 3.0 | 4.5 | 6.0 | 7.6  | 1        | 0 | 0 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 14 |
| 9.2       | 1.5                     | 3.0 | 4.6 | 6.1 | 7.6  | 2        | 0 | 0 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 9.3       | 1.5                     | 3.1 | 4.6 | 6.2 | 7.7  | 3        | 0 | 0 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 9.4       | 1.6                     | 3.1 | 4.7 | 6.3 | 7.8  | 4        | 0 | 1 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 9.5       | 1.6                     | 3.2 | 4.8 | 6.3 | 7.9  | 5        | 0 | 1 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 9.6       | 1.6                     | 3.2 | 4.8 | 6.4 | 8.0  | 6        | 0 | 1 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 9.7       | 1.6                     | 3.3 | 4.9 | 6.5 | 8.1  | 7        | 0 | 1 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 9.8       | 1.7                     | 3.3 | 4.9 | 6.6 | 8.2  | 8        | 0 | 1 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 9.9       | 1.7                     | 3.3 | 5.0 | 6.6 | 8.3  | 9        | 0 | 1 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 10.0      | 1.6                     | 3.3 | 5.0 | 6.6 | 8.3  | 0        | 0 | 0 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 10.1      | 1.7                     | 3.3 | 5.0 | 6.7 | 8.4  | 1        | 0 | 0 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 10.2      | 1.7                     | 3.4 | 5.1 | 6.8 | 8.5  | 2        | 0 | 0 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 10.3      | 1.7                     | 3.4 | 5.1 | 6.9 | 8.6  | 3        | 0 | 1 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 10.4      | 1.7                     | 3.5 | 5.2 | 6.9 | 8.7  | 4        | 0 | 1 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 10.5      | 1.8                     | 3.5 | 5.3 | 7.0 | 8.8  | 5        | 0 | 1 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 10.6      | 1.8                     | 3.5 | 5.3 | 7.1 | 8.8  | 6        | 0 | 1 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 10.7      | 1.8                     | 3.6 | 5.4 | 7.2 | 8.9  | 7        | 0 | 1 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 10.8      | 1.8                     | 3.6 | 5.4 | 7.2 | 9.0  | 8        | 0 | 1 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 10.9      | 1.9                     | 3.7 | 5.5 | 7.3 | 9.1  | 9        | 0 | 2 | 3 | 5 | 6     | 8 | 9 | 1 | 1 | 1 | 1 | 3 | 15 |
| 11.0      | 1.8                     | 3.6 | 5.5 | 7.3 | 9.1  | 0        | 0 | 0 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 11.1      | 1.8                     | 3.7 | 5.5 | 7.4 | 9.2  | 1        | 0 | 0 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 11.2      | 1.8                     | 3.7 | 5.6 | 7.4 | 9.3  | 2        | 0 | 0 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 11.3      | 1.9                     | 3.8 | 5.6 | 7.5 | 9.4  | 3        | 0 | 1 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 11.4      | 1.9                     | 3.8 | 5.7 | 7.6 | 9.5  | 4        | 0 | 1 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 11.5      | 1.9                     | 3.8 | 5.8 | 7.7 | 9.6  | 5        | 0 | 1 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 11.6      | 1.9                     | 3.9 | 5.8 | 7.7 | 9.7  | 6        | 0 | 1 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 11.7      | 2.0                     | 3.9 | 5.9 | 7.8 | 9.8  | 7        | 0 | 1 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 11.8      | 2.0                     | 4.0 | 5.9 | 7.9 | 9.9  | 8        | 0 | 2 | 3 | 5 | 6     | 8 | 9 | 1 | 1 | 1 | 1 | 3 | 15 |
| 11.9      | 2.0                     | 4.0 | 6.0 | 8.0 | 10.0 | 9        | 0 | 2 | 3 | 5 | 6     | 8 | 9 | 1 | 1 | 1 | 1 | 3 | 15 |
| 12.0      | 2.0                     | 4.0 | 6.0 | 8.0 | 10.0 | 0        | 0 | 0 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 12.1      | 2.0                     | 4.0 | 6.0 | 8.0 | 10.1 | 1        | 0 | 0 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 12.2      | 2.0                     | 4.0 | 6.1 | 8.1 | 10.1 | 2        | 0 | 0 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 12.3      | 2.0                     | 4.1 | 6.1 | 8.2 | 10.2 | 3        | 0 | 1 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 12.4      | 2.1                     | 4.1 | 6.2 | 8.3 | 10.3 | 4        | 0 | 1 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 12.5      | 2.1                     | 4.2 | 6.3 | 8.3 | 10.4 | 5        | 0 | 1 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 12.6      | 2.1                     | 4.2 | 6.3 | 8.4 | 10.5 | 6        | 0 | 1 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 12.7      | 2.1                     | 4.3 | 6.4 | 8.5 | 10.6 | 7        | 0 | 1 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 12.8      | 2.2                     | 4.3 | 6.4 | 8.6 | 10.7 | 8        | 0 | 2 | 3 | 5 | 6     | 8 | 9 | 1 | 1 | 1 | 1 | 3 | 15 |
| 12.9      | 2.2                     | 4.3 | 6.5 | 8.6 | 10.8 | 9        | 0 | 2 | 3 | 5 | 6     | 8 | 9 | 1 | 1 | 1 | 1 | 3 | 15 |
| 13.0      | 2.1                     | 4.3 | 6.5 | 8.6 | 10.8 | 0        | 0 | 0 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 13.1      | 2.2                     | 4.3 | 6.5 | 8.7 | 10.9 | 1        | 0 | 0 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 13.2      | 2.2                     | 4.4 | 6.6 | 8.8 | 11.0 | 2        | 0 | 0 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 13.3      | 2.2                     | 4.4 | 6.6 | 8.9 | 11.1 | 3        | 0 | 1 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 13.4      | 2.2                     | 4.5 | 6.7 | 8.9 | 11.2 | 4        | 0 | 1 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 13.5      | 2.3                     | 4.5 | 6.8 | 9.0 | 11.3 | 5        | 0 | 1 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 13.6      | 2.3                     | 4.5 | 6.8 | 9.1 | 11.3 | 6        | 0 | 1 | 2 | 3 | 5     | 6 | 8 | 9 | 1 | 1 | 1 | 3 | 15 |
| 13.7      | 2.3                     | 4.6 | 6.9 | 9.2 | 11.4 | 7        | 0 | 2 | 3 | 5 | 6     | 8 | 9 | 1 | 1 | 1 | 1 | 3 | 15 |
| 13.8      | 2.3                     | 4.6 | 6.9 | 9.2 | 11.5 | 8        | 0 | 2 | 3 | 5 | 6     | 8 | 9 | 1 | 1 | 1 | 1 | 3 | 15 |
| 13.9      | 2.4                     | 4.7 | 7.0 | 9.3 | 11.6 | 9        | 0 | 2 | 3 | 5 | 6     | 8 | 9 | 1 | 1 | 1 | 1 | 3 | 15 |



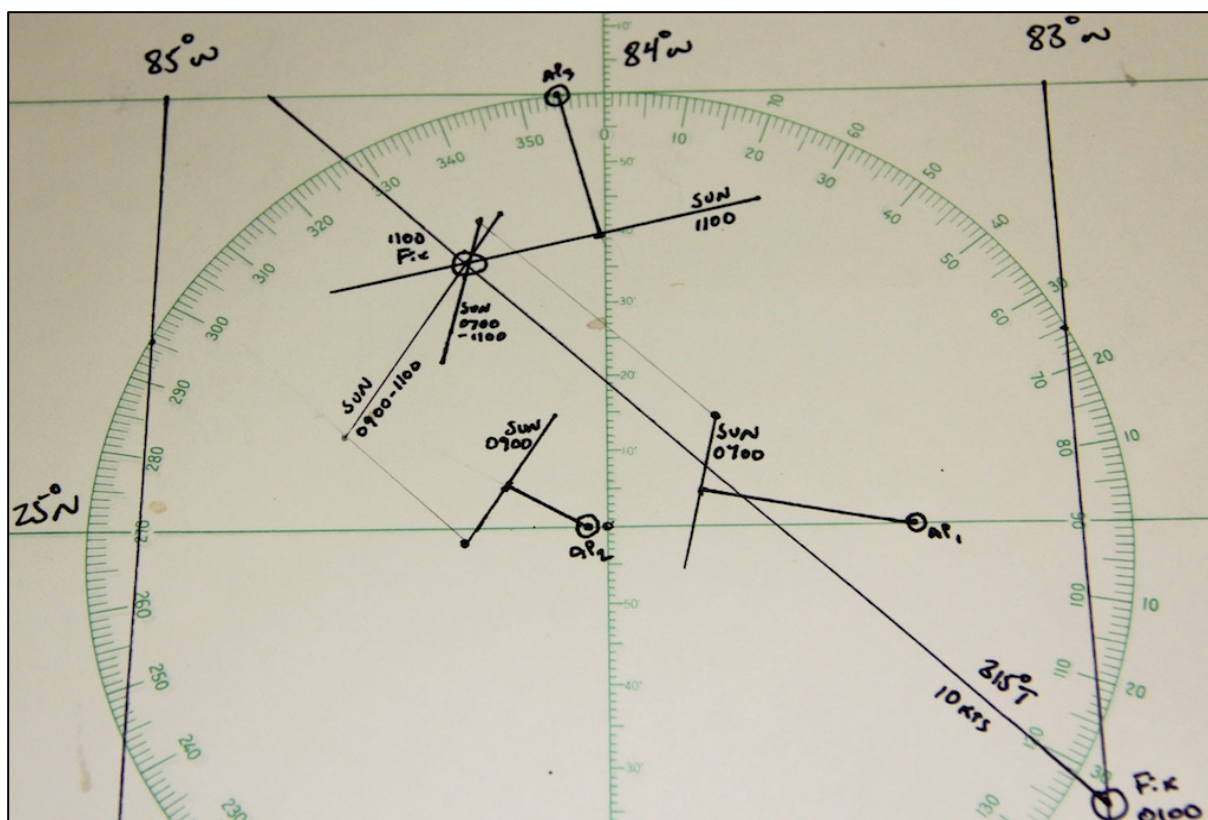
## Celestial Fix and Running Fix Problems

Step 8: Plot each Sun sight's line of position.



Step 9: Advance the 0700 and 0900 Sun lines of position to 1100 to determine the running fix.

**Fix:  $25^{\circ} 35' N$ ,  $84^{\circ} 17' W$**



## Celestial Fix and Running Fix Problems

### Any Celestial Body Fixes

FIX D3. On 6 April your 1830 zone time DR position is latitude  $26^{\circ} 33' \text{ N}$ , longitude  $64^{\circ} 31' \text{ W}$ . You are on course  $082^{\circ} \text{ T}$  at a speed of 16 knots. You observe 3 celestial bodies. Determine the latitude and longitude of your 1900 running fix.

| Body    | Zone Time | GHA                 | Observed Altitude  | Declination                  |
|---------|-----------|---------------------|--------------------|------------------------------|
| Sirius  | 1836      | $73^{\circ} 02.7'$  | $46^{\circ} 00.5'$ | $\text{S } 16^{\circ} 41.7'$ |
| Regulus | 1842      | $23^{\circ} 46.9'$  | $49^{\circ} 07.2'$ | $\text{N } 12^{\circ} 03.5'$ |
| Mirfak  | 1900      | $129^{\circ} 24.3'$ | $35^{\circ} 51.6'$ | $\text{N } 49^{\circ} 47.7'$ |

Answer:  $26^{\circ} 33' \text{ N}$ ,  $64^{\circ} 27' \text{ W}$

Step 1: Determine the DR position of the ship for each star sight. Note this solution uses a plotting sheet, but the position may also be advanced by mid-latitude sailing.

| Sight            | <i>Original DR (1830)</i>    | <i>Sirius (1836)</i>                         | <i>Regulus (1842)</i>                        | <i>Mirfak (1900)</i>                         |
|------------------|------------------------------|----------------------------------------------|----------------------------------------------|----------------------------------------------|
| Course/Speed     | $082^{\circ}$ , 16 knots     | Same                                         | Same                                         | Same                                         |
| Time difference  | -                            | 6 minutes                                    | 12 minutes                                   | 30 minutes                                   |
| Distance covered | -                            | 1.6 nm                                       | 3.2 nm                                       | 8 nm                                         |
| DR latitude      | $26^{\circ} 33.0' \text{ N}$ | <b><math>26^{\circ} 33' \text{ N}</math></b> | <b><math>26^{\circ} 33' \text{ N}</math></b> | <b><math>26^{\circ} 34' \text{ N}</math></b> |
| DR longitude     | $64^{\circ} 31.0' \text{ W}$ | <b><math>64^{\circ} 29' \text{ W}</math></b> | <b><math>64^{\circ} 28' \text{ W}</math></b> | <b><math>64^{\circ} 22' \text{ W}</math></b> |

Step 2: Given the GHA information presented in the question, determine the assumed position of the ship and the LHA for each star sight.

| Sight             |                                                               | <i>Sirius (1836)</i>                           | <i>Regulus (1842)</i>                          | <i>Mirfak (1900)</i>                           |
|-------------------|---------------------------------------------------------------|------------------------------------------------|------------------------------------------------|------------------------------------------------|
| DR latitude       |                                                               | $26^{\circ} 33' \text{ N}$                     | $26^{\circ} 33' \text{ N}$                     | $26^{\circ} 34' \text{ N}$                     |
| DR longitude      |                                                               | $64^{\circ} 29' \text{ W}$                     | $64^{\circ} 28' \text{ W}$                     | $64^{\circ} 22' \text{ W}$                     |
| Assumed latitude  |                                                               | <b><math>27^{\circ} \text{ N}</math></b>       | <b><math>27^{\circ} \text{ N}</math></b>       | <b><math>27^{\circ} \text{ N}</math></b>       |
| GHA (total)       | <i>Given</i>                                                  | $73^{\circ} 02.7'$                             | $23^{\circ} 46.9'$                             | $129^{\circ} 24.3'$                            |
| Assumed longitude | <i>To ensure whole value of LHA</i>                           | <b><math>64^{\circ} 02.7' \text{ W}</math></b> | <b><math>64^{\circ} 46.9' \text{ W}</math></b> | <b><math>64^{\circ} 24.3' \text{ W}</math></b> |
| LHA               | <i>Subtract west, add east (<math>\pm 360^{\circ}</math>)</i> | <b><math>9^{\circ}</math></b>                  | <b><math>319^{\circ}</math></b>                | <b><math>65^{\circ}</math></b>                 |

# Celestial Fix and Running Fix Problems

Step 3: Given the declination and altitude information presented in the question, as well as the LHA information determined in step 2, enter publication HO229 and construct a table with computed altitude (hc), altitude difference (a), and azimuth (zn).

| Sight                   |                   | <i>Sirius (1836)</i> | <i>Regulus (1842)</i> | <i>Mirfak (1900)</i> |
|-------------------------|-------------------|----------------------|-----------------------|----------------------|
| Assumed latitude        |                   | 27° N                | 27° N                 | 27° N                |
| Declination             |                   | S 16° 41.7'          | N 12° 03.5'           | N 49° 47.7'          |
| LHA                     |                   | 9° Contrary          | 319° Same             | 65° Same             |
| Computed altitude (hc)  | <i>From HO229</i> | 46° 07.3'            | 48° 46.6'             | 36° 08.0'            |
| Altitude difference (d) | <i>From HO229</i> | -58.8'               | 27.2'                 | 0.7'                 |
| Azimuth (z)             | <i>From HO229</i> | 167.5°               | 103.1°                | 47.4°                |

| LATITUDE CONTRARY NAME TO DECLINATION |         |       |       |         |       |       |         |       |       |         |       |       |         |       |       |         |       |       |         |       |       |         |       | L.H.A. 9°, 351° |      |
|---------------------------------------|---------|-------|-------|---------|-------|-------|---------|-------|-------|---------|-------|-------|---------|-------|-------|---------|-------|-------|---------|-------|-------|---------|-------|-----------------|------|
| Dec.                                  | 23°     |       |       | 24°     |       |       | 25°     |       |       | 26°     |       |       | 27°     |       |       | 28°     |       |       | 29°     |       |       | 30°     |       |                 | Dec. |
|                                       | Hc      | d     | Z     | Hc      | d     | Z     | Hc      | d     | Z     | Hc      | d     | Z     | Hc      | d     | Z     | Hc      | d     | Z     | Hc      | d     | Z     | Hc      | d     | Z               |      |
| 0                                     | 65 23.5 | -56.5 | 157.9 | 64 27.7 | -56.7 | 158.7 | 63 31.7 | -57.0 | 159.5 | 62 35.4 | -57.2 | 160.1 | 61 38.8 | -57.4 | 160.8 | 60 42.1 | -57.7 | 161.4 | 59 45.1 | -57.8 | 161.9 | 58 48.0 | -58.0 | 162.4           | 0    |
| 1                                     | 64 27.0 | -56.6 | 158.7 | 63 31.0 | -57.0 | 159.5 | 62 34.7 | -57.2 | 160.1 | 61 38.1 | -57.4 | 160.8 | 60 41.4 | -57.6 | 161.4 | 59 44.4 | -57.7 | 161.9 | 58 47.3 | -57.9 | 162.4 | 57 50.0 | -58.1 | 162.9           | 1    |
| 2                                     | 63 30.4 | -56.9 | 159.5 | 62 34.0 | -57.1 | 160.2 | 61 37.5 | -57.4 | 160.8 | 60 40.7 | -57.5 | 161.4 | 59 43.8 | -57.7 | 161.9 | 58 46.7 | -57.9 | 162.4 | 57 49.4 | -58.1 | 162.9 | 56 51.9 | -58.1 | 163.4           | 2    |
| 3                                     | 62 33.5 | -57.1 | 160.2 | 61 36.9 | -57.3 | 160.8 | 60 40.1 | -57.5 | 161.4 | 59 43.2 | -57.7 | 162.0 | 58 46.1 | -57.9 | 162.5 | 57 48.8 | -58.0 | 162.9 | 56 51.3 | -58.1 | 163.4 | 55 53.8 | -58.3 | 163.8           | 3    |
| 4                                     | 61 36.4 | -57.3 | 160.8 | 60 39.6 | -57.5 | 161.4 | 59 42.6 | -57.6 | 162.0 | 58 45.5 | -57.8 | 162.5 | 57 48.2 | -58.0 | 163.0 | 56 50.8 | -58.1 | 163.4 | 55 53.2 | -58.2 | 163.8 | 54 55.5 | -58.3 | 164.2           | 4    |
| 5                                     | 60 39.1 | -57.4 | 161.5 | 59 42.1 | -57.6 | 162.0 | 58 45.0 | -57.8 | 162.5 | 57 47.7 | -57.9 | 163.0 | 56 50.2 | -58.0 | 163.4 | 55 52.7 | -58.2 | 163.9 | 54 55.0 | -58.4 | 164.3 | 53 57.2 | -58.5 | 164.6           | 5    |
| 6                                     | 59 41.7 | -57.6 | 162.0 | 58 44.5 | -57.7 | 162.6 | 57 47.2 | -57.9 | 163.0 | 56 49.8 | -58.1 | 163.5 | 55 52.2 | -58.2 | 163.9 | 54 54.5 | -58.3 | 164.3 | 53 56.6 | -58.3 | 164.7 | 52 58.7 | -58.5 | 165.0           | 6    |
| 7                                     | 58 44.1 | -57.7 | 162.6 | 57 46.8 | -57.9 | 163.1 | 56 49.3 | -58.0 | 163.5 | 55 51.7 | -58.1 | 163.9 | 54 54.0 | -58.3 | 164.3 | 53 56.2 | -58.4 | 164.7 | 52 58.3 | -58.5 | 165.1 | 51 59.8 | -58.5 | 165.4           | 7    |
| 8                                     | 57 46.4 | -57.8 | 163.1 | 56 48.9 | -58.0 | 163.6 | 55 51.3 | -58.1 | 164.0 | 54 53.6 | -58.2 | 164.4 | 53 55.7 | -58.3 | 164.7 | 52 57.8 | -58.4 | 165.1 | 51 59.8 | -58.5 | 165.4 | 50 01.7 | -58.6 | 165.7           | 8    |
| 9                                     | 56 48.6 | -58.0 | 163.6 | 55 50.9 | -58.0 | 164.0 | 54 53.2 | -58.2 | 164.4 | 53 55.4 | -58.3 | 164.8 | 52 57.4 | -58.4 | 165.1 | 51 59.4 | -58.5 | 165.5 | 50 01.3 | -58.6 | 165.8 | 49 03.1 | -58.7 | 166.1           | 9    |
| 10                                    | 55 50.6 | -58.0 | 164.1 | 54 52.9 | -58.2 | 164.5 | 53 55.0 | -58.3 | 164.8 | 52 57.1 | -58.4 | 165.2 | 51 59.0 | -58.5 | 165.5 | 50 00.9 | -58.6 | 165.8 | 49 02.7 | -58.7 | 166.1 | 48 04.4 | -58.8 | 166.4           | 10   |
| 11                                    | 54 52.6 | -58.2 | 164.5 | 53 54.7 | -58.2 | 164.9 | 52 56.7 | -58.3 | 165.2 | 51 58.7 | -58.5 | 165.6 | 50 02.3 | -58.6 | 166.2 | 49 04.0 | -58.7 | 166.4 | 48 05.6 | -58.7 | 166.7 | 47 07.3 | -58.8 | 167.0           | 11   |
| 12                                    | 53 54.4 | -58.2 | 164.9 | 52 56.5 | -58.4 | 165.3 | 51 58.4 | -58.4 | 165.6 | 50 00.2 | -58.5 | 165.9 | 49 03.7 | -58.7 | 166.5 | 48 05.0 | -58.7 | 166.8 | 47 06.9 | -58.8 | 167.0 | 46 08.1 | -58.9 | 167.3           | 12   |
| 13                                    | 52 56.2 | -58.3 | 165.4 | 51 58.1 | -58.4 | 165.7 | 50 00.0 | -58.5 | 166.0 | 49 01.7 | -58.6 | 166.3 | 48 03.4 | -58.7 | 166.5 | 47 06.3 | -58.8 | 167.1 | 46 08.1 | -58.9 | 167.3 | 45 09.2 | -58.9 | 167.6           | 13   |
| 14                                    | 51 57.9 | -58.3 | 165.7 | 50 59.7 | -58.4 | 166.0 | 49 01.5 | -58.6 | 166.3 | 48 03.1 | -58.6 | 166.6 | 47 04.7 | -58.7 | 166.9 | 46 07.5 | -58.8 | 167.2 | 45 08.9 | -58.9 | 167.6 | 44 10.3 | -59.0 | 167.8           | 14   |
| 15                                    | 50 59.6 | -58.5 | 166.1 | 50 01.3 | -58.6 | 166.4 | 49 02.9 | -58.6 | 166.7 | 48 04.5 | -58.7 | 166.9 | 47 06.0 | -58.7 | 167.2 | 46 07.5 | -58.8 | 167.4 | 45 08.9 | -58.9 | 167.6 | 44 10.3 | -59.0 | 167.8           | 15   |
| 16                                    | 50 01.1 | -58.5 | 166.5 | 49 02.7 | -58.5 | 166.7 | 48 04.3 | -58.6 | 167.0 | 47 05.8 | -58.7 | 167.2 | 46 07.3 | -58.8 | 167.5 | 45 08.7 | -58.9 | 167.7 | 44 10.0 | -58.9 | 167.9 | 43 11.3 | -58.9 | 168.1           | 16   |
| 17                                    | 49 02.6 | -58.6 | 166.8 | 48 04.2 | -58.7 | 167.1 | 47 05.7 | -58.8 | 167.3 | 46 07.1 | -58.8 | 167.5 | 45 08.5 | -58.9 | 167.8 | 44 09.8 | -58.9 | 168.0 | 43 10.9 | -58.9 | 168.2 | 42 12.4 | -59.0 | 168.3           | 17   |
| 18                                    | 48 04.0 | -58.6 | 167.1 | 47 05.5 | -58.7 | 167.4 | 46 06.9 | -58.7 | 167.6 | 45 08.3 | -58.8 | 167.8 | 44 09.6 | -58.8 | 168.0 | 43 10.9 | -58.9 | 168.2 | 42 12.2 | -59.0 | 168.4 | 41 13.4 | -59.1 | 168.6           | 18   |
| 19                                    | 47 05.4 | -58.6 | 167.5 | 46 06.8 | -58.7 | 167.7 | 45 08.2 | -58.8 | 167.9 | 44 09.5 | -58.9 | 168.1 | 43 10.8 | -58.9 | 168.3 | 42 12.0 | -59.0 | 168.5 | 41 13.2 | -59.0 | 168.7 | 40 14.3 | -59.0 | 168.8           | 19   |

| 41° , 319° L.H.A. |         |             | LATITUDE SAME NAME AS DECLINATION |             |         |             |         |             |         |             |         |             |         |             |         |             |    |     |    |     | N. Lat. { L.H.A. greater than 180° .....Zn=Z<br>L.H.A. less than 180° .....Zn=360°-Z |     |    |     |      |  |  |  |  |
|-------------------|---------|-------------|-----------------------------------|-------------|---------|-------------|---------|-------------|---------|-------------|---------|-------------|---------|-------------|---------|-------------|----|-----|----|-----|--------------------------------------------------------------------------------------|-----|----|-----|------|--|--|--|--|
|                   |         |             | 23°                               |             |         | 24°         |         |             | 25°     |             |         | 26°         |         |             | 27°     |             |    | 28° |    |     | 29°                                                                                  |     |    | 30° |      |  |  |  |  |
| Dec.              | Hc      | d Z         | Hc                                | d Z         | Hc      | d Z         | Hc      | d Z         | Hc      | d Z         | Hc      | d Z         | Hc      | d Z         | Hc      | d Z         | Hc | d Z | Hc | d Z | Hc                                                                                   | d Z | Hc | d Z | Dec. |  |  |  |  |
| 0                 | 44 00.3 | +32.2 114.2 | 43 35.2                           | +33.4 115.1 | 43 09.4 | +34.4 115.9 | 42 42.8 | +35.5 116.8 | 42 15.4 | +36.5 117.6 | 41 47.2 | +37.5 118.4 | 41 18.4 | +38.4 119.1 | 40 48.8 | +39.4 119.9 | 0  |     |    |     |                                                                                      |     |    |     |      |  |  |  |  |
| 1                 | 44 32.5 | +31.5 113.0 | 44 08.6                           | +32.6 113.9 | 43 47.8 | +33.8 114.8 | 43 18.3 | +34.8 115.7 | 42 51.9 | +35.9 116.5 | 42 24.7 | +36.9 117.3 | 41 56.8 | +37.9 118.1 | 41 28.2 | +38.8 118.9 | 1  |     |    |     |                                                                                      |     |    |     |      |  |  |  |  |
| 2                 | 45 04.0 | +30.7 111.8 | 44 41.2                           | +31.9 112.7 | 44 17.6 | +33.0 113.6 | 43 53.1 | +34.2 114.5 | 43 27.8 | +35.2 115.4 | 43 01.6 | +36.3 116.2 | 42 34.7 | +37.3 117.1 | 42 07.0 | +38.3 117.9 | 2  |     |    |     |                                                                                      |     |    |     |      |  |  |  |  |
| 3                 | 45 34.7 | +29.9 110.6 | 45 13.1                           | +31.2 111.6 | 44 50.6 | +32.4 112.5 | 44 27.3 | +33.4 113.4 | 44 03.0 | +34.6 114.3 | 43 37.9 | +35.7 115.2 | 43 12.0 | +36.7 116.0 | 42 45.3 | +37.7 116.8 | 3  |     |    |     |                                                                                      |     |    |     |      |  |  |  |  |
| 4                 | 46 04.6 | +29.1 109.4 | 45 44.3                           | +30.3 110.3 | 45 23.0 | +31.5 111.3 | 45 00.7 | +32.8 112.2 | 44 37.6 | +33.9 113.1 | 44 13.6 | +35.0 114.0 | 43 48.7 | +36.1 114.9 | 43 20.3 | +37.1 115.8 | 4  |     |    |     |                                                                                      |     |    |     |      |  |  |  |  |
| 5                 | 46 33.7 | +28.3 108.1 | 46 14.6                           | +29.5 109.1 | 45 54.5 | +30.8 110.1 | 45 33.5 | +31.9 111.0 | 45 11.5 | +33.1 112.0 | 44 48.6 | +34.3 112.9 | 44 24.8 | +35.4 113.8 | 44 00.1 | +36.5 114.7 | 5  |     |    |     |                                                                                      |     |    |     |      |  |  |  |  |
| 6                 | 47 02.0 | +27.4 106.8 | 46 44.1                           | +28.7 107.8 | 46 25.3 | +29.9 108.8 | 46 05.4 | +31.2 109.8 | 45 44.6 | +32.4 110.8 | 45 22.9 | +33.5 111.7 | 45 00.2 | +34.7 112.7 | 44 36.6 | +35.8 113.6 | 6  |     |    |     |                                                                                      |     |    |     |      |  |  |  |  |
| 7                 | 47 29.4 | +26.4 105.5 | 47 12.8                           | +27.8 106.5 | 46 55.2 | +29.1 107.6 | 46 36.6 | +30.4 108.6 | 46 17.0 | +31.6 109.6 | 45 56.4 | +32.8 110.5 | 45 34.9 | +34.0 111.5 | 45 12.4 | +35.2 112.4 | 7  |     |    |     |                                                                                      |     |    |     |      |  |  |  |  |
| 8                 | 47 55.8 | +25.5 104.2 | 47 40.6                           | +26.9 105.2 | 47 24.3 | +28.2 106.3 | 47 07.0 | +29.5 107.3 | 46 48.6 | +30.8 108.3 | 46 29.2 | +32.1 109.3 | 46 08.9 | +33.2 110.3 | 45 47.6 | +34.4 111.3 | 8  |     |    |     |                                                                                      |     |    |     |      |  |  |  |  |
| 9                 | 48 21.3 | +24.6 102.8 | 48 07.5                           | +25.9 103.9 | 47 52.5 | +27.3 105.0 | 47 36.5 | +28.6 106.0 | 47 19.4 | +30.0 107.1 | 47 01.3 | +31.2 108.1 | 46 42.1 | +32.5 109.1 | 46 22.0 | +33.7 110.1 | 9  |     |    |     |                                                                                      |     |    |     |      |  |  |  |  |
| 10                | 48 45.9 | +23.5 101.4 | 48 33.4                           | +25.0 102.5 | 48 19.8 | +26.4 103.6 | 48 05.1 | +27.8 104.7 | 47 49.4 | +29.0 105.8 | 47 32.5 | +30.4 106.8 | 47 14.6 | +31.8 107.9 | 46 55.7 | +32.9 108.9 | 10 |     |    |     |                                                                                      |     |    |     |      |  |  |  |  |
| 11                | 49 09.4 | +22.5 100.0 | 48 58.4                           | +24.0 101.2 | 48 46.2 | +25.4 102.3 | 48 32.9 | +26.8 103.4 | 48 18.4 | +28.2 104.5 | 48 02.9 | +29.5 105.6 | 47 46.2 | +30.9 106.6 | 47 28.6 | +32.0 107.7 | 11 |     |    |     |                                                                                      |     |    |     |      |  |  |  |  |
| 12                | 49 31.9 | +21.5 98.6  | 49 22.4                           | +22.9 99.8  | 49 11.6 | +24.4 100.9 | 48 59.7 | +25.8 102.0 | 48 46.6 | +27.2 103.1 | 48 32.4 | +28.6 104.3 | 48 17.1 | +29.9 105.3 | 48 00.6 | +31.3 106.4 | 12 |     |    |     |                                                                                      |     |    |     |      |  |  |  |  |
| 13                | 49 53.4 | +20.3 97.2  | 49 45.3                           | +21.9 98.3  | 49 36.0 | +23.3 99.5  | 49 25.5 | +24.8 100.6 | 49 13.8 | +26.3 101.8 | 49 01.0 | +27.6 102.9 | 48 47.0 | +29.0 104.0 | 48 31.9 | +30.4 105.1 | 13 |     |    |     |                                                                                      |     |    |     |      |  |  |  |  |
| 14                | 50 13.7 | +19.3 95.7  | 50 07.2                           | +20.7 96.9  | 49 59.3 | +22.3 98.1  | 49 50.3 | +23.8 99.2  | 49 40.1 | +25.2 100.4 | 49 28.6 | +26.7 101.6 | 49 16.0 | +28.1 102.7 | 49 02.3 | +29.4 103.8 | 14 |     |    |     |                                                                                      |     |    |     |      |  |  |  |  |

| 65°, 295° L.H.A. |         |             | LATITUDE SAME NAME AS DECLINATION |             |         |             |         |             |         |             |         |             |         |             |         |             |         |             |         |             | N. Lat. { L.H.A. greater than 180° .....Zn=Z<br>L.H.A. less than 180° .....Zn=360°-Z |             |      |  |  |
|------------------|---------|-------------|-----------------------------------|-------------|---------|-------------|---------|-------------|---------|-------------|---------|-------------|---------|-------------|---------|-------------|---------|-------------|---------|-------------|--------------------------------------------------------------------------------------|-------------|------|--|--|
| 23°              |         |             | 24°                               |             |         | 25°         |         |             | 26°     |             |         | 27°         |         |             | 28°     |             |         | 29°         |         |             | 30°                                                                                  |             |      |  |  |
| Dec.             | Hc      | d Z         | Hc                                | d Z         | Hc      | d Z         | Hc      | d Z         | Hc      | d Z         | Hc      | d Z         | Hc      | d Z         | Hc      | d Z         | Hc      | d Z         | Hc      | d Z         | Hc                                                                                   | d Z         | Dec. |  |  |
| 0                | 22 53.6 | +25.3 100.3 | 22 42.7                           | +26.2 100.7 | 22 31.3 | +27.2 101.1 | 22 19.5 | +28.2 101.6 | 22 07.2 | +29.3 102.0 | 21 54.6 | +30.2 102.3 | 21 41.6 | +31.1 102.7 | 21 28.1 | +32.1 103.1 | 21 14.6 | +33.1 103.4 | 21 01.1 | +34.1 103.7 | 20 47.6                                                                              | +35.1 104.0 | 0    |  |  |
| 1                | 23 18.9 | +24.9 99.3  | 23 08.9                           | +25.9 99.8  | 22 58.5 | +27.0 100.2 | 22 47.7 | +27.9 100.6 | 22 36.5 | +28.9 101.0 | 22 24.8 | +29.9 101.4 | 22 12.7 | +30.9 101.8 | 22 00.2 | +31.8 102.2 | 21 47.7 | +32.8 102.5 | 21 35.0 | +33.7 102.9 | 21 22.3                                                                              | +34.7 103.2 | 1    |  |  |
| 2                | 23 43.8 | +24.5 98.3  | 23 34.8                           | +25.6 98.8  | 23 25.5 | +26.5 99.2  | 23 15.6 | +27.6 99.6  | 23 05.4 | +28.5 100.1 | 22 54.7 | +29.5 100.5 | 22 43.6 | +30.5 100.9 | 22 32.0 | +31.5 101.3 | 22 20.7 | +32.5 101.7 | 22 09.4 | +33.5 102.1 | 21 98.1                                                                              | +34.5 102.5 | 2    |  |  |
| 3                | 24 08.3 | +24.1 97.3  | 24 00.4                           | +25.1 97.8  | 23 52.2 | +26.2 98.2  | 23 43.2 | +27.2 98.7  | 23 33.9 | +28.2 99.1  | 23 24.7 | +29.2 99.5  | 23 15.4 | +30.2 99.9  | 23 06.1 | +31.2 100.3 | 22 56.8 | +32.2 100.7 | 22 47.5 | +33.2 101.1 | 22 38.2                                                                              | +34.2 101.5 | 3    |  |  |
| 4                | 24 32.4 | +23.3 96.3  | 24 25.5                           | +24.8 96.8  | 24 18.2 | +25.8 97.2  | 24 10.4 | +26.8 97.7  | 24 02.1 | +27.9 98.1  | 23 53.4 | +28.9 98.6  | 23 44.3 | +29.8 99.0  | 23 34.6 | +30.8 99.4  | 23 25.3 | +31.7 100.0 | 23 16.0 | +32.7 100.4 | 23 06.7                                                                              | +33.7 100.8 | 4    |  |  |
| 45               | 23 27.7 | -0.3 50.2   | 34 05.9                           | -0.7 50.7   | 34 43.6 | -1.7 51.2   | 35 21.0 | -2.7 51.8   | 35 57.9 | -3.7 52.4   | 36 34.3 | -4.7 52.9   | 37 10.2 | -5.7 53.5   | 37 45.6 | -6.8 54.2   | 38 21.1 | -7.8 54.8   | 38 96.6 | -8.8 55.4   | 39 72.1                                                                              | -9.8 56.0   | 45   |  |  |
| 46               | 23 27.4 | -1.0 49.0   | 34 06.6                           | -0.0 49.5   | 34 45.3 | -1.0 50.0   | 35 23.7 | -1.9 50.6   | 36 01.6 | -2.9 51.1   | 36 39.0 | -3.9 51.7   | 37 15.9 | -5.0 52.3   | 37 52.4 | -6.0 52.9   | 38 29.0 | -7.0 53.5   | 39 05.6 | -8.0 54.1   | 39 82.1                                                                              | -9.0 54.7   | 46   |  |  |
| 47               | 23 26.4 | -1.6 47.8   | 34 06.6                           | -0.8 48.3   | 34 46.3 | -0.2 48.8   | 35 25.6 | +1.2 49.3   | 36 04.5 | +2.1 49.9   | 36 42.9 | +3.2 50.4   | 37 20.9 | +4.1 51.0   | 37 58.4 | +5.1 51.6   | 38 35.9 | +6.1 52.2   | 39 13.4 | +7.1 52.8   | 39 90.9                                                                              | +8.1 53.4   | 47   |  |  |
| 48               | 23 24.8 | -2.3 46.4   | 34 05.8                           | -1.4 47.1   | 34 46.5 | -0.5 47.6   | 35 26.8 | +0.4 48.1   | 36 06.6 | +1.4 48.6   | 36 46.1 | +2.3 49.2   | 37 25.0 | +3.4 49.8   | 38 03.5 | +4.4 50.4   | 38 81.0 | +5.4 51.0   | 39 58.5 | +6.4 51.6   | 40 36.0                                                                              | +7.4 52.2   | 48   |  |  |
| 49               | 23 22.5 | -3.0 45.4   | 34 04.4                           | -2.1 45.9   | 34 46.0 | -1.2 46.4   | 35 27.2 | -0.3 46.9   | 36 08.0 | +0.7 47.4   | 36 48.4 | +1.6 48.0   | 37 28.4 | +2.5 48.5   | 38 07.9 | +3.5 49.1   | 38 87.4 | +4.5 49.7   | 39 66.9 | +5.5 50.3   | 40 46.4                                                                              | +6.5 50.9   | 49   |  |  |
| 50               | 23 19.5 | -3.8 44.2   | 34 02.3                           | -2.8 44.7   | 34 44.8 | -2.0 45.2   | 35 26.9 | -1.0 45.7   | 36 08.7 | -0.2 46.2   | 36 50.0 | +0.8 46.7   | 37 30.9 | +1.8 47.3   | 38 11.4 | +2.8 47.8   | 38 91.9 | +3.8 48.4   | 39 72.4 | +4.8 49.0   | 40 52.9                                                                              | +5.8 49.6   | 50   |  |  |
| 51               | 23 15.7 | -4.3 43.0   | 34 02.9                           | -3.6 43.5   | 34 42.8 | -2.6 43.9   | 35 25.9 | -1.8 44.4   | 36 08.5 | -0.9 44.9   | 36 50.8 | +0.0 45.5   | 37 32.7 | +0.9 46.0   | 38 14.2 | +1.9 46.6   | 38 95.7 | +2.9 47.2   | 39 77.2 | +3.9 47.8   | 40 58.7                                                                              | +4.9 48.4   | 51   |  |  |
| 52               | 23 11.4 | -5.1 41.8   | 34 03.9                           | -4.2 42.3   | 34 40.2 | -3.4 42.7   | 35 24.1 | -2.6 43.2   | 36 07.6 | -1.6 43.7   | 36 50.5 | +0.7 44.2   | 37 32.4 | +1.6 44.7   | 38 15.1 | +2.6 45.3   | 38 96.6 | +3.6 45.9   | 39 78.1 | +4.6 46.5   | 40 59.6                                                                              | +5.6 47.1   | 52   |  |  |
| 53               | 23 06.3 | -5.8 40.6   | 34 05.7                           | -5.0 41.1   | 34 36.8 | -4.2 41.5   | 35 21.5 | -3.2 42.0   | 36 06.0 | -2.5 42.5   | 36 50.1 | -1.6 43.0   | 37 33.8 | -0.7 43.5   | 38 17.1 | +0.3 44.0   | 38 98.6 | +1.3 44.6   | 39 80.1 | +2.3 45.2   | 40 61.6                                                                              | +3.3 45.8   | 53   |  |  |
| 54               | 23 00.5 | -6.4 39.4   | 34 06.7                           | -5.6 39.9   | 34 32.6 | -4.8 40.3   | 35 18.3 | -4.1 40.8   | 36 03.5 | -3.1 41.2   | 36 48.5 | -2.3 41.7   | 37 33.1 | -1.4 42.2   | 38 17.4 | -0.6 42.7   | 38 98.9 | +0.4 43.3   | 39 80.4 | +1.4 43.9   | 40 61.9                                                                              | +2.4 44.5   | 54   |  |  |

## Celestial Fix and Running Fix Problems

Step 4: Given the azimuth information in step 3 (which does not account for increments of declination), construct a table to determine correct azimuths.

| Sight                                       |                                                                 | <i>Sirius (1836)</i> | <i>Regulus (1842)</i> | <i>Mirfak (1900)</i> |
|---------------------------------------------|-----------------------------------------------------------------|----------------------|-----------------------|----------------------|
| <i>Base Azimuth (Z)</i>                     | <i>From HO229</i>                                               | 167.5°               | 103.1°                | 47.4°                |
| <i>Next incremental Z</i>                   |                                                                 | 167.8°               | 101.8°                | 46.2°                |
| <i>Difference</i>                           |                                                                 | 0.3°                 | -1.3°                 | -1.2°                |
| <i>Declination Increment</i>                | <i>From given declination</i>                                   | 41.7'                | 3.5'                  | 47.7'                |
| <i>Correction (Diff Z x Increment) / 60</i> |                                                                 | +0.2°                | -0.1°                 | -1.0°                |
| <i>Corrected azimuth (Z)</i>                |                                                                 | 167.7°               | 103.0°                | 46.5°                |
| <i>Azimuth rules corrected azimuth (Zn)</i> | <i>Check azimuth rules for LHA on top/bottom of HO229 pages</i> | <b>192.3°</b>        | <b>103.0°</b>         | <b>313.6°</b>        |

| Dec.<br>Inc. | Altitude Difference (d) |      |      |      |      |          |     |     |     |     |       |     |     |     |     |     |  |  |  |
|--------------|-------------------------|------|------|------|------|----------|-----|-----|-----|-----|-------|-----|-----|-----|-----|-----|--|--|--|
|              | Tens                    |      |      |      |      | Decimals |     |     |     |     | Units |     |     |     |     |     |  |  |  |
|              | 10'                     | 20'  | 30'  | 40'  | 50'  | ↓        | 0'  | 1'  | 2'  | 3'  | 4'    | 5'  | 6'  | 7'  | 8'  | 9'  |  |  |  |
| 0.0          | 0.0                     | 0.0  | 0.0  | 0.0  | 0.0  | .0       | 0.0 | 0.0 | 0.0 | 0.0 | 0.0   | 0.0 | 0.0 | 0.1 | 0.1 | 0.1 |  |  |  |
| 0.1          | 0.0                     | 0.0  | 0.0  | 0.0  | 0.0  | .1       | 0.0 | 0.0 | 0.0 | 0.0 | 0.0   | 0.0 | 0.0 | 0.1 | 0.1 | 0.1 |  |  |  |
| 0.2          | 0.0                     | 0.0  | 0.1  | 0.1  | 0.1  | .2       | 0.0 | 0.0 | 0.0 | 0.0 | 0.0   | 0.0 | 0.0 | 0.1 | 0.1 | 0.1 |  |  |  |
| 0.3          | 0.0                     | 0.1  | 0.1  | 0.2  | 0.2  | .3       | 0.0 | 0.0 | 0.0 | 0.0 | 0.0   | 0.0 | 0.0 | 0.1 | 0.1 | 0.1 |  |  |  |
| 0.4          | 0.1                     | 0.1  | 0.2  | 0.3  | 0.3  | .4       | 0.0 | 0.0 | 0.0 | 0.0 | 0.0   | 0.0 | 0.0 | 0.1 | 0.1 | 0.1 |  |  |  |
| 0.5          | 0.1                     | 0.2  | 0.3  | 0.3  | 0.4  | .5       | 0.0 | 0.0 | 0.0 | 0.0 | 0.0   | 0.0 | 0.0 | 0.1 | 0.1 | 0.1 |  |  |  |
| 0.6          | 0.1                     | 0.2  | 0.3  | 0.4  | 0.5  | .6       | 0.0 | 0.0 | 0.0 | 0.0 | 0.0   | 0.0 | 0.0 | 0.1 | 0.1 | 0.1 |  |  |  |
| 0.7          | 0.1                     | 0.3  | 0.4  | 0.5  | 0.6  | .7       | 0.0 | 0.0 | 0.0 | 0.0 | 0.0   | 0.0 | 0.0 | 0.1 | 0.1 | 0.1 |  |  |  |
| 0.8          | 0.2                     | 0.3  | 0.4  | 0.6  | 0.7  | .8       | 0.0 | 0.0 | 0.0 | 0.0 | 0.0   | 0.0 | 0.0 | 0.1 | 0.1 | 0.1 |  |  |  |
| 0.9          | 0.2                     | 0.3  | 0.5  | 0.6  | 0.8  | .9       | 0.0 | 0.0 | 0.0 | 0.0 | 0.0   | 0.0 | 0.0 | 0.1 | 0.1 | 0.1 |  |  |  |
| 27.0         | 4.5                     | 9.0  | 13.5 | 18.0 | 22.5 | .0       | 0.0 | 0.5 | 0.9 | 1.4 | 1.8   | 2.3 | 2.7 | 3.2 | 3.7 | 4.1 |  |  |  |
| 27.1         | 4.5                     | 9.0  | 13.5 | 18.0 | 22.6 | .1       | 0.0 | 0.5 | 1.0 | 1.4 | 1.9   | 2.3 | 2.8 | 3.3 | 3.7 | 4.2 |  |  |  |
| 27.2         | 4.5                     | 9.0  | 13.6 | 18.1 | 22.6 | .2       | 0.1 | 0.5 | 1.0 | 1.5 | 1.9   | 2.4 | 2.8 | 3.3 | 3.8 | 4.2 |  |  |  |
| 27.3         | 4.5                     | 9.1  | 13.6 | 18.2 | 22.7 | .3       | 0.1 | 0.6 | 1.1 | 1.5 | 2.0   | 2.4 | 2.9 | 3.3 | 3.8 | 4.3 |  |  |  |
| 27.4         | 4.6                     | 9.1  | 13.7 | 18.3 | 22.8 | .4       | 0.2 | 0.6 | 1.1 | 1.6 | 2.0   | 2.5 | 2.9 | 3.4 | 3.8 | 4.3 |  |  |  |
| 27.5         | 4.6                     | 9.2  | 13.8 | 18.3 | 22.9 | .5       | 0.2 | 0.7 | 1.1 | 1.6 | 2.1   | 2.5 | 3.0 | 3.4 | 3.9 | 4.4 |  |  |  |
| 27.6         | 4.6                     | 9.2  | 13.8 | 18.4 | 23.0 | .6       | 0.3 | 0.7 | 1.2 | 1.6 | 2.1   | 2.6 | 3.0 | 3.5 | 3.9 | 4.4 |  |  |  |
| 27.7         | 4.6                     | 9.3  | 13.9 | 18.5 | 23.1 | .7       | 0.3 | 0.8 | 1.2 | 1.7 | 2.2   | 2.6 | 3.1 | 3.5 | 4.0 | 4.4 |  |  |  |
| 27.8         | 4.7                     | 9.3  | 13.9 | 18.6 | 23.2 | .8       | 0.4 | 0.8 | 1.3 | 1.7 | 2.2   | 2.7 | 3.1 | 3.6 | 4.0 | 4.5 |  |  |  |
| 27.9         | 4.7                     | 9.3  | 14.0 | 18.6 | 23.3 | .9       | 0.4 | 0.9 | 1.3 | 1.8 | 2.2   | 2.7 | 3.2 | 3.6 | 4.1 | 4.5 |  |  |  |
| 58.0         | 9.6                     | 19.3 | 29.0 | 38.6 | 48.3 | .0       | 0.0 | 1.0 | 1.9 | 2.9 | 3.9   | 4.9 | 5.8 | 6.8 | 7.8 | 8.8 |  |  |  |
| 58.1         | 9.7                     | 19.3 | 29.0 | 38.7 | 48.4 | .1       | 0.1 | 1.1 | 2.0 | 3.0 | 4.0   | 5.0 | 5.9 | 6.9 | 7.9 | 8.9 |  |  |  |
| 58.2         | 9.7                     | 19.4 | 29.1 | 38.8 | 48.5 | .2       | 0.2 | 1.2 | 2.1 | 3.1 | 4.1   | 5.1 | 6.0 | 7.0 | 8.0 | 9.0 |  |  |  |
| 58.3         | 9.7                     | 19.4 | 29.1 | 38.9 | 48.6 | .3       | 0.3 | 1.3 | 2.2 | 3.2 | 4.2   | 5.2 | 6.1 | 7.1 | 8.1 | 9.1 |  |  |  |
| 58.4         | 9.7                     | 19.5 | 29.2 | 38.9 | 48.7 | .4       | 0.4 | 1.4 | 2.3 | 3.3 | 4.3   | 5.3 | 6.2 | 7.2 | 8.2 | 9.2 |  |  |  |
| 58.5         | 9.8                     | 19.5 | 29.3 | 39.0 | 48.8 | .5       | 0.5 | 1.5 | 2.4 | 3.4 | 4.4   | 5.4 | 6.3 | 7.3 | 8.3 | 9.3 |  |  |  |
| 58.6         | 9.8                     | 19.5 | 29.3 | 39.1 | 48.8 | .6       | 0.6 | 1.6 | 2.5 | 3.5 | 4.5   | 5.5 | 6.4 | 7.4 | 8.4 | 9.4 |  |  |  |
| 58.7         | 9.8                     | 19.6 | 29.4 | 39.2 | 48.9 | .7       | 0.7 | 1.7 | 2.6 | 3.6 | 4.6   | 5.6 | 6.5 | 7.5 | 8.5 | 9.5 |  |  |  |
| 58.8         | 9.8                     | 19.6 | 29.4 | 39.2 | 49.0 | .8       | 0.8 | 1.8 | 2.7 | 3.7 | 4.7   | 5.7 | 6.6 | 7.6 | 8.6 | 9.6 |  |  |  |
| 58.9         | 9.9                     | 19.7 | 29.5 | 39.3 | 49.1 | .9       | 0.9 | 1.9 | 2.8 | 3.8 | 4.8   | 5.8 | 6.7 | 7.7 | 8.7 | 9.7 |  |  |  |

## Celestial Fix and Running Fix Problems

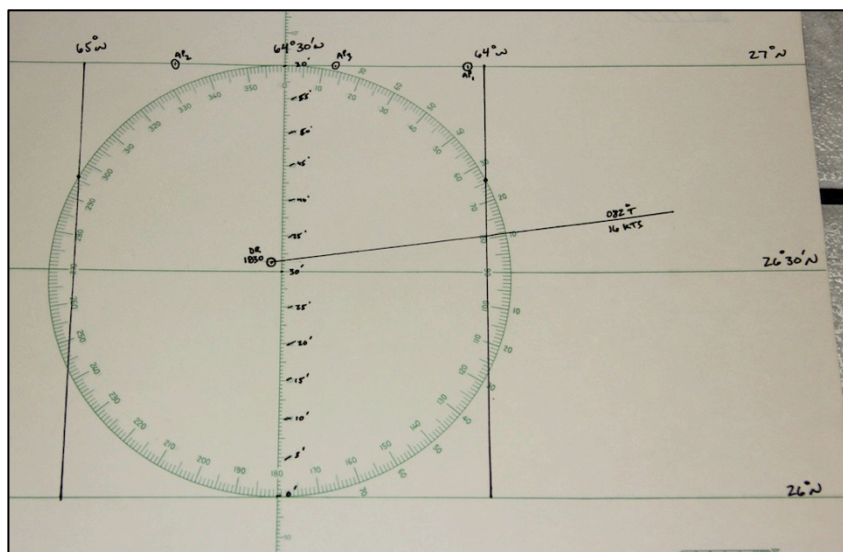
Step 5: Given the tabular HO229 information in step 3, determine the correct computed altitude (hc) for the three-star sights.

| Sight                     |                                       | <i>Sirius (1836)</i> | <i>Regulus (1842)</i> | <i>Mirfak (1900)</i> |
|---------------------------|---------------------------------------|----------------------|-----------------------|----------------------|
| Tabular computed altitude | <i>From step 3</i>                    | <b>46° 07.3'</b>     | <b>48° 46.6'</b>      | <b>36° 08.0'</b>     |
| Altitude difference (d)   | <i>From step 3</i>                    | <b>-58.8'</b>        | <b>27.2'</b>          | <b>0.7'</b>          |
| Declination increment     | <i>From given declination</i>         | 41.7'                | 3.5'                  | 47.7'                |
| Altitude difference       | <i>From HO229 interpolation table</i> | -40.9'               | +1.6'                 | +0.6'                |
| Correct computed altitude |                                       | <b>45° 26.4</b>      | <b>48° 48.2'</b>      | <b>36° 08.6'</b>     |

Step 6: Compare the observed altitudes (given) with the computed altitudes (determined in step 5), to compute intercepts (a) for the three-star sights.

| Sight                          |                                              | <i>Sirius (1836)</i> | <i>Regulus (1842)</i> | <i>Mirfak (1900)</i> |
|--------------------------------|----------------------------------------------|----------------------|-----------------------|----------------------|
| Observed altitude (ho)         | <i>Given</i>                                 | 46° 00.5'            | 49° 07.2'             | 35° 51.6'            |
| Correct computed altitude (hc) | <i>From step 5</i>                           | <b>45° 26.4'</b>     | <b>48° 48.2'</b>      | <b>36° 08.6'</b>     |
| Intercept (a)                  | <i>hc – ho</i>                               | <b>34.1'</b>         | <b>19.0'</b>          | <b>17.0'</b>         |
| Towards/Away                   | <i>If hc is greater, intercept is "away"</i> | <b>Towards</b>       | <b>Towards</b>        | <b>Away</b>          |
| Azimuth                        | <i>Repeated from step 4</i>                  | 192.3°               | 103.0°                | 313.6°               |

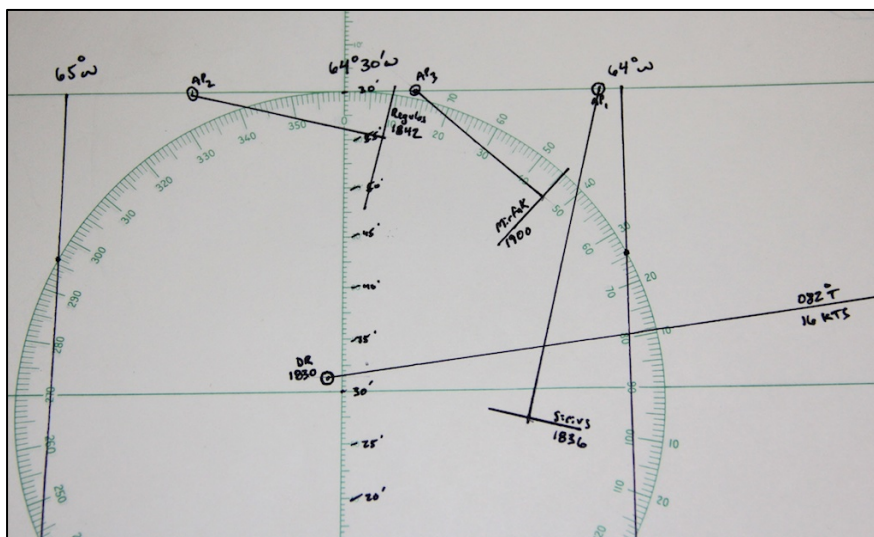
Step 7: Plot the assumed positions for each star sight.





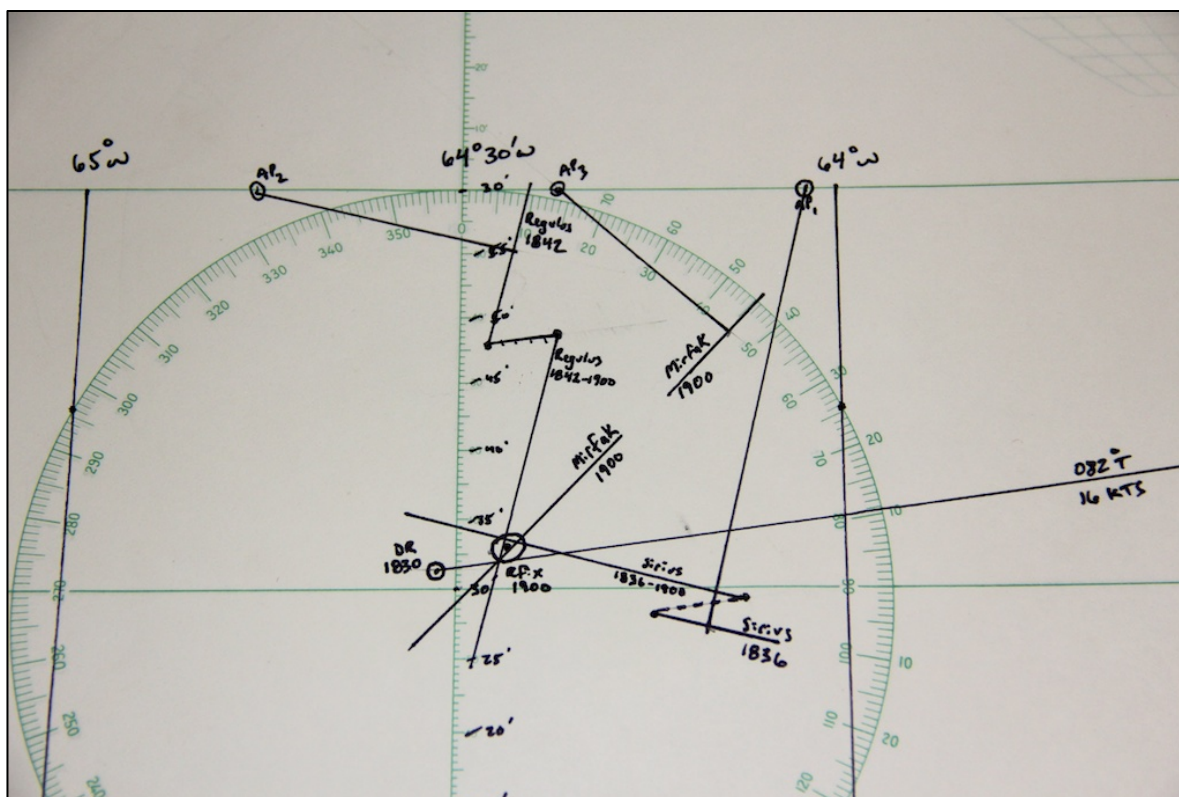
## Celestial Fix and Running Fix Problems

Step 8: Plot each star sight's line of position.



Step 9: Advance the 1836 and 1842 star lines of position to 1900 to determine the running fix.

Fix:  $26^{\circ} 33' N, 64^{\circ} 27' W$



## Celestial Fix and Running Fix Problems

### Sun Problems

FIX B1. On 2 April your 0830 zone time fix gives you a position of latitude  $20^{\circ} 16.0' S$ , longitude  $004^{\circ} 12' E$ . Your vessel is steaming on a course of  $143^{\circ} T$  at a speed of 18 knots. An observation of the Sun's upper limb is made at 0903 zone time, and the observed altitude (ho) is  $42^{\circ} 39.6'$ . The chronometer reads 09h 05m 40s and the chronometer error is 2m 15s fast. Local apparent noon occurs at 1145 zone time and a meridian altitude of the Sun's lower limb is observed. The observed altitude (ho) for this sight is  $63^{\circ} 46.2'$ . Determine the vessel's 1200 position.

- a)  $21^{\circ} 10.1' S$ ,  $004^{\circ} 53.9' E$
- b)  $21^{\circ} 14.0' S$ ,  $004^{\circ} 55.0' E$
- c)  **$21^{\circ} 18.0' S$ ,  $005^{\circ} 00.5' E$  - correct**
- d)  $22^{\circ} 42.0' S$ ,  $004^{\circ} 57.0' E$

FIX B2. On 17 January your 0730 zone time fix gives you a position of latitude  $22^{\circ} 26.0' S$ , longitude  $152^{\circ} 17.0' E$ . Your vessel is steaming on a course of  $116^{\circ} T$  at a speed of 17 knots. An observation of the Sun's lower limb is made at 1015 zone time. The chronometer reads 00h 13m 23s and the chronometer error is 1m 49s slow. The observed altitude (ho) is  $66^{\circ} 02.1'$ . LAN occurs at 1152 zone time and a meridian altitude of the Sun's lower limb is made. The observed altitude (ho) is  $87^{\circ} 54.2'$ . Determine the vessel's 1200 zone time position.

- a)  **$22^{\circ} 53.8' S$ ,  $153^{\circ} 25.6' E$  - correct**
- b)  $22^{\circ} 53.8' S$ ,  $153^{\circ} 28.8' E$
- c)  $22^{\circ} 56.3' S$ ,  $153^{\circ} 25.6' E$
- d)  $22^{\circ} 56.3' S$ ,  $153^{\circ} 28.8' E$

FIX B3. On 24 March your 0800 zone time fix gives you a position of latitude  $22^{\circ} 16' N$ , longitude  $31^{\circ} 45' W$ . Your vessel is steaming on a course of  $285^{\circ} T$  at a speed of 16.5 knots. An observation of the Sun's upper limb is made at 0938 zone time, and the observed altitude (ho) is  $46^{\circ} 32.2'$ . The chronometer reads 11h 41m 01s and the chronometer error is 02m 50s fast. Local apparent noon occurs at 1214 zone time and a meridian altitude of the Sun's lower limb is made. The observed altitude (ho) for this sight is  $68^{\circ} 55.8'$ . Determine the vessel's 1200 zone time position.

- a)  $22^{\circ} 35.0' N$ ,  $30^{\circ} 29.0' W$
- b)  **$22^{\circ} 35.0' N$ ,  $32^{\circ} 51.0' W$  - correct**
- c)  $22^{\circ} 36.0' N$ ,  $32^{\circ} 10.5' W$
- d)  $22^{\circ} 36.0' N$ ,  $32^{\circ} 55.2' W$

FIX B4. On 29 April your 0530 zone time position was latitude  $23^{\circ} 04.0'$  S, longitude  $162^{\circ} 12.0'$  E. Your vessel was steaming on course  $120^{\circ}$  T at a speed of 9 knots. An observation of the Sun's upper limb was made at 0830 zone time. The chronometer read 09h 27m 32s and was slow 2m 24s. The observed altitude (ho) was  $24^{\circ} 58.0'$ . LAN occurred at 1205 zone time. The observed altitude (ho) was  $52^{\circ} 04.0'$ . What was the longitude of your 1200 zone time running fix?

- a)  $163^{\circ} 02.1'$  E
- b)  $163^{\circ} 06.0'$  E - correct**
- c)  $163^{\circ} 09.5'$  E
- d)  $163^{\circ} 11.3'$  E

FIX B5. On 22 February, your 0800 zone time position is latitude  $24^{\circ} 16'$  S, longitude  $95^{\circ} 37'$  E. Your vessel is on course  $126^{\circ}$  T at a speed of 14 knots. An observation of the Sun's lower limb is made at 0945 zone time. The chronometer reads 03h 47m 22s and the chronometer error is 02m 37s fast. The observed altitude (ho) is  $57^{\circ} 02.1'$ . LAN occurs at 1148 zone time, and a meridian altitude of the Sun's lower limb is made. The observed meridian altitude (ho) is  $75^{\circ} 22.3'$ . Determine the vessel's 1200 zone time position.

- a)  $24^{\circ} 49.3'$  S,  $96^{\circ} 24.0'$  E
- b)  $24^{\circ} 49.3'$  S,  $96^{\circ} 27.2'$  E
- c)  $24^{\circ} 52.2'$  S,  $96^{\circ} 24.0'$  E - correct**
- d)  $24^{\circ} 52.2'$  S,  $96^{\circ} 27.2'$  E



### Any Celestial Body Problems

FIX B6. On 15 August your vessel is en route from Bombay to San Francisco. You are steering course 020° T and making a speed of 20 knots. Your 1830 zone time DR is latitude 26° 13.0' N, longitude 135° 18.0' W. You observe 3 celestial bodies. Determine the latitude and longitude of your 1935 running fix.

| Body   | Zone Time | GHA        | Observed Altitude | Declination |
|--------|-----------|------------|-------------------|-------------|
| Spica  | 1848      | 180° 24.3' | 32° 21.4'         | S 11° 03.8' |
| Altair | 1910      | 89° 29.8'  | 43° 06.3'         | N 8° 49.3'  |
| Kochab | 1935      | 170° 33.4' | 39° 12.0'         | N 74° 14.3' |

- a) 26° 15.9' N, 135° 03.6' W
- b) 26° 35.3' N, 135° 24.8' W
- c) 26° 40.5' N, 135° 21.6' W
- d) **26° 48.1' N, 135° 20.7' W - correct**

FIX B7. On 16 April your 0200 zone time DR position is latitude 17° 18' S, longitude 168° 46' E. You are on course 236° T at a speed of 16 knots. You observe 3 celestial bodies. Determine the latitude and longitude of your 0600 running fix.

| Body      | Zone Time | GHA        | Observed Altitude | Declination |
|-----------|-----------|------------|-------------------|-------------|
| Fomalhaut | 0523      | 133° 27.1' | 35° 40.4'         | S 29° 43.4' |
| Peacock   | 0527      | 172° 33.9' | 48° 28.6'         | S 56° 47.6' |
| Antares   | 0531      | 232° 32.3' | 51° 43.9'         | S 26° 23.4' |

- a) 17° 54.9' S, 167° 48.7' E
- b) 17° 55.6' S, 167° 45.1' E
- c) 17° 56.8' S, 167° 52.4' E
- d) **18° 00.4' S, 167° 49.2' E - correct**

FIX B8. On 12 October, your vessel is on course 081° T, speed 20 knots. Your 1800 zone time DR position is latitude 26° 11.0' S, longitude 77° 18.0' E. You observe 3 celestial bodies. Determine the latitude and longitude of your 1835 zone time running fix.

| Body      | Zone Time | GHA        | Observed Altitude | Declination |
|-----------|-----------|------------|-------------------|-------------|
| Vega      | 1810      | 299° 26.6' | 23° 08.7'         | N 38° 46.3' |
| Fomalhaut | 1823      | 237° 37.0' | 50° 23.9'         | S 29° 43.2' |
| Antares   | 1835      | 337° 43.4' | 40° 53.1'         | S 26° 23.4' |

- a) 26° 05.5' S, 77° 14.5' E
- b) 26° 07.5' S, 77° 34.0' E
- c) 26° 09.0' S, 77° 27.5' E
- d) 26° 12.0' S, 77° 31.0' E - correct**

FIX B9. On 20 Nov, your 1030 ZT DR position is LAT 27° 16.0'N, LONG 157° 18.6'E. You are on course 060° T at a speed of 20 knots. You observe three celestial bodies. Determine the latitude and longitude of your 1200 running fix.

| Body  | Zone Time | GHA        | Observed Altitude | Declination |
|-------|-----------|------------|-------------------|-------------|
| Moon  | 1030      | 259° 24.4' | 34° 01.5'         | N 9° 47.3'  |
| Sun   | 1116      | 202° 30.5' | 43° 00.0'         | S 19° 38.0' |
| Venus | 1200      | 162° 57.7' | 24° 26.9'         | S 26° 02.4' |

- a) 27° 16.8' N, 157° 30.5' E
- b) 27° 22.6' N, 157° 37.8' E
- c) 27° 29.7' N, 157° 43.0' E - correct**
- d) 27° 33.4' N, 157° 48.2' E

FIX B10. On 22 Nov, your vessel is en route from Accra Ghana to Montevideo, Uruguay. You are on course 240° T and making a speed of 15 knots. Your 1129 DR position is LAT 28° 25'S, LONG 42° 40W. You observe three celestial bodies. Determine the latitude and longitude of your 1137 running fix.

| Body  | Zone Time | GHA        | Observed Altitude | Declination |
|-------|-----------|------------|-------------------|-------------|
| Venus | 1129      | 350° 00.1' | 43° 26.8'         | S 25° 41.8' |
| Moon  | 1134      | 082° 54.7' | 43° 15.0'         | S 01° 46.5' |
| Sun   | 1137      | 042° 38.0' | 81° 44.7'         | S 20° 11.7' |

- a) 28° 27.0' S, 42° 38.0' W - correct**
- b) 28° 25.2' S, 42° 40.0' W
- c) 28° 25.0' S, 42° 36.0' W
- d) 28° 23.4' S, 42° 42.0' W